





















SYSTEM

OF

GEOMETRY AND TRIGONOMETRY:

199

TOGETHER WITH A

TREATISE ON SURVEYING;

TEACHING VARIOUS WAYS OF TAKING THE SURVEY OF A FIELD; ALSO TO PROTRACT THE SAME AND FIND THE AREA.

LIKEWISE,

RECTANGULAR SURVEYING;

or,

AN ACCURATE METHOD OF CALCULATING THE AREA OF ANY FIELD ARITHMETI;

CALLY, WITHOUT THE NECESSITY OF PLOTTING IT.

TO THE WHOLE ARE ADDED

SEVERAL MATHEMATICAL TABLES.

NECESSARY FOR SULVING QUESTIONS IN

TRIGONOMETRY AND SURVEYING,

WITH A

PARTICULAR EXPLANATION OF THOSE TABLES,

THIRD EDITION.

COMPILED FROM VARIOUS AUTHORS,

BY ABEL FLINT, A. M.

HARTFORD:

PUBLISHED BY OLIVER D. COOKE.

Samuel T. Armstrong, Printer, Baston.
1813.

DISTRICT OF CONNECTICUT, SS.

(L. S.) BE IT REMEMBERED, That on the thirtieth day of October, in the twenty-ninth year of the Independence of the United States of America, OLIVER D. COOKE, of the said District hath deposited in this Office the title of a Book, the right whereof he claims as Proprietor in the words following, viz

"A System of Geometry and Trigonometry: together with a Treatise on Surveying; teaching various ways of taking the Survey of a Field; also to protract the same and find the Area. Likewise Rectangular Surveying; or, an accurate method of calculating the Area of any Field arithmetically, without the necessity of Plotting it. To the whole are added several mathematical Tables, necessary for solving questions in Trigonometry and Surveying; with a particular explanation of those Tables, and the manner of using them. Compiled from various Authors, by ABEL FLINT, A. M."

In conformity to the Act of the Congress of the United States entitled, "An Act for the Encouragement of Learning by securing the Copies of Maps, Charts and Books to the Authors and Proprietors of such Copies during the times therein mentioned."

C. DENISON. Clerk of the District of Connecticut.

Connecticut ss. District Clerk's Office,

A true Copy of Record—Attest,

CH. DENISON, Clerk.

RECOMMENDATIONS.

HAVING perused, with some attention, the following Treatise on Surveying, in Manuscript, it appears to me to be estimable for its simplicity and perspicuity; and, by excluding all matter but remotely connected with the main subject, and reducing the Tables of Logarithms, of Logarithmic Sines, Tangents and Secants, and of Difference of Latitude and Departure, without impairing their use, in their application to most cases which occur in common Surveying, and supplying any possible defect by a Table of Natural Sines, to comprise, in the limits of a pocket Volume, whatever is most essential and most useful in the Art, including the important modern improvement of RECTANGULAR SURVEYING; and on the whole, particularly from the size of the volume, to be well adapted to general use.

JOHN TREADWELL.

FARMINGTON, September 20th, 1804.

WE the subscribers have carefully perused a Treatise on Surveying, prepared for the Press by the Rev. Abel Flint, of Hartford; and find it worthy of the public patronage. Every thing not immediately necessary for the practical Surveyor has been excluded; while it comprises all which is requisite in

Field Surveying, both on the old and new plan; elucidated and explained with a degree of conciseness and perspicuity not usually to be found in Treatises on the same subject. The Mathematical Tables are reduced to less than half the size occupied by others; and any inconvenience which might result from such reduction is obviated by the insertion of a Table of Natural Sines, not usually found in works of this nature. The Surveyor who shall own this will not be under the necessity of purchasing Gibson, which is a more expensive work.

ASHER MILLER, Surveyor General. GEORGE GILLET, Deputy Surveyor for Tolland County.

MIDDLETOWN, October 3d, 1804.

PREFACE.

The following work is chiefly a compilation from other Books; and but very little new is added except a more full explanation, than has yet been published, of Rectangular Surveying, or the method of calculating the Area of Fields arithmetically, without drawing a plot of them and measuring with a Scale and Dividers, as has been the common practice; and also a more particular explanation of the use of Natural Sines than is contained in most Mathematical Books.

The Compiler has endeavored to render this work so easy and intelligible that a Learner will require but little assistance from an Instructor, except with regard to the construction and use of Mathematical and Surveying instruments. Before, however, he enters on the study of this Book he must be well acquainted with common Arithmetic, with Decimal Fractions and the Square Root; and he must also know the various characters or marks used in Arithmetic.

A Surveyor will doubtless find many questions arise in the course of his practice, for the solution of which no particular directions are here given; nor is it possible to give directions for every case that may occur. In all practical Sciences much must be left to the judgment of the practitioner, who, if he is well acquainted with the general principles of his Art, will readily learn to apply those principles to particular cases.

The primary design of this treatise is to teach common Field Surveying; at the same time it contains the elements of Surveying upon a larger scale; and the system of Geometry and Trigonometry with which it is introduced, with the Problems for the mensuration of Superficies, as also the Mathematical Tables at the end, will be found useful for many other purposes. It would be well, therefore, for those who do not intend to become practical Surveyors to acquaint themselves with what is here taught; and with this view the following work is very proper to be introduced into Academies, and those higher Schools which are designed to fit young men for active business in life. Indeed every person who frequently buys and sells land should learn to calculate the Contents of a Field arithmetically; a knowledge which may be acquired in a very little time, from the particular explanation here given of that method.

Notwithstanding the many Books already published on the subjects here treated upon, it was thought a work of this kind was really wanted, and that if judiciously executed it would be useful. It is more particularly necessary at the present time in Connecticut, as the Legislature of the State have lately enacted a Law on the subject of Surveying, in consequence of which more attention must be paid to the Theory of that Art than has been common.

These considerations induced the Compiler to select from various publications what appeared to him important; and to arrange the whole in a method best adapted, in his view, for teaching that useful Art. How far he has succeeded in his endeavors to simplify the subject and render it easy to the Learner, must be submitted to the test of experience.

HARTFORD, (Con.) October, 1804.

A General view of the Contents of this Work.

THE System of Geometry is divided into two parts. The first contains Geometrical Definitions respecting Lines, Angles, Superficies, &c. The second part contains a number of Geometrical Problems necessary for Trigonometry and Surveying.

The System of Trigonometry is also divided into two parts; and teaches the solution of Questions in Right and Oblique angled Trigonometry by Logarithms and also by Natural Sines.

The Treatise on Surveying is divided into three parts. Part first treats of measuring Land, and is divided into three Sections. The first contains several Problems respecting Mensuration, and for finding the Area of various Right-lined Figures and Circles.

The second Section teaches different methods of taking the Survey of fields; also to protract them, and find their Area in the manner commonly practised, and likewise by Arithmetical and Trigonometrical calculations, without measuring Diagonals and Perpendiculars with a Scale and Dividers; interspersed with sundry useful rules and directions.

The third Section is a particular explanation and demonstration of Rectangular Surveying, or the method of computing the Area of Fields from the Field Notes, by Mathematical Tables, without the necessity of plotting the Field. To this Section is added a useful Problem for ascertaining the true Area of a Field which has been measured by a Chain too long or too short.

Part second treats of laying out Land in various shapes.

Part third contains sundry Problems and Rules for dividing Land and determining the true Course and Distance of dividing Lines, or from one part of a Field to another. To this is added an Appendix concerning the Variation of the Compass and Attraction of the Needle; also, a Rule to find the difference between the present Variation, and that at a time when a Tract was formerly surveyed, in order to trace or run out the original lines.

The Mathematical Tables, are A Traverse Table, or Table of Difference of Latitude and Departure, calculated for every Degree and quarter of a Degree, and for any distance up to 50; a Table of Natural Sines calculated for every Minute; a Table of Logarithms comprised in four pages, yet sufficiently extensive for common use; and a Table of Logarithmic or Artificial Sines, Tangents and Secants, calculated for every 5 Minutes of a Degree. To these Tables are prefixed particular explanations of the manner of using them.

GEOMETRY.

GEOMETRY is a Science which treats of the properties of Magnitude.

PART I.

Geometrical Definitions.

1. A Point is a small Dot; or, Mathematically considered, is that which has no parts, being of itself indivisible.

2. A Line has length but no breadth.

3. A Superficies or Surface, called also Area, has length and breadth, but no thickness.

4. A Solid has length, breadth and thickness.

5. A Right Line is the shortest that can be drawn between two Points.

6. The inclination of two Lines meeting one another, or the opening between them, is called an Angle. Thus at B. Plate I. Figure 1. is an Angle, formed

by the meeting of the Lines AB and BC.

7. If a right Line CD. Fig. 2. fall upon another Right Line AB, so as to incline to neither side, but make the Angles on each side equal, then those Angles are called Right Angles; and the Line CD is said to be Perpendicular to the other Line.

8. An Obtuse Angle is greater than a Right Angle;

as ADE. Fig. 3.

9. An Acute Angle is less than a Right Angle; as EDB. Fig. 3.

Note. When three letters are used to express an Angle, the middle letter denotes the angular Point.

10. A Circle is a round Figure, bounded by a Line equally distant from some Point, which is called the Centre. Fig. 4.

11. The Circumference or Periphery of a Circle is

the bounding Line; as ADEB. Fig. 4.

12. The Radius of a Circle is a Line drawn from the Centre to the Circumference; as CB. Fig. 4.

Therefore all Radii of the same Circle are equal.

13. The Diameter of a Circle is a Right Line drawn from one side of the Circumference to the other, passing through the Centre; and it divides the Circle into two equal parts, called Semicircles; as AB or DE. Fig. 5.

14. The Circumference of every Circle is supposed to be divided into 360 equal parts called Degrees; and each Degree into 60 equal parts, called Minutes; and each Minute into 60 equal parts, called Seconds;

and these into Thirds, &c.

Note. Since all Circles are divided into the same number of Degrees, a Degree is not to be accounted a quantity of any determinate length, as so many inches or Feet, &c. but is always to be reckoned as being the 360th part of the Circumference of any Circle, without regarding the bigness of the Circle.

15. An Arch or Arc of a Circle is any part of the Circumference; as BF or FD, Fig. 5; and is said to be an Arch of so many Degrees as it contains parts of 360 into which the whole Circle is divided.

16. A Chord is a Right Line drawn from one end of an Arch to the other, and is the measure of the Arch;

as HG is the Chord of the Arch HIG. Fig. 6.

Note. The Chord of an Arch of 60 degrees is equal in length to the Radius of the Circle of which the Arch is a part.

17. The Segment of a Circle is a part of a Circle, cut off by a Chord; thus the space comprehended between the Arch HIG and the Chord HG is called a Segment. Fig. 6.

18. A Quadrant is one quarter of a Circle; as ACB.

Fig. 6.

19. A Sector of a Circle is a space contained between two Radii and an Arch less than a Semicircle; as BCD

or ACD. Fig. 6.

20. The Sine of an Arch is a Line drawn from one end of the Arch, perpendicular to the Radius or Diameter drawn through the other end: Or, it is half the Chord of double the Arch; thus HL is the Sine of the Arch HB. Fig. 7.

21. The Sines on the same Diameter increase in length till they come to the Centre, and so become the Radius. Hence it is plain that the Radius CD Fig. 7. is the greatest possible Sine, or Sine of 90 Degrees.

22. The Versed Sine of an Arch is that part of the Diameter or Radius which is between the Sine and the Circumference; thus LB is the Versed Sine of the

Arch HB. Fig. 7.

23. The Tangent of an Arch is a Right Line touching the Circumference, and drawn perpendicular to the Diameter; and is terminated by a Line drawn from the Centre through the other end of the Arch; thus BK is the Tangent of the Arch BH. Fig. 7.

Note. The Tangent of an Arch of 45 Degrees is equal in length to the Radius of the Circle of which

the Arch is a part.

24. The Secant of an Arch is a Line drawn from the Centre through one end of the Arch till it meets the Tangent; thus CK is the Secant of the Arch BH. Fig. 7.

25. The Complement of an Arch is what the Arch wants of 90 Degrees, or a Quadrant; thus HD is the

Complement of the Arch BH. Fig. 7.

26. The Supplement of an Arch is what the Arch wants of 180 Degrees, or a Semicircle; thus ADH is the Supplement of the Arch BH. Fig. 7.

27. The Sine, Tangent or Secant of the Complement of any Arch is called the Co-Sine, Co-Tangent or Co-Secant of the Arch; thus FH is the Sine, DI the Tangent and CI the Secant of the Arch DH; or they are the Co-Sine, Co-Tangent and Co-Secant of the Arch BH. Fig. 7.

28. The measure of an Angle is the Arch of a Circle contained between the two Lines which form the Angle, the angular Point being the Centre; thus the Angle HCB. Fig. 7. is measured by the Arch BH; and is said to contain so many Degrees as the Arch does.

Note. An Angle is esteemed greater or less according to the opening of the Lines which form it, or as the Arch intercepted by those Lines contains more or fewer Degrees. Hence it may be observed, that the bigness of an Angle does not depend at all upon the length of the including Lines; for all Arches described on the same Point, and intercepted by the same Right Lines, contain exactly the same number of Degrees, whether the Radius be longer or shorter.

29. The Sine, Tangent or Secant of an Arch is also the Sine, Tangent or Secant of the Angle whose measure the Arch is.

30. Parallel Lines are such as are equally distant from each other, as AB and CD. Fig. 8.

31. A Triangle is a Figure bounded by three Lines;

as ABC. Fig. 9.

32. An Equilateral Triangle has its three sides equal in length to each other. Fig. 9.

33. An Isoceles Triangle has two of its sides equal,

and the other longer or shorter. Fig. 10.

34. A Scalene Triangle has three unequal Sides. Fig. 11.

35. A Right Angled Triangle has one Right Angle.

Fig. 12.

36. An Obtuse Angled Triangle has one Obtuse

Angle. Fig. 13.

37. An Acute Angled Triangle has all its Angles Acute. Fig. 9, or 10.

1 38. Acute and Obtuse Angled Triangles are called Oblique Angled Triangles, or simply Oblique Triangles; in all which the bottom Side is generally called the Base and the other two, Legs.

39. In a Right Angled Triangle the longest Side is called the Hypothenuse, and the other two, Legs, or

Base and Perpendicular.

Note. The three Angles of every Triangle being added together, will amount to 180 Degrees; consequently the two Acute Angles of a Right Angled Triangle amount to 90 Degrees, the Right Angle being also 90.

40. The perpendicular height of a Triangle is a Line drawn from one of the Angles to its opposite Side; thus the dotted Line AD. Fig. 14. is the perpendicular

height of the Triangle ABC.

Note. This Perpendicular may be drawn from either of the Angles; and whether it falls within the Triangle or on one of the Lines continued beyond the Triangle, is immaterial.

41. A Square is a Figure bounded by four equal Sides, and containing four Right Angles. Fig. 15.

42. A Parallelogram, or Oblong Square, is a Figure bounded by four Sides, the opposite ones being equal and the Angles Right. Fig. 16.

43. A Rhombus is a Figure bounded by four equal

Sides, but has its Angles Oblique. Fig. 17.

44. A Rhomboides is a Figure bounded by four Sides, the opposite ones being equal, but the Angles

Oblique. Fig. 18.

45. The perpendicular height of a Rhombus or Rhomboides is a Line drawn from one of the Angles to its opposite Side; thus the dotted Lines AB. Fig. 17. and Fig. 18. represent the perpendicular height of the Rhombus and Rhomboides.

46. A Trapezoid is a Figure bounded by four Sides, two of which are parellel though of unequal lengths.

Fig. 19. and Fig. 20.

Note. Fig. 19. is sometimes called a Right Angled Trapezium.

47. A Trapezium is a Figure bounded by four unequal Sides. Fig. 21.

48. A Diagonal is a Line drawn between two oppo-

site Angles; as the Line AB. Fig. 21.

49. Figures which consist of more than four Sides are called Polygons; if the sides are equal to each other they are called regular Polygons, and are sometimes named from the number of their Sides, as Pentagon or Hexagon, a Figure of five or six Sides, &c. if the Sides are unequal they are called irregular Polygons.

PART II.

Geometrical Problems.

PROBLEM I. To draw a Line parallel to another Line at any given distance as at the point D. to make a Line, parallel to the Line AB. Plate 1. Fig. 22.

With the Dividers take the nearest distance between the Point D and the given Line AB; with that distance set one foot of the Dividers any where on the Line AB, as at E, and draw the Arch C; through the Point D draw a Line so as just to touch the top of the Arch C.

A more convenient way to draw parallel Lines is with a parallel Rule.

PROBLEM II. To bisect a given Line; or to find the middle of it. Fig. 23.

Open the Dividers to any convenient distance, more than half the given Line AB, and with one foot in A describe an Arch above and below the Line, as at C and D; with the same distance, and one foot in B describe Arches to cross the former; lay a Rule from C to D, and where the Rule crosses the Line, as at E, will be the middle.

PROBLEM III. To erect a Perpendicular from the end, or any part of a given Line. Fig. 24.

Open the Dividers to any convenient distance, as from D to A, and with one foot on the Point D, from which the Perpendicular is to be erected, describe an Arch, as AEG; set off the same distance from A to E and from E to G; upon E and G describe two Arches to intersect each other at H; draw a line from H to D, and one Line will be perpendicular to the other.

Note. There are other methods of erecting a Perpen-

dicular, but this is the most simple.

PROBLEM IV. From a given Point, as at C, to drop a Perpendicular on a given Line AB. Fig. 25.

With one foot of the Dividers in C describe an Arch to cut the given Line in two places, as at F and G; upon F and G describe two Arches to intersect each other below the Line as at D; lay a Rule from C to D and draw a Line from C to the given Line.

Perpendiculars may be more readily raised and let fall, by a small Square made of Brass, Ivory or Wood.

PROBLEM V. To make an Angle at E, equal to a given Angle ABC. Fig. 26.

Open the Dividers to any convenient distance, and with one foot in B describe the Arch FG; with the same distance and one foot in E, describe an Arch from H; measure the Arch FG, and lay off the same distance on the Arch from H to I; draw a Line through I to E, and the Angles will be equal.

PROBLEM VI. To make an Acute Angle equal to a given number of Degrees, suppose 36. Fig. 27.

Draw the Line AB to any convenient length; from a Scale of Chords take 60 Degrees with the Dividers, and with one foot in B describe an Arch from the Line AB; from the same Scale take the given number of Degrees, 36, and lay it on the Arch from C to D; draw a Line from B through D, and the Angle at B will be an Angle of 36 Degrees.

PROBLEM VII. To make an Obtuse Angle, suppose of 110 Degrees. Fig. 28.

Take a Chord of 60 Degrees as before, and describe an Arch greater than a Quadrant; set off 90 Degrees from B to C, and from C to E set off the excess above 90, which is 20; draw a Line from G through E and the Angle will contain 110 Degrees.

Note. In a similar manner Angles may be measured; that is, with a Chord of 60 Degrees describe an Arch on the angular Point, and on a Scale of Chords measure the Arch intercepted by the Lines forming the angle.

A more convenient method of making and measuring Angles is to use a Protractor instead of a Scale and Dividers.

PROBLEM VIII. To make a Triangle of three given Lines, as BO, BL, LO. Fig. 29.

Draw the Line BL from B to L; from B, with the length of the Line BO, describe an Arch as at O; from L, with the length of the Line LO, describe another Arch to intersect the former; from O draw the Lines OB and OL, and BOL will be the Triangle required.

PROBLEM IX. To make a Right Angled Triangle, the Hypothenuse and Anlges being given. Fig. 30.

Suppose the Hypothenuse CA 25 Rods or Chains, the angle at C 35° 30′ and consequently the Angle at A 54° 30′. See Note after the 39th Geometrical Definition.

Note. When Degrees and Minutes are expressed, they are distinguished from each other by a small Cypher at the right hand of the Degrees, and a Dash at the right hand of the Minutes; thus 35° 30' is 35 Degrees and 30 Minutes.

Draw the Line CB an indefinite length; at C make an Angle of 35° 30'; through where that number of Degrees cuts the Arch draw the Line CA 25 Rods, which must be taken from some Scale of equal parts; drop a Perpendicular from A to B, and the Triangle will be completed.

Note. The length of the two Legs may be found by measuring them upon the same Scale of equal parts from which the Hypothenuse was taken.

PROBLEM X. To make a Right Angled Triangle, the Angles and one Leg being given. Fig. 31.

Suppose the Angle at C 33° 15′, and the Leg AC 285.

Draw the Leg AC making it in length 285; at A erect a Perpendicular an indefinite length; at C make an Angle of 33° 15'; through where that number of Degrees cuts the Arch draw a Line till it meets the Perpendicular at B.

Note. If the given Line CA should not be so long as the Chord of 60°, it may be continued beyond A, for the purpose of making the Angle.

PROBLEM XI. To make a right Angled Triangle, the Hypothenuse and one Leg being given. Fig. 32.

Suppose the Hypothenuse AC 40, and the Leg AB 28.

Draw the Leg AB in length 28; from B erect a Perpendicular an indefinite length; take 40 in the Dividers, and setting one foot in A, wherever the other foot strikes the Perpendicular will be the Point C.

Note. When the Triangle is constructed the Angles may be measured by a Protractor, or by a Scale of Chords.

PROBLEM XII. To make a Right Angled Triangle, the two Legs being given. Fig. 33.

Suppose the Leg AB 38, and the Leg BC 46.

Draw the Leg AB in length 38; from B erect a Perpendicular to C in length 46; and draw a Line from A to C.

PROBLEM XIII. To make an Oblique Angled Triangle, the Angles and one Side being given. Fig. 34.

Suppose the side BC 98; the Angle at B 45° 15′, the Angle at D 108° 30′, consequently the other Angle 26° 15′.

Draw the side BC in length 98; on the Point B make an angle of 45° 15′; on the Point C make an Angle of 26° 15′, and draw the Lines BD and CD.

PROBLEM XIV. To make an Oblique Angled Triangle, two Sides and an Angle opposite to one of them being given. Fig. 35.

Suppose the Side BC 160, the Side BD 79, and the

Angle at C 29° 9'.

Draw the Side BC in length 160; at C make an Angle of 29° 9′, and draw an indefinite Line through where the degrees cut the Arch; take 79 in the Dividers, and with one foot in B lay the other on the Line CD; the point D will be the other Angle of the Triangle.

PROBLEM XV. To make an Oblique Angled Triangle, two Sides and their contained Angle being given. Fig. 36.

Suppose the Side BC 109, the Side BD 76, and the

Angle at B 101° 30'.

Draw the Side BC in length 109; at B make an Angle of 101° 30′ and draw the Side BD in length 76; draw a Line from D to C and it is done.

PROBLEM XVI. To Make a square. PLATE II. Fig. 37.

Draw the Line AB the length of the proposed Square; from B erect a Perpendicular to C and make it of the same length as AB; from A and C, with the same distance in the Dividers, describe Arches intersecting each other at D, and draw the Lines AD and DC.

PROBLEM XVII. To make a Parallelogram. Fig. 38.

Draw the Line AB equal to the longest Side of the Parallelogram; on B erect a Perpendicular the length of the shortest side to C; from C, with the longest Side,

and from A, with the shortest Side, describe Arches intersecting each other at D, and draw the Lines AD and CD.

PROBLEM XVIII. To describe a Circle which shall pass through any three given Points, not lying in a Right Line, as A, B, D. Fig. 43.

Draw Lines from A to B and from B to D; bisect those Lines by PROBLEM II. and the Point where the bisecting Lines intersect each other, as at C, will be the Centre of the Circle.

PROBLEM XIX. To find the centre of a Circle. By the last Problem it is plain, that if three Points be any where taken in the given Circle's Periphery, the Centre of the Circle may be found as there taught.

Directions for constructing irregular Figures of four or more sides may be found in the following Treatise on Surveying.

TRIGONOMETRY.

TRIGONOMETRY is that part of practical Geometry by which the Sides and Angles of Triangles are measured; whereby three things being given, either all Sides or Sides and Angles, a fourth may be found; either by measuring with a Scale and Dividers, according to the Problems in Geometry, or more accurately by calculation with Logarithms, or with Natural Sines.

TRIGONOMETRY is divided into two Parts, Rectangular and Oblique-angular.

PART I.

RECTANGULAR TRIGONOMETRY.

This is founded on the following methods of apply-

ing a Triangle to a Circle.

PROPOSITION I. In every Right Angled Triangle, as ABC, PLATE II. Figure 44. it is plain from PLATE I. Fig. 7. compared with the Geometrical Definitions to which that Figure refers, that if the Hypothenuse AC be made Radius, and with it an Arch of a Circle be described from each end, BC will be the Sine of the Angle at A, and AB the Sine of the Angle at C; that is, the Legs will be Sines of their opposite Angles.

PROPOSITION II. If one Leg, AB, Fig. 45. be made Radius, and with it on the Point A an Arch

be described, then BC, the other Leg, will be the Tangent and AC the Secant of the Angle at A; and if BC be made Radius, and an Arch be described with it on the Point C, then AB will be the Tangent and AC the Secant of the Angle at C; that is, if one Leg be made Radius the other Leg will be a Tangent of its opposite Angle, and the Hypothenuse a Secant of the same Angle.

Thus, as different Sides are made Radius, the other Sides acquire different names, which are either Sines,

Tangents or Secants.

As the Sides and Angles of Triangles bear a certain proportion to each other, two Sides and one Angle, or one Side and to Angles being given, the other Sides or Angles may be found by instituting Proportions, according to the following Rules.

RULE I. To find a Side either of the Sides may be made Radius, then institute the following Proportion:

As the name of the Side given, which will be either

Radius, Sine, Tangent or Secant; Is to the length of the Side given;

So is the name of the Side required, which also will

be either Radius, Sine, Tangent or Secant;

To the length of the Side required.

RULE II. To find an Angle one of the given Sides must be made Radius, then institute the following Proportion;

As the length of the given Side made Radius;

Is to its name, that is Radius;

So is the length of the other given Side;

To its name, which will be either Sine, Tangent or Secant.

Having instituted the Proportion, look the corresponding Logarithms, in the Logarithms for Numbers for the length of the Sides, and in the Table of Artificial Sines, Tangents and Secants, for the Logarithmic Sine, Tangent or Secant.

Having found the Logarithms of the three given Terms, add together the Log. of the second and third Terms, and from their Sum subtract the Log. of the

first Term, the Remainder will be the Log. of the fourth Term, which seek in the Tables and find its corresponding Number or Degrees and Minutes.

See the Introduction to the Table of Logarithms; which should be attentively studied by the Learner be-

fore he proceeds any further.

Note. The Logarithm for Radius is always 10, which is the Logarithmic Sine of 90°, and the Logarithmic Tangent of 45°.

The preceding Propositions and Rules being duly attended to, the solution of the following Cases of Rectangular Trigonometry will be easy.

CASE I.

The Angles and Hypothenuse given to find the Legs.

Fig. 39.

In the Triangle ABC, given the Hypothenuse AC 25 Rods or Chains; the Angle at A 35° 50′, and consequently the Angle at C 54° 50′: to find the Legs.

Making the Hypothenuse Radius, the Proportions

will be:

| To find the Leg. AB. | | To find the Leg BC. | |
|----------------------|----------|----------------------------------|----------|
| As Radius | 10.00000 | As Radius | |
| : Hyp. AC, 25 - | 1.39794 | : Hyp. AC, 25 | 1.39794 |
| :: Sine ACB, 54° 30' | 9.91069 | :: Sine CAB, 35° 30 [*] | 9.76395 |
| A CONTRACTOR OF | - | | |
| | 11.30863 | | 11.16189 |
| | 10.00000 | | 10.00000 |
| | | | |
| Leg. AB, 20.35 - | 1.30863 | :Leg BC, 14.52 - | 1.16189 |
| , | 4 | | - |

Note. When the first Term is Radius, it may be Subtracted by cancelling the first figure of the Sum of the other two Terms.

Making the Leg AB Radius, the Proportions will be:

To find the Leg AB.
As Secant CAB, 35° 30'
: Hyp. AC, 25
:: Radius
: Leg AB, 20.35

To find the Leg BC.
As Secant CAB, 35° 30'
: Hyp. AC, 25
:: Tangent CAB, 35° 30'
: Leg BC, 14.52

Making the Leg BC Radius, the Proportions will be:

To find the Leg AB.
As Secant ABC, 54° 30'

: Hyp. AC, 25

:: Tangent ACB, 54° 30'

: Leg AB, 20.35

To find the Leg BC. As Secant ACB, 54° 30'

: Hyp. AC, 25

:: Radius

:Leg. BC, 14.52

The Logarithms of the four last Proportions being looked out, and added and subtracted according to the Rule, the result will be found to be the same as the two first Proportions.

By Natural Sines.

This Case may be solved by Natural Sines,* ac-

cording to the following Proportions:

As Unity or 1; Is to the length of the hypothenuse; So is the Natural Sine of the smallest Angle; To the length of the shortest Leg. Or, So is the Natural Sine of the largest Angle; To the length of the longest Leg.

Or, which is the same thing, Multiply the Natural Sines of the two Angles by the Hypothenuse, the Pro-

ducts will be the length of the two Legs.

EXAMPLE.

| Nat. Sine of 35° 30′ 0.58070 Hyp. 25 | Nat. Sine of 54° 30' 0.81412 Hyp. 25 |
|--|--------------------------------------|
| 290350 116140 | 407060 162824 |
| 14.51750 | 20.35300 |
| Leg BC 14.52 | Leg AB 20.35 |

^{*}See the Introduction to the Table of Natural Sines.

Note. The third Decimal figure in the first Product being 7, the preceding figure may be called one more than it is, viz. 2. And whenever in any Product, &c. there are more places of Decimals than you wish to work with, if the one at the Right Hand of the last which you wish to retain is more than 5, add a Unit to the last; because a

greater number than 5 is more than half.

As the Table of Artificial or Logarithmic Sines, Tangents and Secants contained in this Book, is calculated only for every 5 Minutes of a Degree, whenever any Question is to be solved where the Minutes cannot be found in that Table; or where the length of the Hypothenuse is such a number as cannot be found in the Table of Logarithms for Numbers, the Question may be solved by Natural Sines, as above taught.

CASE II.

The Angles and one Leg given, to find the Hypothe-

nuse and the other Leg. Fig. 40.

In the Triangle ABC, given the Leg AB 325, the Angle at A 33° 15', and the Angle at C 56° 45'; to find the Hypothenuse and the Leg BC.

Making the given Leg Radius, the Proportions will

be:

| To find the Hypothenuse | | To find the Leg BC. | |
|-------------------------|----------|---------------------|----------|
| As Radius, | 10.00000 | As Radius, | 10.00000 |
| : Leg AB, 325 | 2.51188 | :Leg AB, 325 | 2.51188 |
| :: Sec. CAB, 33° 15' | 10.07765 | :: Tan CAB, 38° 15' | 9.81666 |
| : Hyp. 388.6 | 12.58953 | :Leg BC, 213.1 | 12.32854 |
| 11) p. 000.0 | 12.00000 | . 1108 130, 210.1 | 12.02054 |

Note. Reject the first figure, which is the same as subtracting Radius, and seek the numbers corresponding to the other figures.

Making the Leg BC Radius, the Proportions will be;

To find the Hypothenuse. To find the Leg BC. As Tang. ACB, 56° 45' As Tang. ACB, 56° 45' : Leg AB, 325 : Leg AB, 325

:: Sec. ACB, 56° 45' :: Radius

: Leg BC, 213.1 : Hyp. 388.6

Making the Hypothenuse Radius, the Proportions will be:

To find the Hypothenuse. As Sine BCA, 56° 45'

: Leg AB, 325

:: Radius

: Hyp. 388.6

To find the Leg BC. As Sine BCA, 56° 45'

: Leg AB, 325

:: Sine BAC, 33° 15'

: Leg BC, 213.1

Note. If the Leg BC had been given, instead of the Leg AB, the Proportions would have been the same mutatis mutandis.

By Natural Sines.

To solve this Case by Natural Sines, institute the

following Proportions:

To find the Hypothenuse. As the Natural Sine of the Angle opposite the given Leg; Is to the length of the Leg; So is Unity or 1; To the length of the Hypothenuse.

Or, which is the same thing, Divide the given Leg by the Natural Sine of its opposite Angle, and the

Quotient will be the Hypothenuse.

To find the other Leg. As the Natural Sine of the Angle opposite the given Leg; Is to the length of the given Leg; So is the Natural Sine of the Angle opposite the other Leg; To the length of the other Leg.

EXAMPLE.

Given Leg 325. Nat. Sine of 56° 45', the Angle opposite the given Leg 0.83629. Nat. Sine of 33° 15', the Angle opposite the other Leg 0.54829.

As 0.83629: 325::1:388.6

As 0.83629 : 325 : : 0.54829 :

CASE III.

The Hypothenuse and one Leg given, to find the Angles and the other Leg. Fig. 41.

In the Triangle ABC, given the Hypothenuse AC 50 and the Leg AB 40; to find the Angles and Leg BC.

Making the Hypothenuse Radius, the Proportion to find the Angle ACB will be:

As Hyp. 50 - 1.69897 : Radius - 10.00000 : : Leg AB, 40 - 1.60206 11.60206

: Sine ACB, 53° 10′ 9.90309

The Angle ACB being 53° 10′ the other is consequently 36° 50′.

Making the Leg AB Radius, the Angle BAC may

be found by the following Proportion:

As Leg AB, 40 - 1.60206 : Radius - 10.00000 : Hyp. 50 - 1.69897

11.6989**7** 1.60206

: Sec. BAC, 36° 50′ 10.09691

The Angles being found, the Leg BC may be found by either of the preceding Cases. It is 30.

By Natural Sines.

The Angle opposite the given Leg may be found by the following Proportion:

As the Hypothenuse; Is to Unity or 1; So is the given leg; To the Nat. Sine of its opposite Angle.

Or, which is the same thing, Divide the given Leg by the Hypothenuse, and the Quotient will be the Nat. Sine.

EXAMPLE.

The Leg AB 40 divided by the Hypothenuse 50 quotes 0.80000 which looked in the Table of Nat. Sines, the nearest corresponding number of Degrees and Minutes will be found to be 53° 8′, the Angle ACB.

Note. The reason why the Angle as found by Nat. Sines differs 2 Minutes from the Angle as found by Logaruhms, is that the Table of Logarithmic Sines, &c. contained in this Book, is calculated only for every 5 Minutes. By a Table of Logarithmic Sines, &c. calculated for every Minute, the Angle will be found the same.

By the Square Root.

In this Case the required Leg may be found by the Square Root without Finding the Angles; according to the following Proposition:

In every Right Angled Triangle, the Square of the Hypothenuse is equal to the Sum of the Squares of the

two Legs. Hence,

The Square of the given Leg being subtracted from the Square of the Hypothenuse, the Remainder will be

the Square of the required Leg.

As in the preceding Example; The Square of the Leg AB 40 is 1600; this subtracted from the Square of the Hypothenuse 50 which is 2500, leaves 900, the Square of the Leg BC, the Square Root of which is 30, the length of Leg BC as found by Logarithms.

CASE IV.

The Legs given to find the Angles and Hypothenuse. Fig. 42.

In the Triangle ABC, given the Leg AB 78.7 and the Leg BC 89; to find the Angles and Hypothenuse.

Making the Leg AB Radius, the Proportion to find the Angle BAC will be:

As Leg AB, 78.7 - 1.89597 : Radius - 10.00000 : Leg BC, 89 - 1.94939

11.94939 1.8959**7**

: Tang. BAC, 48° 30′ 10.05342

The Angle ACB is consequently 41° 30'.

Making the Leg BC Radius, the Proportion to find the Angle BCA will be the same as the above, mutatis mutandis.

The Angles being found, the Hypothenuse may be found by Case II. It is nearest 119.

By the Square Root.

In this Case the Hypothenuse may be found by the Square Root, without finding the Angles; according to the following Proposition.

In every Right Angled Triangle, the Sum of the Squares of the two Legs is equal to the Square of the

Hypothenuse.

In the above Example, the Square of AB 78.7 is 6193.69, the Square of BC 89 is 7921; these added make 14114.69 the Square Root of which is nearest 119.

By Natural Sines.

The Hypothenuse being found by the Square Root, the Angles may be found by Nat. Sines, according to the preceding Case.

Hyp. Leg. BC. Nat Sine 119) 89.00000 (74789 83 3....

| 570 476 |
|----------------|
| 940 833 |
| 1070 952 |
| 1180 1071 |
| 109 |

The nearest Degrees and Minutes corresponding to the above Nat. Sine are 48° 24′, for the Angle BAC. The difference between this and the Angle as found by Logarithms is occasioned by dividing by 119, which is not the exact length of the Hypothenuse, it being a Fraction too much.

PART II.

OBLIQUE TRIGONOMETRY.

The solution of the two first Cases of Oblique Trigonometry depends on the following Proposition.

In all Plane Triangles, the Sides are in proportion to each other as the Sines of their opposite Angles. That is, As the Sine of one Angle; Is to its opposite Sides So is the Sine of another Angle; To its opposite Side. Or, As one Side; Is to the Sine of its opposite Angle; So is another Side; To the Sine of its opposite Angle.

Note. When an Angle exceeds 90° make use of its Supplement, which is what it wants of 180°. As the Sine of 90° is the greatest possible Sine, the Sine of any greater number of Degrees will be as much less as that number of Degrees exceeds 90; and will be the same as the Sine of the Supplement of that number of Degrees: Thus the Sine of 100° is the same as the Sine of 80°, and the Sine of 130° the same as the Sine of 50°, &c.

CASE I.

The Angles and one side given, to find the other Sides. PLATE II. Figure 47.

In the Triangle ABC, given the Angle at B 48°, the Angle at C 72°, consequently the Angle at A 60°, and the Side AB 200; to find the Sides AC and BC.

| To find the Side AC. As Sine ACB, 729 - 9.97821 : Side AB, 200 2.30103 :: Sine ABC, 489 - 9.87107 | |
|---|--------------------------|
| 1272.0 9.9782 | |
| : Side AC, 156 2.19399 | : Side BC, 182 - 2.26035 |

By Natural Sines.

As the Nat. Sine of the Angle opposite the given Side; Is to the given Side; So is the Nat. Sine of the Angle opposite either of the required Sides; To that required Side.

Given Side 200; Nat. Sine of 72°, its opposite Angle, 0.95115; Nat. Sine of ABC 48°, 0.74334; Nat. Sine of BAC 60°, 0.86617.

As 0.95115: 200:: 0.74334: 156 As 0.95115: 200:: 0.86617: 182

CASE II.

Two Sides and an Angle opposite to one of them given,

to find the other Angles and Side. Fig. 48.

In the Triangle ABC, given the Side AB 240, the Side BC 200, and the Angle at A 46° 30'; to find the other Angles and the Side AC.

| To find the Angle ACB. | |
|--|------------------------------|
| As Side BC. 200 - 2.30103 | Angle at A - 46° 30' |
| : Sine BAC, 46° 30′ 9.86056 | C - 60 30 |
| :: Side AB, 240 - 2.38021 | |
| * | 107.00 |
| 12.24077 | |
| 2.60103 | Sum of the three Angles 180° |
| The same of the sa | Sum of two 107 |
| : Sine ACB, 60° 30' 9.93974 | |
| | Angle at B 73 |
| The Side AC will be for | ind by Case I. to be near- |

est 253.

Note. If the given Angle be Obtuse the Angle sought will be Acute; but if the given Angle be Acute, and opposite a given lesser Side, then the Angle found by the operation may be either Obtuse or Acute. It ought therefore be mentioned which it is, by the conditions of the question.

By Natural Sines.

As the Side opposite the given Angle; Is to the Nat. Sine of that Angle; So is the other given Side; To the Nat. Sine of its opposite Angle.

One given Side 200; Nat. Sine of 46° 30′, its opposite Angle, 0.72537; the other given side 240.

As 200: 0.72537: : 240: 0.87044=60° 30'.

CASE III.

Two Sides and their contained Angle given, to find the other Angles and Side. Fig. 49.

The solution of this Case depends on the following

Proposition.

In every Plane Triangle, As the Sum of any two Sides; Is to their Difference; So is the Tangent of half the Sum of the two opposite Angles; To the Tangent of half the Difference between them. Add this half difference to half the Sum of the Angles and you will have the greater Angle; and substract the half Difference from the half Sum and you will have the lesser Angle.

| In the Triangle ABC. Side AC 180, and the A | given the | side AF 36° 40' t | 3, 240, the | |
|---|------------|---------------------------|--------------------------|-----|
| other Angles and Side. Side AB AC | 240 180 | AB AC | - 240 - 180 | |
| Sum of the two Sides | 420 | Difference | - 60 | |
| The given Angle B. 180°, leaves 145° 20′ the the half of which is 71° | e Sum of t | 40', subtr he other to | acted from wo Angles; | 100 |
| As the Sum of two S : Their Difference, 60 | | 10 mg 4- | 2.62325 1.77815 | |
| : : Tangent half unknown | wn Ang. 7 | 1° 40' | 10.47969 | |
| | , | | 12 25784 2.62325 | |
| : Tangent half Differen | ce, 23° 20 | • | 9.63459 |) |
| The half sum of the two. The half difference between | | | 71°40' 23 20 | |
| Add, gives the greater A | Ingle ACI | 3 - | 95 00 | |
| Subtract, gives the lesse | r Angle A | BC - | 48 20 | |

The Side BC may be found by CASE I or II.

CASE IV.

The three Sides given to find the Angles. Fig. 50. The solution of this CASE depends on the following PROPOSITION.

In every Plane Triangle, As the longest side; Is to the Sum of the other two Sides; So is the Difference between those two Sides; To the Difference between the Segments of the longest Side, made by a Perpendicular let fall from the Angle opposite that Side.

Half the Difference between these Segments, added to half the Sum of the Segments, that is to half the

length of the longest Side, will give the greatest Segment; and this half Difference subtracted from the half Sum will be the lesser Segment. The Triangle being thus divided becomes two Right Angled Triangles, in which the Hypothenuse and one Leg are given to find the Angles.

In the Triangle ABC, given the Side AB 105, the Side AC 85, and the Side BC 50; to find the Angles.

| Side AC BC | • | 85 . 50 | AC BC | - | • | 85 50 |
|--------------------------------------|----------|------------|--------------|-----------|----------------------------------|----------------|
| Sum of the t | wo Side | s 135 | Dif | ferenc | e | 35 |
| As the lose Sum of the :: Difference | e other | two Sic | les, 135 | | 2.021 2.130 1.544 3.674 | 033 07 — |
| : Difference | betwee | n the S | egments | , 45 | 2.021 | April 100 |
| Half the ! | | | - e Segme | - ents | | 2.5 |
| Add, give | | | | | - | 5.0 |
| Subtract, | gives th | ne lesse | r Segme | ent Bl | 3 | 0.0 |

Thus the Triangle is divided into two Right Angled Triangles, ADC and BDC; in each of which the Hypothenuse and one Leg are given to find the

| # 101. D | |
|--|--|
| To find the Angle DCA. | To find the Angle DCB. |
| As Hyp. AC, 85 - 1.92942 | As Hyp. BC, 50 - 1.69897 |
| : Radius 10.00000 | : Radius 10.00000 |
| : Seg. AD, 75 - 1.87506 | :: Seg. BD, 30 - 1.47712 |
| Annual international designation of the second seco | |
| 11.87506 | 11.47712 |
| 1.92942 | 1.69897 |
| Beauting of the second | / programmy and a second secon |
| : Sine DCA, 61° 55' 9.94564 | : Sine DCB, 36° 504 9.77815 |
| * Principal International Communication | |

The Angle DCA 61° 55′ subtracted from 90° leaves the Angle CAD 28° 5′

The Angle DCB 36° 50' subtracted from 90' leaves

the Angle CBD 53° 10'

The Angle DCA 61° 55′ added to the Angle DCB 36° 50′ gives the Angle ACB 98° 45′

This Case may also be solved according to the fol-

lowing Proposition.

In every plane Triangle, As the Product of any two Sides containing a required Angle; is to the Product of half the Sum of the three Sides, and the Difference between that half Sum and the Side opposite the Angle required; So is the Square of Radius; To the Square of the Co-Sine of half the Angle required.

Those who make themselves well acquainted with Trigonometry will find its application easy to many useful purposes, particularly to the mensuration of Heights and Distances; called Altimetry and Longineerry. These are here omitted because, as this work is designed principally to teach the Art of common Field Surveying, it was thought improper to swell its size, and consequently increase its price, by inserting any thing not particularly connected with that Art.

It is recommended to those who design to be Surveyors to study Triconometry thoroughly; for though a common Field may be measured without an acquaintance with that Science, yet many cases will occur in practice where a knowledge of it will be found very beneficial; particularly in dividing Land, and ascertaining the boundaries of old Surveys. Indeed no one who isi gnorant of Triconometry, can be an accomplished Surveyor.

SURVEYING.

SURVEYING is the Art of measuring, laying out and dividing Land.

PART I.

MEASURING LAND.

THE most common measure for Land is the Acre; which contains 160 Square Rods, Poles or Perches; or 4 Square Roods, each containing 40 Square Rods.

The instrument most in use, for measuring the Sides of Fields, is Gunter's Chain, which is in length 4 Rods or 66 Feet, and is divided into 100 equal parts, called Links, each containing 7 Inches and 92 Hundredths. Consequently, 1 Square Chain contains 16 Square Rods, and 10 Square Chains make 1 Acre.

In small Fields, or where the Land is uneven, as is the case with a great part of the Land in New-England, it is better to use a Chain of only two Rods in length; as the Survey can be more accurately taken.

1 2 37

SECTION I.

PRELIMINARY PROBLEMS.

PROBLEM I. To reduce Two Rod Chains to Four Rod Chains.

RULE. If the number of Two Rod Chains be even take half the number for Four Rod Chains, and annex the Links if any: Thus, 16 Two Rod Chains and 37 Links make 8 Four Rod Chains and 37 Links.

But if the number of Chains be odd, take half the greatest even number for Chains, and for the remaining number add 50 to the Links: Thus, 17 Two Rod Chains and 42 Links make 8 Four Rod Chains and 92 Links.

PROBLEM II. To reduce Two Rod Chains to Rods and Decimal Parts.

RULE. Multiply the Chains by 2 and the Links by 4, which will give Hundredths of a Rod: Thus, 17 Two Rod Chains and 21 Links make 34 Rods and 84 Hundreths; expressed thus 34.84 Rods.

If the Links exceed 25 add 1 to the number of Rods and multiply the excess by 4: Thus, 15 Two Rod

Chains and 38 Links make 31.52 Rods.

PROBLEM III. To reduce Four Rod Chains to Rods

and Decimal parts.

Rule. Multiply the Chains, or Chains and Links, by 4; the Product will be Rods and Hundredths: Thus, 8 Chains and 64 Links make 34.56 Rods.

Note. The reverse of this Rule, that is, dividing by 4 will reduce Rods and Decimals to Chains and Links: Thus, 105.12

Rods make 26 Chains and 28 Links.

PROBLEM IV. To reduce Square Rods to Acres. Rule. Divide the Rods by 160, and the Remainder by 40, if it exceeds that number, for Roods or Quarters of an Acre: Thus, 746 Square Rods make 4 Acres, 2 Roods and 26 Rods.

PROBLEM V. To reduce Square Chains to Acres.
Rule. Divide by 10; or, which is the same thing, cut off the Right hand figure: Thus, 1460 Square Chains make 146 Acres; and 846 Square Chains make 84 Acres and 6 Tenths.

PROBLEM VI. To Reduce Square Links to Acres. Rule. Divide by 100000; or, which is the same thing, cut off the 5 Right hand figures: Thus, 3845120 Square Links make 38 Acres and 45120 Decimals.

Note. When the Area of a Field by which is meant its Superficial Contents, is expressed in Square Chains and Links, the whole may be considered as Square Links, and the number of Acres, contained in the Field, found as above. Then multiply the figures cut off by 4, and again cut off 5 figures, and you have the Roods; multiply the figures last cut off by 40, and again cut off 5 figures, and you have the Rods.

EXAMPLE. How many Acres, Roods and Rods are there in 156 Square Chains and 3274 Square Links?

15)63274 Square Links

2)53096 40

21)23840

Answer. 15 Acres 2 Roods and 21 Rods.

PROBLEMS for finding the Area of Right Lined Figures, and also of Circles.

PROBLEM VII. To find the Area of a Square or Parallelogram.

RULE. Multiply the length into the breadth; the Product will be the Area.

PROBLEM VIII. To find the Area of a Rhombus or Rhomboides.

Rule. Drop a Perpendicular from one of the Angles to its opposite Side, and multiply that side into the Perpendicular; the Product will be the Area.

PROBLEM, IX. To find the Area of a Triangle.

RULE 1. Drop a Perpendicular from one of the Angles to its opposite Side, which may be called the Base; then multiply the Base by half the Perpendicular, or the Perpendicular by half the Base; the Product will be the Area. Or, multiply the whole Base by the whole Perpendicular, and half the Product will be the Area.

RULE 2. If it be a Right Angled Triangle, multiply one of the Legs into half of the other; the Product will be the Area. Or, multiply the two Legs into each other, and half the Product will be the Area.

RULE 3. When the three Sides of a Triangle are known, the Area may be found Arithmetically, as fol-

lows:

Add together the three Sides; from half their Sum subtract each side, noting down the Remainders; multiply the half Sum by one of those Remainders, and that Product by another Remainder, and that Product by the other Remainder; the Square Root of the last Product will be the Area.

EXAMPLE. Suppose a Triangle whose three Sides are 24, 20 and 18 Chains. Demanded the Area.

24+20+18=62, the Sum of the three Sides, the half of which is 31. From 31 subtract 24, 20 and 18;

the three Remainders will be 7, 11 and 13.

 $31\times7=217$; $217\times11=2387$; $2387\times18=31031$, the Square Root of which is 176.1 or 17 Acres-2 Roods and 17 Rods.

By Logarithms.

As the Addition of Logarithms is the same as the Multiplication of their corresponding Numbers; and as the Number answering to the one half of a Logarithm will be the Square Root of the Number corresponding to that Logarithm; it follows, That if the Logarithm of the half Sum of the three Sides and the Logarithms of the three Remainders be added together, the Number corresponding to one half the Sum of those Logarithms will be the Area of the Triangle.

| The half Sum, 31 The first Remainder, 7 The second Remainder, 11 The third Remainder, 13 | 1.49136 0.84510 1.04139 1.11394 |
|---|--|
| The Square of the Arca, 31000 | 4.49179 |
| Area 176 Square Chains - | 2.24589 |

Rule 4. When two Sides of a Triangle and their contained Angle, that is, the Angle made by those Sides, are given, the Area may be found as follows:

Add together the Logarithms of the two Sides and the Logarithmic Sine of the Angle; from their sum subtract the Logarithm of Radius, the Remainder will be the Logarithm of double the Area.

Example. Suppose a Triangle one of whose Sides is 105 Rods and another 85 and the Angle contained between them 28° 5'. Demanded the Area.

| | CL CK DAS | C |
|-------------------------|-----------|--|
| One Side, 105 | | 2.02119 |
| The other Side, 85 | - | 1.92942 |
| Sine Angle, 28° 5′ - | •• | 9.67280 |
| | | , |
| | | 13.62341 |
| Subtract Radius | - | - 10.00000 |
| 6 1 | | Opposite the state of the state |
| Double Area, 4200 Rods. | - | 3.62341 |
| | | |

2100 Rods. Answer.

Note. Radius may be subtracted by cancelling the Lest hand figure of the Index, or subtracting 10, without the trouble of setting down the Cyphers.

By Natural Sines.

Multiply the two given Sides into each other; and that Product by the Natural Sine of the given Angle; the last Product will be double the Area of the Triangle.

Nat. Sine of the Angle 28° 5'. 0.47076.

 $105 \times 85 = 8925$, and $8925 \times 0.47076 = 4201$ the dou-

ble Area of the Triangle.

PROBLEM X. To find the Area of a Trapezoid.

Rule. Multiply half the Sum of the two parallel Sides by the perpendicular distance between them, or the sum of the two parallel Sides by half the perpendicular distance; the Product will be the Area.

PROBLEM XI. To find the Area of a Trapezium,

or irregular Four Sided Figure.

Rule. Draw a Diagonal between two opposite Angles, which will divide the Trapezium into two

Triangles. Find the Area of each Triangle and add them together. Or, multiply the Diagonal by half the Sum of the two Perpendiculars let fall upon it, or the Sum of the two Perpendiculars by half the Diagonal; the Product will be the Area.

Note. Where the length of the four Sides and of the Diagonal is known, the Area of the two Triangles, into which the Trapezium is divided, may be calculated Arithmetically, according to Prob. IX. Rule 3.

PROBLEM XII. To find the Area of a figure containing more than Four Sides.

Rule. Divide the Figure into Triangles and Trapezia, by prawing as many Diagonals as are necessary; which Diagonals must be so drawn as not to intersect each other: Then find the Area of each of the several Triangles or Trapezia, and add them together; the Sum will be the Area of the whole Figure.

Note. A little practice will suggest the most convenient way of drawing the Diagonals; but whichever way they are drawn, provided they do not intersect each other, the whole Arez will be found the same.

PROBLEM XIII. Respecting Circles.

RULE 1. If the Diameter be given, the Circumference may be found by one of the following Proportions: As 7 is to 22; or more exactly, as 113 is to 355; or in Decimals, as 1 is to 3.14159; So is the Diameter to the Circumference.

RULE 2. If the Circumference be given, the Diameter may be found by one of the following Proportions: As 22 is to 7; or as 355 is to 113; or as 1 is to 0.31831; so is the Circumference to the Diameter.

RULE 3. The Diameter and Circumference being known, multiply half the one into half the other, and the Product will be the Area.

Rule 4. From the Diameter only to find the Area: Multiply the Square of the Diameter by 0.7854, and the Product will be the Area.

RULE 5. From the Circumference only to find the Area; Multiply the Square of the Circumference by 0.07958, and the Product will be the Area.

RULE 6. The Area being given to find the Diameter: Divide the Area by 0.7854, and the Quotient will be the Square of the Diameter; from this extract the Square Root, and you will have the Diameter.

RULE 7. The Area being given to find the Circumference: Divide the Area by 0.07958, and the Quotient will be the Square of the Circumference: from this extract the Square Root, and you will have the Circumference.

SECTION II.

The following Cases teach the most usual methods of taking the Survey of Fields; also how to protract or draw a Plot of them, and to calculate their Area.

Note. The FIELD Book is a Register containing the length of the Sides of a Field, as found by measuring them with a Chain; also the Bearings or Courses of the Sides, or the Quantity of the several Angles, as found by a Compass, or other instrument for that purpose; together with such remarks as the Surveyor thinks proper to make in the Field.

CASE I.

To survey a Triangular Field.

Measure the Sides of the Field with a Chain, and enter their several lengths in a Field Book; protract the Field on Paper, and then find the Area by Prob. IX. Rule 1. Or, without plotting the Field, calculate the Area by Prob. IX. Rule 3.

FIELD BOOK. See PLATE II. Fig. 46.

| , | | CI | nains |
|------------|---------|------|-------|
| AB | • | | 20 |
| BC | - | - | 24 |
| CA | | - | 18 |
| To f | ind the | Area | . 1 |
| | | | L. |
| Base BC | - 1 | - 24 | 00. |
| Half Perp. | AD | - 7 | .34 |
| | | | |

9600 7200 16800

Acres 17)61600

4

Roods 2)46400

40

Rods 18)56000

Acres Roods Rods

Area 17 — 2 — 18.56

Note. When there are Cyphers at the Right Hand of the Links, they may be rejected; remembering to cut off a proper number of figures according to Decimal Rules.

Observe, That in measuring with a Chain, slant or inclined Surfaces, as the Sides of Hills, should be measured horizontally, and not on the Plane or Surface of the Hill; otherwise a Survey cannot be accurately taken. To effect this, the lower end of the Chain must be raised from the ground, so as to have the whole in a horizontal Line; and the end thus raised must be directly over the Point where the Chain begins or ends, according as you are ascending or descending a Hill; which Point may be ascertained by a Plummet and Line.

CASE II.

To survey a Field in the form of a Trapezium.

Measure the several sides, and a Diagonal between two opposite Angles; protract the Field, and find the Area by Problem XI. Or, without protracting the Field, calculate the Area according to the Note at the

end of that PROBLEM.

FIELD BOOK. See PLATE II. Fig. 51.

AB - - 27.50 BC - - 11.70 CD - 21.50 DA - 14.70 Diagonal AC - 28.

To protract this Trapezium.

Draw the Side AB the given length; with the Diagonal AC 28 and the Side BC 11.70 describe cross Arches as at C, from A and B as Centres; and the Point of intersection will represent that Corner of the Field: Then with the Side CD 21.50 and the Side AD 14.70 describe cross Arches as at D, from A and C as Centres; and the Point of intersection will represent that Corner of the Field.

| To find | the . | Area. | |
|-------------------|-------|-------|--------|
| Perpendicular B a | A | | 11.34 |
| — D m | 628 | 100 | 11.10 |
| | | | 22.44 |
| Half Diagonal AC | • | • | 14.00 |
| | | | 897600 |
| and the same | | ť | 2244 |
| | Bu. | Acres | 31)416 |
| | | | 4 |
| | | Rood | 1)664 |
| | | | 40 |
| | | Rods | 26)560 |
| | | | |

Acres Rood Rods
Area 31 — 1 — 26.56

Note. The Perpendiculars need not be actually drawn; their length may be obtained as follows: From the Angle opposite the Diagonal open the Dividers so as when one Foot is in the angular Point, as at B, the other, being moved backwards and forwards, may just touch the Diagonal at a, and neither go the least above or below it; that distance in the Dividers being measured on the Scale will give the length of the Perpendicular.

CASE III.

To survey a Field which has more than four Sides,

by the Chain only.

Measure the several Sides, and from some one of the Angles, from which the others may be seen, measure Diagonals to them; draw a Plot of the Field, and find the Area by PROBLEM XII.

FIELD BOOK. See Plate II. Fig. 52.

| ė. | | | Ch. L. | 1 4 6 6 |
|----|-----|------|--------|------------|
| AB | | - / | 30.60 | Diagonals. |
| BC | - 1 | 1/41 | 20.40 | Ch. L. |
| CD | - | - | 22.40 | AC 45. |
| DE | - | | 16.20 | AD 35. |
| EF | - | - " | 13.50 | AE 24.20 |
| FA | 9 | - | 28. | |

To Protract this Field.

Draw the Side AB, making it the given length 30. 60; with the Diagonal AC 45 and the Side BC 20.40 describe cross Arches as at C, from the Points A and B as Centres; and the Point of intersection will represent that Corner of the Field; draw the Side BC and the dotted Diagonal AC: With the Diagonal AD 35 and the Side CD 22.40 describe cross Arches as at D, from the Points A and C; and draw the Side CD and the dotted Diagonal AD. Proceed in this manner till all the Sides and Diagonals are drawn.

To find the Area.

The Field being plotted may be divided into one Trapezium and two Triangles; the Area of which is calculated as follows.

| Ourockining and no | | | |
|--------------------|------------------------|------------------|--------------|
| The Trapezium | ABCD. | The Triangle ADE | E |
| Perpend. B a | - 1.1.68 | Half Perp. E m - | 4.90 |
| | - 17.10 | Diag. AD. | - 35. |
| Half Diag. AC | 28.78 22.50 | | 2450 1470 |
| | 143900 5756 5756 | Square Chains - | 171.50 |
| Square Chains - | 647.5500 | | |

| The Triangle AFE Perpend. E n - 11.65 Half Side AF 14 | Trap. ABCD - 647.55 Triangle ADE - 171.50 Triangle AFE - 163.10 |
|---|---|
| 4660 1165 | Acres 98)215 |
| Square Chains - 163.10 | Roods .860 |
| Acres Rood Rods Area 98 — 0 — 34.4 | Rods 34)400 |

REMARKS.

As each of the Sides of the several Triangles into which the preceding Plot of a Field is divided, is known from the field Book, the Area of the Field may be calculated Arithmetically, by finding the Area of each Triangle, according to PROB. IX. Rule 3; and then adding the whole together. This method, though it may require more time, is preferable to the other, because more accurate. Indeed it is always better to calculate the Area of a Field Arithmetically than Geometrically; for in the former no two persons can differ in their calculations; whereas according to the latter, which is the common method of casting the Contents of a Field, it is hardly to be expected that any two persons will perfectly agree. The inaccuracy of Scales, and the difficulty of determining with precision the length of Sides and Perpendiculars, with a Scale and Dividers, render it almost if not quite impossible to obtain the exact Area of a Field, in the method commonly practised; even if the Surveyor has measured it accurately in the first place.

Other methods of taking the Survey of a Field, by the Chain only are mentioned in some Treatises on this subject, but they are rather curious than useful; and it is much better to ascertain the Angles by an accurate Compass, or some Instrument designed purposely for

taking Angles.

CASE IV.

To survey a Field with a Chain and Compass.

Measure the length of the Sides with a Chain, and take their Bearing or Course with a Compass;* enter these in a Field Book; plot the Field on Paper, and calculate the Area by the directions already given.

To protract or draw a Map of a Field.

Draw a Line to represent a Meridian or North and South Line, from which lay off the Bearing or Course of the first Side of a Field, with a Protractor or from a Line of Chords; and from a Scale of equal Parts measure the length of the Side and draw a Line to represent it. At the end of this Line draw a Line parallel to the Meridian Line, and then lay off the second Side of the Field as before taught: Proceed in the same manner to draw parallel Lines and lay off the several Sides till the whole is protracted.

In protracting a Field, let the top of the Paper be considered as North; the Bottom, South; the Right hand, East; and the Left hand, West: Lay the Course to the Right or Left of the Meridian Line, according as it is East or West; and from the upper or lower part of the Line, according as it is North or South.

In all protractions, if the end of the last distance falls exactly on the Point from which you began, the Course also being right, the Field work and protraction are truly taken and performed; if not, an error must have been committed in one of them: In such cases make a second protraction; if this agrees with the former, it is to be presumed the fault is in the Field work; a re-survey must then be taken.

EXAMPLE I.

FIELD BOOK. See PLATE II. Fig. 53.

* A Compass may be so constructed with two Indexes, one moveable and the other fixed, as to ascertain the Angle made by two Sides, without reference to the Bearing of those Sides. Such a Compass would be particularly useful in surveying Land where there are mineral substances which have an influence upon the Compass Needle, attracting it one way or the other; and thus rendering it impossible to take a Course by it with precision.

Ch. L. AB. N. 7° 0' W. 28.20 BC. N. 74 0 E. 39.50 E. S. 9 0 CD. W. DE. N. 63 20 14.55 S. 74 0 W. 28.60 Acres Rood Rods Area 117 — 1 — 6

REMARKS.

The Sides of the several Triangles into which the Plot of a Field is divided may be found by Trigonometry; and then the Area of each Triangle may be calculated according to Prob. IX. Rule 3. The Sum of the Areas of the several Triangles will be the Area of the whole Field. This method may require more time but it is perfectly accurate, since no dependance is placed on the uncertain measurement of Scale and Dividers.

In the preceding Example, suppose the Field divided into three Triangles. See Fig. 53. In the Triangle EAB, the Sides EA and AB are known from the FIELD Book, and their contained Angle is known from the Bearing of the Sides. The other Angles and the Side EB may be found by Oblique Trigonometry, CASE III; and then there will be the three Sides to find the Area. In the Triangle EBC, the Side BC is known from the FIELD BOOK, and the Side EB is found as above mentioned; the Angle EBA is also found as above; this subtracted from the angle ABC, which may be found from the Bearing of the Sides AB and BC, will leave the Angle EBC; there will then be two Sides and their contained Angle to find the third Side; and this being found there will be the three Sides to find the Area. In the Triangle EDC, the Sides DE and DC are known from the FIELD Book, and their contained Angle is known from the Bearing of the Sides. The Side EC and the Area may be found as above.

It is recommended to the Learner to make these calculations, as it will improve him in the knowledge of Trigonometry.

Note. Two Sides and their contained Angle being given the Area may be found by Prob. IX. Rule 4.

Another Method of protracting Fields.

Without drawing parallel Lines at the end of each Side, a Field may be protracted by the Angles made by the several Sides; and the Angle made between any two Sides may be found by the following Rules.

RULE 1. If the Course or Bearing of one of the Sides is Northerly and the other Southerly, one Easterly and the other Westerly subtract the less Course from the greater; the Remainder will be the Angle between them.

RULE 2. If one is Northerly and the other Southerly, and both Easterly or Westerly, add both Courses together; the Sum will be the Angle between them.

RULE 3. If both are Northerly or Southerly, and one Easterly and the other Westerly, subtract the Sum of both from 180°; the Remainder will be the Angle between them.

RULE 4. If both are Northerly or Southerly, and both Easterly or Westerly, add 90°, the less Course and the Complement of the greater together; the Sum

will be the Angle between them.

To protract a Field according to the preceding Rules is preferable to the method of doing it by parallel Lines, though it may not be so easy to the Learner at first. It is difficult to draw parallel Lines with perfect accuracy, particularly without a parallel Rule; and a small deviation from a true Line may make considerable difference in the Plot of a Field.

EXAMPLE II. FIELD BOOK. See PLATE III. Fig. 58. Ch. L. AB. 16° 30′ E. 22. N. BC. E. 19.60 N. 82 0 E. S. 17 0 24 DE. S. 37 0 W. 22. EA. N. 49 25.20 Area 85 Acres.

To draw a Plot of this Field according to the precede

ing Rules.

Having drawn the Side AB, according to the directions before given for laying off the first Course and Distance, compare the first and second Courses together, and they will be found to be both Northerly and both Easterly; consequently the Angle between them is found by Rule 4. as follows: 90° added to 16° 30' the less Course and 8° the Complement of the greater, the Sum is 114° 30' for the Angle at B. Compare the second and third Courses, and they will be found to be one Northerly and one Southerly and both Easterly; consequently, according to Rule 2. 82° the second Course added to 17° the third Course, the Sum 199° is the Angle at C. The third and fourth Courses are both Southerly and one Easterly and the other Westerly. The Angle between them at D is 126°; for 17° the third Course added to 37° the fourth Course is 54° which subtracted from 180° leaves 126°, according to Rule 3. The fourth and fifth Courses are one Southerly and the other Northerly and both Westerly. According to Rule 2. 37° the fourth Course added to 49° the fifth Course, the Sum 86° is the Angle at E.

A little practice will render this mode of protracting a Field familiar and easy; and an attention to the Courses will show in what direction the Angle is to be

made.

EXAMPLE III. FIELD BOOK. See PLATE IV. Fig. 66. Ch. L. AB. N. 56° 15' E. 21.60

E. AB. N. 15 21.60 N. 26 BC. 30 E. 13.44 CD. S. E. 71 30 18.96 DE. S. E. 26 30 13.44 W. EF. S. 71 18.96 30 FG. S. E. 4.5 8.47 0 S. GH. 63 30 E. 13.44 HI. N. 45 E. 0 8.47 IK. S. E. 26 30 13.44 KL. S. W. 45 -(.) 8.47

37

LM. S. 63 30 W. 13.44
MN. N. 76 0 W. 24.73
NA. N. 36 45 W. 30.
Acres Rood Rods

Area 167 — 1 — 30

The above Field may be protracted, and its Area calculated according to the directions given in the preceding Examples.

ARULE to determine whether the Courses in any Sur-

vey have been accurately taken.

By the Rules for protracting a Field, Page 48, find the Quantity of the several Angles, and add the whole together; to their Sum add 360°; divide this Sum by 180°; and, if the Survey is right, the Quotient will equal the number of Angles contained in the Field. Thus, in the preceding Example, the Sum of all the Angles is 1980°; to this add 360° and it makes 2340°; this Sum being divided by 180° the Quotient will be 13, which is the number of Angles in the Field. See the Figure.

When the Angle is without the Field, as at B, F, G and H, subtract the Quantity of the Angle, as found by the preceding directions, from 360 and make use of the Remainder in adding the several Angles. Thus the Angle at B 150° 15' must be subtracted from 360°, and the Remainder 209° 45' considered as the real Quantity of that Angle. If there is an error, the Field must be re-surveyed, and the error corrected, else the

true Area cannot be ascertained.

Note. Directions will be given in Section III. for determining whether the Sides have been accurately measured.

Demonstration of the preceding Rule.

Suppose a Plot of a Field, as ABCD, &c. PLATE II. Ing. 54. From some Point within the Field, as at a, draw Lines to the several Angles; and it is evident the whole will be divided into as many. Triangles as there are Sides to the Field, that is 7. How, as the three Angles of every Triangle amount 180°, the Sum of the Angles of all these Triangles will be 7 times 180°, that is 1260°. The Sum of the Angles at the Centre is 360°, because the Arches which measure those Angles form a Circle. Therefore, 360° the Sum of those central Angles, subtracted from 1260° will leave the Sum of all the other Angles; which are the Angles made by the several Sides of the Field. The Angles of this Field will be found to contain 900°; if to this you add 360° and divide the Sum, viz. 1260° by 180° the Quotient will be 7, the number of the Sides or Angles of the Field.

Several Field Books to exercise the Learner in plotting Fields and calculating their Area.

| | No. I. | | | | | | |
|------|--------|------|------|----|-------|--|--|
| | | 7.4 | | 7 | Rods. | | |
| 1. | N. | 15° | 0' | E. | 320 | | |
| 2. | N. | .37 | 30 | E. | 160 | | |
| 3. | Eas | ť | | | 120 | | |
| 4. | S. | 11 | 0 | E. | 200 | | |
| 5. | Sou | th | | | 216 | | |
| 6. | We | st | | | 160 | | |
| 7. | S. | 36 | 30 | W. | 160 | | |
| 8. | N. | 38 | 15 | W. | 136 | | |
| | Acr | es l | Rood | s | Rods | | |
| Irea | 74 | 4 | - 3 | | 28 | | |

No. II.

| | | | | | Ch. L. | |
|------|------|------|-----|---------|--------|--|
| 1. | N. | 75° | 01 | E. | 13.70 | |
| 2. | N. | 20 | 30 | E. | 10 30 | |
| 3. | East | | | | 16.20 | |
| 4. | S. | 33 \ | 30 | W. | 35 30 | |
| 5. | S. | 76 | 0 | W. | 16. | |
| 6. | Nor | th | | | 9. | |
| 7. | S. | 84 | 0 | W. | 11.60 | |
| 8. | N. | 53 | 15 | W. | 11.60 | |
| 9. | N. | 36 | 45 | E. | 19.20 | |
| 10. | N. | 22 | 30 | E. | 14. | |
| 11. | S. | 76 | 45 | E. | 12. | |
| 12. | S. | 15 | 0 | W. | 10.85 | |
| 13. | S. | 16 | 45 | W. | 10.12 | |
| | Acr | es l | Roo | ds | Rods | |
| Irea | 110 | - | 2 | e-redit | 23 | |
| | | | | | | |

No. III.

| | | | . 7. | 0. 17 | ≥ • |
|---|-----|-----|------|-------|------------|
| | | | | 1,1 | Rods. |
| | 1. | S. | 65° | 40' | W. 49.7 |
| | 2. | S. | 67 | 15 | W. 34.5 |
| | 3. | S. | 54 | 0 | W. 17.9 |
| | 4. | S. | 20 | 0 | W. 5.8 |
| | 5. | S. | 7 | 30 | E. 29.4 |
| | 6 | N. | 83 | 0 | E. 107.4 |
| | 7. | N. | 5 | 50 | W. 22. |
| | 8. | N. | 18 | 30 | W. 46. |
| | | Ac | | | d Rods |
| A | rea | . 3 | 4 - | 1 | 19 |
| | | | | | |

No. IV.

| | | - A 1 | 10. 1 | | |
|------|-----|-------|-------|------------|--------|
| | | | | | Rods |
| 1. | N. | 430 | 0, | W. | 12.44 |
| 2. | N. | 64 | 0 | W. | 8. |
| 3. | N. | 52 | Ő | W. | 14.60 |
| 4. | N. | 37 | 5 | W. | 51.36 |
| 5. | N. | 15 | 30 | W. | 21.76 |
| 6. | N. | 20 | 40 | W. | 44.60 |
| 7. | N. | 88 | 20 | E. | 167.60 |
| 8. | S. | 34 | 40 | E. | 71.20 |
| 9. | S. | 75 | 0 | W. | 69.72 |
| 10. | S. | 55 | 0 | W_{τ} | 64.60 |
| 11. | S. | 25 | 0 | W. | 18.12 |
| | Acr | es | Roc | ods | Rods |
| Area | 97 | - | - 2 | , , | . 29 |
| | | | | | |

| No. V. | | | | | |
|-----------------|----------------------------------|--|--|--|--|
| | F | Rods. | | | |
| • 50' | W. | 34.6 | | | |
| 20 | E. | 93.6 | | | |
| 0 | W. | 34.9 | | | |
| 55 | E. | 40.1 | | | |
| 20 | W. | 35.5 | | | |
| 40 | W. | 60. | | | |
| , O | W . | 30.6 | | | |
| 20 | W. | 1.2 | | | |
| 30 | W. | 10.4 | | | |
| 55 | W. | 15.2 | | | |
| Acres Rood Rods | | | | | |
| _ 1 | | 34 | | | |
| | 50' 20 0 55 20 40 0 20 30 55 Roo | 50' W. 20 E. 0 W. 55 E. 20 W. 40 W. 0 W. 20 W. 30 W. 55 W. | | | |

No. VI.

| | | | - | | Rods. |
|------|-----|------|-----|-----|-------|
| P. | S. | 340 | G' | Ε. | 42.8 |
| 2. | S. | 29 | 0 | E. | 69.4 |
| 3. | S. | 64 | 50 | W. | 53. |
| 4. | S. | 25 | 0 | E. | 4. |
| 5. | S. | 66 | 30 | W. | 39. |
| 6. | N. | 25 | 0 | W. | 4. |
| 7. | S. | 64 | 45 | W. | 32.2 |
| 8. | N. | 3.0 | 30 | W. | 1.8.3 |
| 9. | N. | 56 | 30 | E. | 34.5 |
| 10. | N. | 64 | 0. | E. | 12.5 |
| 11. | N. | 49 | 0 | E. | 14. |
| 12. | N. | 26 | 10 | W. | 19.3 |
| 13. | N. | 21 | 0 | W. | 18.3 |
| 14. | N. | 44 | 10 | W. | 18. |
| 15. | N. | 64 | 40 | E. | 30.5 |
| 16. | N. | 18 | 30 | W. | 39. |
| 17. | N. | 86 | 5 | E. | 26.7 |
| | Acr | es | Roo | d I | Rods |
| Area | 48 | 3. — | - 1 | | 1,2 |
| | | | | | |

No. VII.

| | | | | (| Jh. L. |
|-----|----|-----|-----|----|--------|
| 1. | N. | 00. | 45' | w. | 9. |
| 2. | N. | 19 | 30 | W. | 5.35 |
| 3. | N. | 23 | 0 | W. | 4.09 |
| 4. | N. | 41 | 35 | W. | 6,15 |
| 5. | N. | 3 | 0 | W. | \$6.75 |
| 6. | S. | 86 | 50 | W. | 43.33 |
| 7. | N. | 2 | 15 | W. | 17.65 |
| 8. | N. | 85 | 45 | E. | 12.56 |
| 9. | S. | 2 | 10 | E. | 8. |
| 10. | N. | 86 | 45 | E. | 7.38 |
| HI. | S. | 3 | 15 | E: | 13.20 |

| 12. | N. | 87 | O. | E. | 29.92 | |
|--------------------|----|-----|----|----|-------|--|
| 13. | N. | 49 | 20 | E. | 4.04 | |
| 19. | No | rth | | | 2.23 | |
| 15. | N. | 50 | 35 | E. | 6.50: | |
| 16. | S. | 22 | 50 | E. | 17.94 | |
| 17. | S. | 34 | 0 | W. | 3.50 | |
| 18. | S. | 41 | 0 | W. | 3. | |
| 19. | S. | 22 | 50 | W. | 9.25 | |
| 20. | S. | 3 | 40 | E. | 2.64 | |
| 21. | S. | 86 | 0 | W. | 2.50 | |
| 22. | S. | 0 | 25 | W. | 14.50 | |
| 23. | S. | 2 | 0 | W. | 5.38 | |
| 24. | S. | 10 | 0 | E | 11.75 | |
| 25. | S. | 86 | 0 | W. | 34.60 | |
| Acres Roods Rods | | | | | | |
| Area 268, — 3. — 7 | | | | | | |

| No. | V | 11 | I. |
|-----|---|----|----|
| | | | |

| No. VIII. | | | | | |
|-----------|----|------|------------|---------------|-------|
| | | | | | Rods. |
| 1. | S. | 60 | 30' | E. | 19.1 |
| 2. | S. | 63 | 30 | E. | 14.36 |
| 3. | S. | 67 | 0. | E. | 10.68 |
| 4. | N. | 88 | O. | E. | 13.3 |
| 5. | S. | 31 | 30 | w. | 32.44 |
| 6. | S. | 31 | 55 | W. | 96.5 |
| 7. | S. | . 33 | 25 | W. | 34.9 |
| 8. | S. | 20 | 45 | E. | 3.68 |
| 9. | S. | 16 * | 1.5 | $\mathbf{W}.$ | 64. |
| 10. | N. | 52 | 30 | W. | 12.8 |
| 11. | S. | 45 | 0 | W. | 18.24 |
| 12. | S. | 69 | 0 | W. | 21.4 |
| 13. | S. | 12 | 40 | W. | 9.4 |
| 14. | S. | 84 | 20 | W. | 9,5 |
| 15. | N. | 22 | 15 | W. | 24. |
| 16. | No | rth | | | 9.8 |
| 17. | N. | 29 | 15 | W. | 30.6 |
| 18. | N. | 44 | 25 | W. | 21.8 |
| 19. | N. | 61 | 30 | W. | 23.1 |
| 20. | N. | 41 | 0 | W. | 10.8 |
| 21. | N. | 36 | . 0 | E. | 41.56 |
| 22. | S. | 68 | 0 | E. | 80.6 |
| 23. | N. | 44 | 30 | E. | 20.4 |
| 24. | N. | 2 | 30 | W. | 41. |
| 25. | N. | 14 | 45 | W. | 62.32 |
| 26. | | 16 | 0 | W. | 14.8 |
| 27. | N. | 1 | 45 | W. | 14.8 |
| 28. | N. | 82 | 30 | E. | 99. |
| | | res | Roc | od | Rods. |
| Area | 1 | 35 - | → 1 | Name of | 1,5. |
| | | | | | |

CASE V.

To survey a Field from one Station, at any place within the Field, from which the several Angles may be seen.

Take the Bearing of the Angles, and measure their

Distance from the Station.

FIELD BOOK. See PLATE III. Fig. 61.

From Station to A. N. 20° W. 8.70

B. N. 60 E. 10. C. N. 87 E. 11.40

D. S. 15 E. 10.50 E. S. 60 W. 12.

F. N. 65 W. 8.78

To protract this Field.

Draw a Meridian line as N. S. From some point in that Line as a Centre lay off the Bearing and Distance to the several Angles, and draw Lines from one Angle to another, as AB, BC, CD, &c.

To find the Area.

The Area may be calculated according to PROB. XII. by measuring Diagonals and Perpendiculars; or

more accurately according to PROB. IX. Rule 4.

As the Bearing and Distance of the Lines from the Station to the several Angles are known, two Sides and their contained Angle are given in each of the Triangles into which the Plot is divided; the Area may, therefore, be readily calculated by the Rule above referred to.

Note. As in the operation, the Logarithm of Radius is to be subtracted from the Sum of the other Logarithms, it may be done by rejecting the Left hand figure, without the trouble of putting down the Cyphers and subtracting.

| Triangle aAB. | | Triangle aCD. | a |
|------------------|---------|---------------------|-----------------------------|
| aA, 8.70 | 0.93952 | aC, 11.40 | 1.05690 |
| aB, 10 | 1.00000 | aD, 10.50 | 1.02119 |
| Sine AaB, 80° - | 9.99335 | Sine CaD, 78° - | 9.99040 |
| | | | |
| Doub. Area, 85.7 | 1.93287 | Doub. Area, 117 | 2.06849 |
| | - | Carrier and Control | |
| Triangle aBC. | | Triangle aDE. | |
| aB, 10 | 1.00000 | aD, 10.50 - | 1.02119 |
| aC, 11.40 | 1.05690 | aE, 12 | 1.07918 |
| Sine BaC, 27° - | 9.65705 | Sine DaE, 75° - | 9.98494 |
| | | | |
| Doub. Area, 51.8 | 1.71395 | Doub. Area, 122 | 2.08531 |
| | | | Second Second Second Second |

| | • | | |
|---|--|--|---------------------------------------|
| Triangle aEF. aE, 12 aF, 8.78 Sine EaF, 55° - | I.07918 0.94349 9:91336 | Triangle aFA. aF, 8.78 aA, 870 - Sine FaA, 45° - | 0.94349 0.93 952 9.84948 |
| Doub. Area, 86.3 | 1.93603 | Doub. Area, 54 | 1.73249 |
| al al | AB - BC - CD - 1 DE - 1 EF - FA - | 51.8 17. 22., 86.3 | |
| Double Ar | - | 16.8 Square Chai | ns. |

Area - 25)84

3)36

14)40

Acres Roods Rods

Area 25 — 3 — 14.4

CASE VI.

To survey a Field from some one of the Angles, from

which the others may be seen.

From the Stationary Angle take the Bearing and Distance to each of the other Angles, with a Compass and Chain.

FIELD BOOK. See PLATE III. Fig. 59.

FG. N. 70° W. 14.60 FA. N. 50 W. 18.20 FB. N. 30 W. 16.80 FC. N. 10 W. 21.20 FD. N. 7 E. 16.95

FE. N. 30 E. 8.50

To draw a Plot of this Field.

Draw a Meridian Line to pass through the stationary Angle, as at F. From the Point F lay off the Bear-

ing and Distance to the several Angles, and connect them by Lines, as FG, FA, FB, &c.

The Area may be calculated as taught in the preced-

ing CASE.

CASE VII.

To survey a Field from two Stations within the Field, provided the several Angles can be seen from each Station.

Find the Bearing from each Station to the respective Angles; and also the Bearing and Distance from one Station to the other.

| FIELD BOOK. Se | ee PLATE III. Fig. 62. |
|---------------------|------------------------|
| First Station. | Second Station. |
| AC. N. 38° 30′ E. | BC. S. 82° 0′ E. |
| AD. S. 69 0 E. | BD. S. 17 0 E. |
| AE. S. 59 0 W. | BE. S. 28 0 W. |
| AF. N. 63 0 W. | BF. S. 49 0 W. |
| AG. N. 21 · 0 W. | BG. N. 76 0 W. |
| AH. North. | BH. N. 24 0 W. |
| Stationary Line AB. | N. 14° E. 20 Chains. |

To protract this Field.

At the first Station A draw a Meridian Line and lay off the Bearings to the respective Angles; draw the stationary Line AB, according to the Bearing and Distance; at B draw a Meridian Line parallel to the other, and lay off the Bearings to the Angles, as taken from this Station; from each Station draw Lines through the Degree which shows the Bearing of each Angle, as marked by the Protractor or Line of Chords, and the Points where those Lines intersect each other will be the Angles of the Field. Connect those angular Points together by Lines, and those Lines will represent the several Sides of the Field.

CASE VIII.

To survey an inaccessible Field.

Fix upon two Stations, at a convenient distance from the Field; from each of which the several Angles may

be seen; from each Station take the Bearing of the Angles; and take the Bearing and Distance from one Station to the other.

FIELD BOOK. See PLATE IV. Fig. 67.

Second Station. First Station. AE. N. 9° 15' E. BE. N. 50° O' W. AF. N. 16 N. 29 15 W. 0 E. BD. N. 24 0 W. AG. N. 14 30 E. AD. N. 39 0 E. BG. N. 21 30. W. AH. N. 40 O E. BH. N. 5 0 E. AC. N. 72 O E. BC. N. 20 30 E. Ch. L.

Stationary Distance AB, S. 88° 30' E. 19.20

The directions given in the last Case for plotting the Field, will apply in this Case also; and the Area in this and the preceding Case may be calculated in the manner pointed out in Case IV. by dividing the Plot into Triangles and measuring Diagonals and Perpendiculars. Or the Sides may be found by Trigonometry, and the Area calculated Arithmetically, as already taught.

CASE IX.

To survey a Field where the boundary Lines are very irregular, without noticing with the Compass every small Bend.

Begin near one Corner of the Field, as at A, PLATE IV. Fig. 68. and measure to the next large Corner, as B, in a straight Line; noticing also the Bearing of this Line. From the Line take Offsetts to the several Bends, at Right Angles from the Line; noticing in the Field Book at what part of the Line they are taken, as A 1, H 2, I 5, B 4. Proceed in the same manner round the Field. In the Figure the dotted Lines represent the stationary Lines, and the black Lines the Boundaries of the Field.

FIELD BOOK.

| Dearing and D | istance. | Unsets | Bearing and Distance | Offsets |
|---------------|----------|--------|------------------------|---------|
| | | Ch. L. | | Ch. L. |
| AB. N. 85° 0' | E. 11.20 | 0.56 | EF. S. 67° 50' W. 8.20 | 0.40 |
| | at 5.40 | | at 1.4 | 1 |
| | 8.26 | 0.36 | 2.96 | 0.33 |
| | the end | 0.36 | 5.88 | 1. |
| | 3 | | the end | 0.12 |
| BC. N. 7° 20' | E. 7.96 | 0.20 | 1.8) 1, | |
| | at 2.36 | 0.36 | FG. S. 27° 40' E. 7.06 | 1.20 |
| | 4.28 | 0.9.6 | at 2. | 0.24 |
| | the end | 0.30 | the end | 0.16 |
| CD. N. 62° 0' | W. 4.68 | | GA. S. 25° 20' W, 6.48 | |
| | at 4.34 | 1 | at 3.80 | 1 000 |
| DE. N. 11°10' | W. 4.20 | 0.30 | the end | 0.40 |

To protract this Field.

Draw the stationary Lines according to the directions in Case IV. From A make an Offset of 56 Links to 1; measure from A to H 540 Links and make the Offset H 2, 140 Links; measure from A to I 826 Links and make the Offset I 3, 36 Links: at B make the Offset B 4, 36 Links. Proceed in the same manner round the Field, and connect the ends of the Offsets by Lines, which will represent the Boundaries of the Field.

To find the Area.

Find the Area within the Stationary Lines as before aught; then of the several small Trapezoids Parallelograms and Triangles made by the Stationary Lines, Offsetts and boundary Lines, and add the whole together: Thus, add 56 Links the Offset A 1 to 140 Links the Offset H 2 and multiply their sum 196 by half 540 the length of the Line AH, and the Product 52920 Square Links will be the Area of the Trapezoid AH21: Again, add 140 the Offset H2 to 36 the Offset I3 and multiply their Sum 176 by half 286 the length of the

Line HI, and the product 25168 Square Links will be the Area of the Trapezoid HI32. Proceed in the same manner to calculate the Area of all the Trapezoids, Triangles, &c.

CASE X.

To survey a Field by taking Offsets both to the Right and Left; that is, within and without the Field, as occasion shall require, in consequence of the Stationary Lines crossing the boundary Lines: Also, by Intersections, that is, taking the Bearing of an inaccessible Corner from two Stations.

The directions given in the preceding Case, together with the following Field Book, will show the Learner how to survey a Field like the following, and also to protract it when surveyed.

FIELD BOOK. See PLATE IV. Fig. 69.

| Offsets to the Left. | | Offsets to the Right. | Remarks. |
|-----------------------|---|-----------------------------|--|
| Ch. L. 1.12 3.40 1.25 | Ch. L. AB. N. 88° 0′ W. 22.12 at 4.25 7.40 13. | Ch. L. | A Tower bears from A. N. 48°. W. |
| 0.45 | BC. N. 27°45′ W. 21.12 at 4.10 10.25 15. | | |
| | C 1. S. 82° 15′ E. 5.45 1, 2. N. 70 0 E. 13.25 2 D. N. 20 0 E. 3.36 | | From C go into the Field to 1, on account of some impediment on or near the boundary Line. At D, you get into another Corner of the Field. |
| 5 | DF. S. 35° 0′ E. 15.15 | | E an inaccessible Corner bears from D. S. 65° 30′ E. |
| 2.20 2.32 | FA. S. 15° 15′ E. 15.10 at 1.20 7.45 12.25 | 0.36 | E the inaccessible Corner bears from F N. 4° W. |

Note. To draw a Tree, House, Tower, or any other remarkable object, in its proper place, in the Plot of a Field—From any two Stations, while surveying the Field, take the Bearing of the object; and the intersection of the Lines, which represent the Bearings, will determine the place of the object; in the same manner that the Tower is drawn in the Figure.

To find the Area of the above Field.

Find the Area within the stationary Lines, and then of the several small Trapezoids, &c. remembering to distinguish those without the stationary Lines from those which are within. Subtract the Area of those within the stationary Lines from the Area of those without, and add the Remainder to the Area contained within the stationary Lines; the sum will be the whole Area of the Field.

SECTION III.

RECTANGULAR SURVEYING, or an accurate method of calculating the Area of a Field Arithmetically, from the Field Book, without the necessity of protracting it, and measuring with a Scale and Dividers, as is commonly practised.

1. Survey the Field, in the usual method, with an accurate Compass and Chain; and from the Field Book set down, in a Traverse Table, the Course or Bearing of the several Sides, and their length in Chains and Links, or Rods and Decimal parts of a Rod; as in the 2d and 3d Columns of the following Example.

| × |
|-----|
| |
| M'P |
| PIE |
| [H |
| - |

| | | က | 7 | 6 | C)r | 4 | , (2) | 22 | p4 | No. |
|---|--|------------------|----------------|---------------|---------------|----------------|----------|------------------|---------------|----------------------------|
| | | N. 38 15 W. | S. 3630 W. | West | 5 South | 4 S. 11 0 E. | 3 East | 2 N. 37 30 E. 40 | N.15° 0'E. 80 | Courses |
| _ | | 34 | 40 | 40 | 54 | 50 | 30 | 40 | 80 | ch |
| - | 135 70 135 23 84.60 84.84 135 46 135 46 84 77 84 79 | 25.70 26.65 | | ÷ | | : | | 31.73 31.66 | 77.27 77.15 | z |
| | 135 23 84.60 135 46 84 77 | • | 32.1 5 | | 54.0 54.10 | 49.08 49.15 | | | | ŝ |
| | 84.60 84.73 | • | | | | 9.54 9.56 | 30.04 | 24.35 24.38 | 20.71 | in in |
| | 84.84 | 21.05 21.02 | 23.79 23.75 | 40°6 39.95 | | : | | | | W. |
| 3 | - | 0. 0 | 21.02 | 44.77 | 84.72 | 8 4.72 | 75.16 | 45.12 | 20.74 | 1 Dep: Col. |
| | | 21.02 | 65.79 | 129.49 | 169.44 | 159.88 | 120.28 | 65.86 | 20.74 | |
| | 245.4016 | 5 60.1830 | | • | | • | <u></u> | 2085.1276 | 1600.0910 | 2 Dep. North Col. Areas |
| | 4245.4016[19143.9019 | • | 2119.0959 | • | 9166.7040 | 7858.1020 | | : | | South |

19143.9019 Sum of South Areas 4245.4016 North Do.

2)14898.5003 Double Area of the Field

Acres 744)92501 Area

4

Roods 3)70004

40

Rods 28)00160

Acres Roods Rods

Area 744 — 3 — 28

2. Calculate by RIGHT ANGLED TRIGONOMETRY, CASE I, or find by the Table of Difference of Latitude.

and Departure,* or by the Table of Natural Sines;† the Northing or Southing, Easting or Westing made on each Course, and set them down against their several Courses, in their proper Columns, marked N. S. E. W.

Note. To determine whether the Latitude and departure for any particular Course and Distance are accurately calculated, square each of them; and if they are right, the Sum of their Squares will equal the Square of the Distance, for the following reason: The Latitude and Departure represent the two Legs of a Right Angled Triangle, and the Distance the Hypothenuse; and it is a Mathematical truth, that the Square of the Hypothenuse of any Right Angled Triangle is equal to the Sum of the Squares of the two Legs.

3. If the Survey has been accurately taken, the Sum of the Northings will equal the Southings; and the Eastings will equal the Westings. If upon adding up the respective Columns, these are found to differ very considerably, the Field should be again surveyed; as some error must have been committed either in taking the Courses or measuring the Sides.‡ If the difference is small, a judicious, experienced Surveyor will judge from the nature of the ground or shape of the Field surveyed, where the mistake was most probably made, and will correct accordingly. Or, the Northings and Southings, and the Eastings and Westings may be equalled by balancing them, as follows: Subtract one half the difference from that Column which is the largest, and add the other half to that Column which is the smallest; and let the difference to be added or subtracted be divided among the several Courses according to their length.

^{*} For an explanation of this Table, and the manner of using it, see the Remarks preceding the Table.

[†] See the Remarks preceding the Table of Natural Sines.

[‡] A method of determining whether the Courses are right has been already explained. See page 50. The Surveyor, before he leaves the Field, should calculate the Northings, Southings, &c. and if he finds much difference determine whether the Courses are right. This will show him whether a re-survey is necessary, and will enable him to ascertain whether the error lies in the Courses or Distances.

In Example I. the upper numbers are the northings, &c. as found by a Table of Difference of Latitude and Departure. The Several Columns being added, the Northings are found to exceed the Southings 47 Links; and the Westings to exceed the Eastings 24 Links. They may be balanced by taking 24 Links from the Northings, and adding 23 Links to the Southings; and taking 12 Links from the Westings and adding 12 Links to the Eastings. Take from the first Course of the Northings 12 Links, from the second 7, and from the third 5; to the first Southing add 7 Links, to the second 10, and to the third 6: Add to the first Easting 3 Links, to the second 3, to the third 4, and to the fourth 2; take from the first Westing 5 Links, from the second 4, and from the third 3. The lower numbers will then represent the Northings, &c. as balanced.

4. These Columns being balanced, proceed to form a Departure Column, or a Column of Meridian Distances; which shows how far the end of each Side of the Field is East or West of the Station where the calculation begins. This Column is formed by a continual addition of the Eastings and subtraction of the Westings; or by adding the Westings and subtracting the Eastings: See Example I.

The first Easting 20.74 is set for the first number in the Departure Column; to this add 24.38 the second Easting, and it makes 45.12 for the second number; to this add 30.04 the third Easting, and it makes 75.16 for the third number; to this add 9.56 the fourth Easting, and it makes 84.72 for the fourth number; the fifth Course being South, it is evident the Meridian Distance will remain the same, therefore place against it the same Easting as for the preceding Course; from this subtract 39.95 the first Westing, and it leaves 44.77 for the sixth Course; from this subtract 23.75 the second Westing, and it leaves 21.02 for the seventh Course; from this subtract 21.02 the last Westing, and it leaves 0.0 to be set against the last course, which shows that the additions and subtractions have been accurately made. For as the Eastings and Westings equal

each other, it is evident that one being added and the other subtracted, there will in the end be no Remainder.

5. The next step in the process is to form a second departure Column, the numbers in which show the Sum of the Meridian Distances at the end of the first and second, second and third, third and fourth Courses, &c.

The first number in this Column will be the first in the other Departure Column; to which add the second number in that Column for the second in this; for the third add the second and third; and for the fourth the third and fourth; and so on till the Column be com-

pleted. See Example I.

The first number to be placed in the second Departure Column is 20.74; to this add 45.12 and it makes 65.86 for the second number; to 45.12 add 75.16 and it makes 120.28 for the third number; to 75.16 add 84.72 and it makes 159.88 for the fourth number; to 84.72 add 84.72 and it makes 169.44 for the fifth number; to 84.72 add 44.77 and it makes 129.49 for the sixth number; to 44.77 add 21.02 and it makes 65.79 for the seventh number; to 21.02 add 0.0 and it makes 21.02 for the eighth number.

6. When the work is thus far prepared, multiply the several numbers in the second Departure Column, by the Northings or Southings standing against them respectively; place the Products of those multiplied by the Northings in the Column of North Areas, and of those multiplied by the Southings in the Column of South Areas; add up these two Columns and subtract the less from the greater; the Remainder will be double the Area of the Field, in Square Rods or Square Chains and Links, whichever measure was used in the Survey.

Demonstration of the preceding Rules. See PLATE

III. Fig. 63. and Example I.

The dotted Line A 2 represents the Northing, and the Line 2 B the Easting made by the first Course: These multipled together, that is, 77.15×20.74 = 1600:0910, which is double the Area of the Tri-

angle A 2 B, as is evident from the Rule to find the Area of a Triangle, PROB. IX. Rule 1. This number is to be placed for the first number in the Column of North Areas. The Line 3 C represents the Sum of the Eastings made by the first and second Courses, which is 45.12 the second number in the first Departure Column; if to this you add 20.74 the length of the Line 2 B you have 65.86, which is the second number in the second Departure Column, and which represents the Sum of the two Lines 3 C and 2B. These two Lines with the Line 2, 3 which represents the Northing made by the second course, and the Line BC, one of the Sides of the Field, form a Right Angled Trapeziod. Now, by the Rule to find the Area of such a Trapezoid, See Prob. X. 65.86×31.66=2085.1276. double the Area of the Trapezoid 2 BC 3. Place this Product for the second number in the Column of North Areas.

To the Line 3 C add CD 30.04 the Easting made by the third Course, and you have 75.16 which is the Sum of the Eastings made by the three first Courses, and the third number in the first Departure Column. this add 9.56 the Easting of the fourth Course, and you have 84.72 the length of the line 1 E, which represents the Sum of the Eastings made by the four first Courses, and is the fourth number in the first Departure Column. These two, viz. the Lines 3 D 75.16 and 1 E 84.72 added together make 159.88 the fourth number in the second Departure Column; which being multiplied by 49.15 the length of the line 3, 1 which represents the Southing made by the fourth Course, will give double the Area of the Trapezoid 1 ED 3. The number thus produced is 7858.1020, which is to be placed for the first number in the Column of South Areas.

The fifth Course being due South, it is evident the Sum of the Eastings will remain the same as at the end of the fourth Course: That is, the Line 4 F equals the Line 1 E, which is 84.72. These added make 169.44 the fifth number in the second Departure Column. This being multiplied by 54.10 the length of the Line

EF, which is the Southing of the fifth Course, as corrected in balancing, and the same as the Line 1, 4—will give double the Area of the Parallelogram 1EF4, which is 9166.7040 the second number in the Column of South Areas.

From the Line 4F 84.72 subtract 39.95 which is a West Course, and it leaves 4G 44.77 the Sum of the Eastings, or the Meridian Distance, at the end of the sixth Course, and the sixth number in the first Departure Column. From this subtract 23.75 the Westing made by the seventh Course, and you have 21.02 the length of the Line 5H, which is the Meridian Distance at the end of the seventh Course, and the seventh number in the first Departure Column. The Line 4G 44.77 added to the Line 5H 21.02 make 65.79 the seventh number in the second Departure Column. This being multiplied by 32.21 the length of the Line 4, 5—which is the Southing of the seventh Course, will give double the Area of the Trapezoid 4GH5, which is 2119.0959 the third number in the Column of South Areas.

The Line H5, 21.02 is the Westing of the last Course, and the last number in the second Departure Column. This being multiplied by 26.65 the length of the Line 5A, and the Northing of the last Course, produces 560.1830, which is double the Area of the Triangle A5H, and the last number in the Column of North Areas.

Note. It will be observed that against the third and sixth Courses there are no Areas; the reason is that these Courses being one East and the other West, there is no Northing or Southing to be multiplied into them; regard can therefore be had to them only in forming the Departure Columns.

By inspecting the Figure, and attending to the preceding illustrations, it will be seen that the three North Areas represent double the Area of the Triangle A2B, the Trapezoid 2BC3, and the Triangle A5H, all of which are without the boundary Lines of the Field: Also, that the three South Areas represent double the Area of the Trapezoid 3DE1, the Parallelogram 1EF4 and the Trapezoid 4GH5; and that these in-

clude not only the Field but also what was included in the North Areas. Therefore the North Areas subtracted from the South, the Remainder will be double the Area of the Field, contained within the black Lines.

Additional Directions and Explanations.

The Northings and Southings may be added and subtracted instead of the Eastings and Westings; then there will be two Latitude Columns instead of Departure Columns; and the numbers in the second Latitude Column must be multiplied into the Eastings and Westings, and you will have East and West Areas.

When the Course is directly North or South, the Distance must be set in the North or South Column; when East or West, in the East or West Column. There will therefore sometimes be no number to be added to or subtracted from the number last set in the Latitude or Departure Column; then the number last placed in the Column must be brought down and set against such Course; as in Example I. at the 5th Course. It may also sometimes be the Case that there will be no number to multiply into the number in the second Latitude or Departure Column; then that number must be omitted, and against such Course there will be no Area; as in Example I. at the 3d and 6th a Courses.

When the Northings or Southings, Eastings or Westings, beginning at the top, will not admit of a continual addition of the one and subtraction of the other, without running out before you get through the several Courses, you may begin at such a Course as will admit of a continual addition and subtraction; and when you get to the bottom go to the top, and you will end in Cypher at the Course next above that where you began; as in Example II. which begins at the 9th Course to add the Eastings and subtract the Westings.

EXAMPLE II.

| | 1 | Dist | 1 | | | | 1 dep | 2 dep | North | South |
|-----|-------------|--------|------|-------|------|-----------|-------|-------|----------|----------|
| No. | Courses. | Rods | N. | S. | E. | W. | Col. | Col. | Areas | Areas |
| | | | | | | | | | | |
| 1 | N.7500/F. | 54.8 | 14.2 | | | | | | 3341.26 | |
| 2 | M. 20 30 E | 41.2 | 38.6 | • • • | 14.4 | | 158.5 | 302.6 | 11680.36 | |
| 3 | Bast. | 54.8 | | | 648 | | 223.3 | 381 8 | | |
| 4 | S. 33 30 W | 141.2 | | 117.7 | | 77.9 | 145 4 | 363.7 | | 43395,99 |
| 1 5 | S. 76 U W. | 64 | • | 15 5 | | 62.1 | 833 | 228.7 | | 3544.85 |
| ñ | North. | 35 | 36 | | | | 83.3 | 166.6 | 5997.60 | |
| 17 | S 84 0 W. | 16.4 | • | 4.9 | | 46.1 | 37 2 | 120.5 | | 590.45 |
| 8 | N. 53 15 W. | 4.4 | 27.8 | | | 37.2 | 0.0 | 37.2 | 1034 16 | |
| 9 | N. 3545 E. | 76.8 | 61.5 | | 46 | | 46 | 46 | 2829 | |
| 10 | N 22 SO E. | 56 | 51.7 | | 21 4 | | 67 4 | 113.4 | 5862.78 | |
| 11 | S. 76 45 E. | 48 | | 11 | 467 | | 114. | 181.5 | | 1996.50 |
| 12 | S. 15 0 W | . 43.4 | | 41.9 | | 11.2 | 1029 | 217 | | 9092.30 |
| 13 | S. 16 45 W | . 40.7 | | | | | | 1 | | 7531.08 |

Area 110 Acres, 2 Roods, 23 Rods.

Note. In the above Example you might begin at the 4th Course to add the Westings and substract the Eastings; or at the 6th Course to add the Northings and substract the Southings; or at the 11th Course to add the Southings and substract the Northings. So in every Survey some place may be found where you may begin to add and substract without running out before you get through all the Courses.

When a Field is very irregularly shaped, it will often happen that parts of the same Area will be contained in several different products in the Columns of Areas; but in the final result, one Column being subtracted from the other will leave what is included within the boundary Lines of the Field.

DEMONSTRATION. See PLATE III. Fig. 64. and Example II.

The Area standing against the 9th Course, which is where the Calculation begins, is the Triangle I2K, all without the Field.

The Area against the 10th Course is the Trapezoid 2KL3, also without the Field.

The Area against the 11th Course is the Trapezoid 4ML3. This is a South Area, and contains a part of the Field and also part of the preceding North Area;

The Area against the 12th Course is the Trapezoid 5NM4, part within and part without the Field.

The Area against the 13th Course is the Trapezoid

6AN5, part within and part without the Field.

The Area against the 1st Course is the Trapezoid 6AB7, part within and part without the Field. This is a North Area and to be ultimately subtracted from the South Areas; but this includes a part of the preceding South Area, viz. the space nAso; it will however be seen hereafter that this same space is included in another South Area. This North Area contains also a part of the first North Area, viz. the space 6no7; but the same space is also included in another South Area.

The Area against the 2d Courses is also a North Area, and is the Trapezoid 7BC8. This Trapezoid contains the space sBCx, without the Field; the space osxw, within the Field; and the space 70w8, without the Field. But the space osxw will be contained in the next South Area; and the space 70w8, which was contained in the two first North Areas, will be contained in the next South Area.

By examining the whole Figure, in this manner, it will be seen that the North Areas contain all without the Field that is taken into the Calculation, and some of it twice over; they also contain part of the Area within the Field. The South Areas contain all within the Field, and all without the Field that is contained in the North Areas. / They also contain, twice over, so much of the Field as is included in any of the North Areas; and likewise, twice over, that part without the Field which is contained twice in the North Areas. So that subtracting the North from the South Areas leaves double the Area of the Field.

This method of calculating the Area of a Field by the Northings. Southings, Eastings and Westings, divides the Field, with a certain quantity of the adjoining ground, into Right Angled Triangles, Right Angled Trapezoids, Parallelograms, or Squares, as may be seen by the Figures. It may therefore with propriety be

called RECTANGULAR SURVEYING.

A USEFUL PROBLEM.

To find the true Area of a Field which has been measured by a Chain too long or too short.

Calculate the Area as if the Chain was of a true

length, then institute the following Proportion:

As the Square of the length of the true Chain;

Is to the Area, as found by the Chain made use of; So is the Square of the length of that Chain;

To the true Area of the Field.

EXAMPLE.

Suppose a Field, measured by a Two Rod Chain 3 Inches too long, is found to contain 41 Acres 1 Rood

and 33 Rods, what is the true Area?

As the Square of 33 Feet, the true length of a Two Rod Chain; Is to 41 Acres 1 Rood and 33 Rods; So is the Square of 33 Feet 3 Inches, the length of the Chain used in the Survey; To 42 Acres and 13 Rods. 33 Feet=396 Inches, 396×396=156816 Square Inches.

41 Acres 1 Rood 33 Rods=6633 Rods.

33 Feet 3 Inches=399 Inches. 399×399=159201 Square Inches.

 $159201 \times 6633 \div 156316 = 6733$ Rods.

6733 ÷ 160 = 42 Acres 13 Rods, the true Area.

PART II.

LAYING OUT LAND.

PROBLEM I. To lay out any number of Acres in

the form of a Square.

Annex 5 Cyphers to the number of Acres, which will turn them into Square Links, the Square Root of which will be the Side of the Square in Links.

Example. It is required to lay out 810 Acres in

the form of a Square.

Answer. Each Side of the Square must be 9000 Links, or 90 Chains.

PROBLEM II. To lay out any number of Acres in the form of a Parallelogram, whereof one Side is given.

Divide the number of Acres, when turned into Square Links, by the given Side; the Quotient will be the Side required.

EXAMPLE. What must be the longest side of a Parallelogram, which is to contain 25 Acres, when the

shortest side is 5 Chains and 50 Links?

Answer. 2500000 ÷ 550=4545 Links for the longest Side.

PROBLEM III. To lay out any number of Acres in

a Field, 3, 4, 5, 6, &c. times as long as it is broad.

Divide the Acres, when turned into Square Links, by the proportion between the length and breadth; the Square Root of the Quotient will be the shortest Side.

Example. It is required to lay out 100 Acres 5

times as long as it is broad.

Answer. 10000000 ÷ 5 = 2000000 the Square Root of which is 1414 Links for the shortest Side, and the longest will be 7070 Links.

PROBLEM IV. To make a Triangle which shall contain a given number of Acres, being confined to a certain Base.

Double the given number of Acres, to which annex 5 Cyphers, and divide by the Base; the Quotient will be the Perpendicular in Links.

Example. Upon a Base of 40 Chains to lay out

100 Acres in a Triangular form.

Answer. 5000 Links or 50 Chains will be the length

of the Perpendicular.

The Perpendicular may be erected from any part of the Base: Thus, the Triangle ABC. See PLATE II. Fig. 55. is the same as ABE, each containing 100 Acres.

When the given Base is so situated that a Perpendicular of sufficient length cannot be erected therefrom, continue the Base as from B to D. Fig. 56. from which erect the Perpendicular DC, and complete the Triangle ABC, which will contain 100 Acres.

PART III. DIVIDING LAND.

As different Fields are so variously, and many of them irregularly shaped, and as they are required to be divided in many different proportions, it is difficult to give Rules which will apply to particular cases. The business of dividing Land must therefore be left, in a great measure, to the skill and judgment of the Surveyor; who, if he is well acquainted with Trigonometry, and with measuring Land, will not find it difficult after a little practice, to divide a Field in such a manner as shall be desired. If he has before him a Plot of the Field, and knows the number of parts into which it is to be divided, and the proportion which each part is to bear to the others, he will readily find out where the dividing Lines are to be drawn.

A few Rules and Examples will be given for the

general instruction of the Learner.

PROBLEM I. To cut off any number of Acres from

a Square or Parallelogram.

Say, As the whole number of Acres in the Field; Is to the length of the Square or length or breadth of the Parallelogram; So is the number of Acres proposed to be cut off; To their proportion of the length or breadth.

PROBLEM II. To cut off any number of Acres by a Line proceeding from any Angle of a Triangle.

Measure the Base, or Side opposite the Angle from which the dividing Line is to be drawn; Then say, As the number of Acres in the whole Triangle; Is to the whole Base; So is the given number of Acres; To their part of the Base.

EXAMPLE. See PLATE II. Fig. 57.

In the Triangle ABC, which contains 48 Acres, it is required to cut off 18 Acres, by a Line proceeding from C to the Base AB, which is 40 Chains.

As 48: 40:: 18: 15

Lay 45 Chains on the Base from B to D, and draw the Line CD. The Triangle will then be divided as was proposed; BCD containing 18 Acres.

PROBLEM III. To take off any given number of Acres from a multangular Field.

EXAMPLE I. See PLATE III. Fig. 65.

Let ABCD, &c. be the Plot of a Field containing 11 Acres, from which it is required to cut off 5 Acres.

Join two opposite Corners of the Field as D and G, with the Line DG (which you may judge to be near the partition Line) and find the Area of the part DEFG, which suppose may want 140 Rods of the quantity proposed to be cut off. Measure the Line DG, which suppose to be 70 Rods; divide 140 by 35 the half of DG, and the Quotient 4 will be the length of a Perpendicular whose Base is 70 and Area 140. Lay off 4 Rods from G to I, and draw the Line DI, which will be the dividing Line.

EXAMPLE II. See PLATE III. Fig. 60.

Let ABCD, &c. be a Tract of Land, to be divided into two equal parts, by a Line from I to the opposite Side CD; To find Arithmetically on what part of the Line CD the dividing Line IN will fall; or to find the Distance CN.

| | | | | | FIELD | BOOK. |
|-----|----|-----|----|----|-------|--------------------|
| | | | | | Rods. | Rods. |
| AB, | N, | 19° | 0' | E. | 108 | GF. West, 70.9 |
| BC. | S. | 77 | 0 | E. | 91 | GH. N. 36 0 W. 47 |
| CD. | S. | 27 | Q | E. | 115 | HI. North, 64.3 |
| DE. | S. | 52 | 0 | W. | . 58 | IA. N. 62 15 W. 59 |
| EF. | S. | 15 | 30 | E. | 76 | Acres Rood Rods |
| | | | | | , | Area 152 — 1 — 25 |

Find the Area of the part IABCI, according to Section III. Page 59, as follows: Set the Latitude and Departure of the three first Sides IA, AB and BC in their proper Columns, in a Traverse Table; and place as much Southing, viz. 109.1 equal to the Line CK, and as much Westing, viz. 71.7 equal to the Line KI, as will balance the Columns. This Southing and Westing will be the Latitude and Departure made by the Line CI. The Area of IABCI will be found to be 8722 Rods, which is less than half the Area of the whole Field by 3470 Rods, the quantity to be contained in the Triangle ICN.

Find the Bearing and Distance of CI by RIGHT ANGLED TRIGONOMETRY, CASE IV. as follows:

| As CK, the Southing of CI, 109 | 2.03748 |
|--------------------------------|----------|
| :: KI, the Westing of CI, 71.7 | 1.85552 |
| | 11.85552 |
| | 2.03743 |
| : Tangent Course S. 33° 20' W. | 9.81809 |
| As Sine Course 33° 20' | 9.73997 |
| Departure KI 71.7 | 1.85552 |
| :: Radius | 10.00000 |
| | 11.85552 |
| | 9.73997 |
| Distance IC 130 | 2.11555 |

Note. In this way the Course and Distance may be found

from one Angle of a Field to another.

Having found the Line CI divide 3470, the number of Rods to be contained in the Triangle ICN, by one half the Line CI, viz. 65, the Quotient will be the length of the Perpendicular PN, viz. 53.4.

Now by the Bearings of CI and CD it appears that they form an Angle of 60° 20′; wherefore in the Triangle CPN are given the side PN 53.4 and the Angle

at C 60° 20', to find the Hypothenuse CN.

| As Sine PCN 60° 20′ : Side PN 53.4 : : Radius | 9.93898 1.72754 10.00000 |
|---|--------------------------------|
| | 11.72754 9.93898 |
| : Hyp. CN 61.5 | 1.78856 |

Thus the dividing Line must go from I to a Point on the Line CD, which is 61.5 Rods from C. The Bearing and Distance of this Line may be found by the directions given above for finding the Bearing and Distance of the Line CI. Or, they may be found by Oblique Trigonometry CASE III.

Another method of finding the Distance CN.

Having ascertained the Latitude and Departure of the Line CI, set them down in a Traverse Table; find the Latitude and Departure of the Line CD, and place them in the Table; the Difference between the Northing of the Line IC, and the Southing of the Line CD will be the Southing of the Line DI. viz. 6.6; and the Sum of the Eastings of those Lines, as they are both Easterly will be the Westing of the Line DI, viz. 123.9. Proceed to calculate the Area of the Triangle ICD, which will be found to be 6522 Rods, nearest.

Note. As in this Triangle two Sides and their contained Angle are given, the Area may be found by PROB. IX. Rule 4. Page 39.

Having found the Area of this Triangle, proceed to find CN according to Prob. II. Page 71, as follows:

As the Area of the Triangle; Is to CD the Base; So is the quantity to be contained in the Triangle ICN; To CN its proportion of the Base.

As 6522: 115:: 3470: 61.2

A third method of finding the Distance CN.

To the Logarithm of double the Area to be contained within the Triangle ICN add Radius; from this Sum subtract the Logarithmic Sine of the Angle at C; and from the Remainder subtract the Logarithm of the Side IC; the last Remainder will be the Logarithm of the Side CN.

The double Area of the Triangle ICN is 6940; the

Angle at C is 60° 20′; the Side IC is 130.

| Double Area 6940 Radius | - | 3.84136 10.00000 |
|----------------------------|-----|---------------------|
| Sine ICN 60° 20' | | 13.84136 9.93898 |
| Side IC 130 | | 3.90238 2.11394 |
| Side CN 61.5 | ek: | 1.78844 |

Note. Radius may be added by placing a Unit before the Index of the Logarithm for the double Area without the trouble of setting down the Cyphers.

By Natural Sines.

Divide the double Area by the Natural Sine of the given Angle, and that Quotient by the given Side; the last Quotient will be the Side CN.

Nat. Sine of the Angle at C 60° 20' 0.86892

 $6940 \div 0.86892 = 7986.92$

 $7986.92 \div 130 = 61.43$

From the above the following general Rule may be drawn.

To find the Side of a Triangle when the Area is given, with one of the Sides and the Angle contained between the

given Side and the Side required.

To the Logarithm of double the Area add Radius; from this sum subtract the Logarithmic Sine of the given Angle, and from the Remainder subtract the Logarithm of the given Side; the last Remainder will be the Logarithm of the Side required.

Or, By Natural Sines: Divide the double Area by the Nat. Sine of the given Angle, and that Quotient by the given Side; the last Quotient will be the Side re-

quired.

CONCLUDING REMARKS.

Other methods of surveying Fields are taught by some authors on this Subject. The preceding, however, will be found most useful in actual practice. Other instruments beside those mentioned in this Book are also sometimes used; such as the Plain Table, Semicircle, Perambulator, Theodolite, &c. But of these instruments very little use is made in New-England; and they are not often to be met with. For general practice none will be found more useful than a common Chain, and a Compass upon Rittenhouse's construction. A Surveyor should also provide himself with an Offset Staff, ten Links in length, and accurately divided into Links. This should be made of firm, hard wood, and will be found very convenient in taking Offsets, and also in measuring the Chain: which should be often done, as from a variety of causes a Chain is liable to become inaccurate.

It will be observed that in this work there are no descriptions of Mathematical and Surveying instruments. The Compiler omitted such descriptions from a belief that nothing which can be written on the Subject will enable a person to understand them without an actual inspection of the instruments themselves, and some instruction from those acquainted with them.

The general principles here taught may be applied to the surveying of Townships, Roads, Rivers, Har-

bors, &c.

APPENDIX.

Of the VARIATION of the COMPASS and ATTRACTION of the NEEDLE.

THE Variation of the Compass is the number of Degrees that the Magnetic Needle points from the true North, either East or West. This differs in different places, and in the same place at different times. It is, at present, in Connecticut, a few degrees to the Westward. That is, the Needle points to the Westward of North and is gradually approaching the true North.

The following method of ascertaining the Variation, by the North Star has been adopted by many Surveyors, as the most eligible to be practised on Land. It was communicated to the Compiler by Moses Warren, jun. Esq. of Lyme, an experien-

sed Surveyor, with permission to publish it.

The Star commonly called the North Star, is not directly North but revolves round the Pole in a small circle, once in 24 hours. It cannot therefore be due north but twice in that peried; and that is within a very few minutes of the time when a Star, called Alioth, in the Constellation of Ursa Major, or the Great Bear, is directly over or under it. There is also another Star nearly in an opposite direction from the Pole, called Gamma, in the Constellation of Cassiopeia. When these three Stars are vertical, the North Star is very near the Meridian; and when they are horizontal, it is at its greatest Elongation, that is, at its greatest distance East or West of the Pole, and on the same side as the Star in Cassiopeia. The Variation may be calculated when the Star is on the Meridian, or when at its greatest Elongation; more accurately, however, at the latter period, because its motion being then nearly vertical for some time, gives the observer a better opportunity to complete his observation.*

* The following Figure exhibits a view of the relative situation of these Stars as they appear, when in a horizontal position: or when the North Star is in its greatest Eastern Elongation.

To find the Elongation of this Star in any Latitude, its Declination must be known; that is, its distance North of the Equator. This being found, institute the following Proportion:

As Co-Sine of the Latitude; Is to Radius; So is Co-Sine of

the Declination; to Sine of the Elongation.

From a Table in Blunt's Practical Navigator it appears that the Declination of the North Star, January 1, 1800, was 88° 14′ 32″, and increasing at the rate of 19.69 Seconds annually. Consequently, January 1, 1805, the Declination will be 88° 16′ 10″, and the Co-Declination or Polar Distance will be 1° 43′ 50″.

According to the above Proportion, the Elongation, January 1, 1805, in Lat 41° 30′ will be 2° 18′ 39″, and in Lat. 42° it will

be 2° 19' 44".

The following Table shows the Elongation in several different Latitudes for five years successively. It is calculated for the first of January in each year; and in using it, if the time when the Elongation is required, be past the middle of the year, take it for the beginning of the next year.

A Table showing the Elongation of the North Star.

| Latitud. | 1805 | 1806 | 1807 | 1808 | 1809 |
|----------|-------------|------------|------------|------------|------------|
| 39° 30′. | 2° 14′ 35′′ | 20 14' 10" | 2° 13′ 44′ | 2° 13′ 19″ | 3° 12′ 53″ |
| 40 | 2 15 34 | 2 15 8 | 2 14 43 | 2 14 17 | 2 13 52 |
| 40 30 | 2 163 4 | 2 16 8 | 2 15 42 | 2 15 17 | 2 14 51 |
| 41 | 2 17 36 | 3 17 10 | 2 16 44 | 2 16 18 | 2 15 52 |
| 41 30 | 2 18 39 | 2 18 13 | 2 17 47 | 2 17 20 | 2 16 54 |
| 42 | 2 19 44 | 2 19 18 | 2 18.51 | 2 18 25 | 2 17 58 |
| 42 30 | 2 20 51 | 2 20 24 | 2 19 58 | 2 19 31 | 2 19 5 |
| 13 | 2 22 0 | 2 21 33 | 2 21 6 | 2 20 40 | 2 20 ,13 |
| 43 30 | 2 32 10 | 2 22 43 | 2 22 16 | 2 21 49 | 2 21 22 |

The Elongation for the Latitude of the observation being calculated, or taken from the above Table, proceed to find its

range, according to the following directions:

Take a pole 18 or 20 feet in length; to the end of it fasten a small line; raise it to an elevation of 45° or 50°: and support it by two crotches of a suitable height to keep it firm in its place. At the end of the line, near the ground, fasten a weight of half a pound or more, which should swing in water to prevent the air from moving the line. Southward of the line, fix a Compass sight; or other piece of metal or wood, with a narrow, perpendic-

ular aperture at a convenient height from the ground, say about 2 or 2 1-2 feet; and let it be so fixed that it can be moved a small distance East or West at pleasure. Let an assistant hold a light either NE. or NW. of the line, nearly as high as the range from the sight to the North Star, in such a position that the line may be plainly seen; then, (the three Stars above mentioned being parallel or nearly so with the Horizon) move the sight-vane East or West, until through the aperture, the line is seen to cut the Star; and continue to observe, at short intervals, till the Star is seen at its greatest Elongation. Let a lighted candle be placed in an exact range with the sight-vane and line at the distance of 20 Rods or more, which should stand perpendicularly, be made fast, extinguished and left till morning. Then the sight-vane, the line and the candle will be the range of Elongation, which observe accurately with a Compass; and if the Elongation be-East and the Variation West, the former must be subtracted from the latter; but if they are both West they must be added, and their difference or sum will be the true Variation.

Of the ATTRACTION of the NEEDLE.

IT is well known that any Iron substance has an influence upon the magnetic Needle, attracting it one way or the other from the point where it would settle, were there no such attraction. A Surveyor should therefore be careful to see that no Iron is near the Compass when taking a Bearing. But as the Earth in certain spots contains, near its surface, Iron or other minerals which attract the Needle, it will frequently happen that it will point wrong. To ascertain whether this is the case, the Surveyor, at each station, should take a back view of the one last left; and if he finds that the Compass does not reverse truly he may be sure, provided the Compass be accurately graduated and placed horizontally, that he either made a mistake at the last station, or that in one or the other of the stations, the Needle was attracted from the true point. When he finds a place where he suspects there is an attraction he should go a few rods backward or forward, and see whether the Needle points differently. In this way he may prevent making mistakes in his Field notes, by putting down a wrong course. take back sights is particularly necessary in running long Lines, and laying out new Lands; where the needle is the only thing to guide the Surveyor.

By practice and experience a knowledge will be acquired on this subject, and with regard to many other things in Surveying, which cannot be taught by Books; and after all the directions which can be written the Practitioner will frequently find occasion for the exercise of his own judgment. A Rule to find the difference between the present Variation of the Compass, and that at a time when a Tract was formerly surveyed, in order to trace or run out the original lines.

Go to any part of the premises where any too adjacent corners are known; and, if one can be seen from the other, take their bearing; which, compared with that of the same line in the former survey, shows the difference. But if one corner cannot be seen from the other, run the line according to the given bearing, and observe the nearest distance between the line so run and the corner: then work by the following proportion,

As the length of the whole line,
Is to 57.3 Degrees,*
So is the said distance,
To the difference of Variation required.

EXAMPLE.

Suppose it be required to run a line which some years ago bore N. 45°. E. distance 20 Chains, and in running this line by the given bearing, the corner is found 20 Links to the left hand; what is the present bearing of this line?

Ch. Deg. L.
As 20: 57.3:: 20

100 20

2000 1146.0
60

2000)687£0(34 Minutes.

Answer 34 Minutes to the left hand is the allowance required, and the line in question bears N. 44°. 26' E.

^{• 57.3} Degrees is the Radius of a Circle (nearly) in such parts as the Circumference contains 360.

MATHEMATICAL TABLES.

VIZ.

- I. A Traverse Table, or Table of Difference of Latitude and Departure.
- II. A Table of Natural Sines.
- III. A Table of Logarithms for Numbers.
- IV. A Table of Logarithmic or Artificial Sines, Tangents and Secants.
- I. A TRAVERSE TABLE, or TABLE OF DIFFERENCE OF LAT-ITUDE AND DEPARTURE, calculated for Degrees and Quarters of Degrees, and for any Distance up to 50 Rods, Chains, &c; by which the Northings and Southings, Eastings and Westings made in a Survey may be found.

Note. Northings and Southings are called Difference of Latitude, or simply Latitude; Eastings and Westings are called Departure, Meridian Distance, or Longitude.

Explanation of the Table.

To find the Latitude and Departure, or Northing, &c. for any Course and Distance.

If the Course be less than 45° look for it at the Top, but if more than 45° at the Bottom of the Page; and look for the Distance in the Right or Left hand Column: Against the Distance, and directly under or over the Course, stand the Northing, &c. in whole numbers and Decimals.

If the Course be less than 45°, the Northing or Southing will be greater than the Easting or Westing; but if more than 45°, the Easting or Westing will be the greatest.

When the Distance exceeds 50, divide it by 2, 3, or 4, that is, take one half, one third, or one fourth of it, and multiply the Latitude and Departure by the number by which the Distance was divided: Or, take any two or more numbers, which added together will equal the Distance, and find the Latitude and Departure for each of those numbers; add the Several Latitudes together and the sum will be the whole Latitude; and so for the Departure. And when the Distance is in Chains and Links, or whole Numbers and Decimals, find the Latitude, &c. for the Chains or whole Numbers, and then for the Links or Decimals, remembering to remove the Decimal Point in the Table further to the Left, according to the given Decimal.

EXAMPLES.

- 1. Required the Latitude and Departure for 45 Rods, on a Course N. 15° 15' W.
- Under 15° 15' and against 45 is 43.42 for the Northing and 11.84 for the Westing.
- 2. Required the Latitude and Departure for 120 Rods, on a Course S. 58° 30' E'.

Take one third of 120 which is 40; against this number, over 58° 30′ is 20.90 for the Latitude and 34.11 for the Departure. These multiplied by 3 give 62.70 for the Southing and 102.33 for the Easting.

3. Required the Latitude and Departure for 37.36 Rods or 37 Chains and 36 Links, on a Course N. 26° 45' E.

| For 37. Lat. 0.36 | .32 | Dep. | 16.65 |
|-------------------|-------|------|-------|
| 37.36 | 33.36 | | 16.81 |

Northing 33.36 Easting 16.81

Wote. When the Minutes are not 15, 30 or 45, the Northings, &c. must be calculated by Natural Sines, or by Trigonometry.

Note in the second Edition. The Traverse Table, as published in the first Edition of this work was copied from a Table in Gibson. The Compiler, finding that to be incorrect in several places, has calculated the whole anew; and it is presumed it will be found to be correct as published in this Edition.

| o i | Deg. | TR | AVE | RSET | ABL | E. | 83 |
|------|----------------|----------|------------------|------|----------------|------|------------|
| | , 00 | 15' | 90 | 30′ | 00 | 45' | U |
| ist. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep | Diet |
| 1 | 1.00 | 0.00 | 1.00 | 0.01 | 1.00 | 0.01 | |
| 2 | 2.00 | 0.01 | 2.00 | 0.02 | 2.00 | 0.03 | 2 |
| 3 | 3.00 | 0.01 | 3.00 | 0.03 | 3.00 | | 3 |
| 4 | | 0.02 | 4,00 | 0.03 | 4.00 | | 4 |
| 5 | | 0.02 | 5.00 | | 5.00 | | |
| 6 | | 0.03 | 6.00 | 0.05 | 6.00 | | |
| 7 | | 0.03 | 7.00 | 0.06 | 7.00 | | |
| 8 | | 0.03 | 8.00 9.00 | 0.07 | 8.00 9.00 | | - 1 |
| 10 | | 0.04 | 10.00 | 0.09 | 10.00 | 0.12 | |
| - | 11.00 | | | | 11.00 | 0.14 | |
| 11 | | 0.05 | 1 i .00 12.00 | 0.10 | 12.00 | 0.14 | 1 |
| 1 | 13.00 | 0.05 | 13.00 | 0.10 | 13.00 | 0.17 | - 45 |
| | 14.00 | | 14.00 | | 14.00 | 1 | 1 - 1 |
| 1 | 15.00 | 0.07 | | 0.12 | 15.00 | 1 | 1 1 |
| | 16.00 | | 16.00 | | 1600 | | 3 2 |
| • | 17.00 | 0.07 | | 0.15 | 00 | 3 | 8 U |
| | 18 00 | 0.08 | 18.00 | 0.16 | 18.00 | 0.24 | |
| 19 | 19.00 | 0.08 | 19.00 | 0.17 | 19.00 | 0 25 | 19 |
| 20 | 20.00 | 0.09 | 20.00 | 0.17 | 20.00 | 0.26 | 20 |
| 21 | 21.00 | 0.09 | 21.00 | 0.18 | 21.00 | 0.27 | 21 |
| | ,22.00 | 0.10 | 22.00 | | 100 | 0.29 | 22 |
| 23 | 23.00 | 0.10 | 23.00 | 0.20 | 23.00 | 0.30 | 23 |
| 24 | 24.00 | 0.10 | 24.00 | 0.21 | 24,00 | 0.31 | 24 |
| | 25.00 | | 25.00 | 0.22 | 25.00 | 0.33 | 25 |
| | 25.00 | | 26.00 | | 26.00 | | 9 |
| | 27 00 | | 27.00 | | 27.00 | | 3 3 |
| | 28 00 | | 28.00 | | 28.00 | | 1 |
| | 29.00 | | 29.00 | | 29.00 | 0.38 | A 1 |
| ~ | 30.00 | . No. 11 | 30 00 | - | 30.00 | | } |
| | 31.00 | | 31.00 | | 31.00 | 0.41 | |
| _ | 32.00 | | 32 00 | | 32.00 | | |
| 1 | 33.00 34.00 | | 33 00 | | 33.00 | | |
| | 35.00 | | 34.00 35.00 | | 34.00 35.00 | 0.45 | |
| | 36:00 | | 36 00 | | 36.00 | | |
| | 37.00 | | 37.00 | | 37.00 | 0.48 | 30 |
| | 38.00 | | 38.00 | _ | 38.00 | | 30 |
| | 39.00 | | 39.00 | | 39.00 | 0.51 | 30 |
| | 40.00 | | 40.00 | | 40.00 | 0.52 | 40 |
| - | 41.00 | | 41.00 | | 41.00 | 0.54 | |
| | 242.00 | | 42.00 | - 1 | 42.00 | 0.55 | L |
| | 3 43.00 | | 43.00 | | 43.00 | 0.56 | 12 |
| - 1 | 44.00 | | 44.00 | | 44.00 | 0.58 | 44 |
| 45 | 5 45.00 | | 45.00 | | 45.00 | 0.59 | 4.5 |
| 4.6 | 5 46.00 | 0.20 | 46.00 | 0.40 | 46.00 | 0.60 | 4.6 |
| 47 | 47.00 | 0.20 | 47.00 | l . | 47.00 | 0.62 | 47 |
| | 3 48.00 | 1 | 48.00 | | 48.00 | 0.63 | 4.8 |
| | 49.00 | | 49.00 | | 49.00 | 0.64 | 49 |
| 50 | 50.00 | | 50.00 | | 50.00 | | 50 |
| st. | Dep. | Lat. | Dep. | Lat. | | Lat. | ist. |
| 19 | 89.9 | 4.5% | 890 | 30% | 890 | 15% | 5 |

| 8 | 4 | | T | RAVE | ERSE | | | | | eg | |
|----|------|-----------|------|----------|--------|-------|--------|-------|------|-------|---|
| J | | 10 | 0' | 10 | 5' | 10 | 30' | 10 | 45' | 0 | |
| Ø. | ist: | Late | Dep. | Lat- | Dep. | Latel | Dep. | Lat. | Dep. | ist | |
| ı | | onlinear. | - | | 0.02 | 1.00 | 0.03 | 1.00 | 0.03 | 一 | |
| ı | 1 | 1.00 | 0.02 | 1.00 | 0.04 | 2.00 | | | 0.06 | 2 | |
| ı | 2 | 2 00 | 0.03 | | | | 0.05 | 2.00 | 0.09 | 3 | |
| 1 | 3 | | 0.05 | | 0.07 | 3.00 | 0.08 | 3.00 | | Ł | |
| ı | 4 | 4.00 | 0.07 | 2 | 0.09 | 4.00 | 0.10 | 4.00 | 0.12 | 4 | |
| 1 | 5 | 5.00 | 0.09 | 1 | 0.11 | 5.00 | 0.13 | 5.00 | 0 15 | 5 | |
| ı | 6 | 6.00 | 0 10 | 1 | 0.13 | 6.00 | 0.16 | 6.00 | 0.18 | 6 | |
| ì | 7 | 7.00 | 0.12 | | 0.15 | 7.00 | 0.18 | 7 00 | 0.21 | 7 | |
| | 8 | 8.00 | 0.14 | | 0.17 | 8.00 | 0.21 | 8.00 | | 8 | |
| ı | 9 | | | 1 | 0.20 | 9.00 | 0.24 | 9.00 | | _ | |
| I | 10 | 10.00 | 0.17 | 10.00 | 0 22 | 10.00 | 0.26 | 10.00 | 0.31 | | |
| 1 | ī i | 11.00 | 0 19 | 11.00 | 0.24 | 11.00 | 0.29 | 10.99 | 0.34 | 11 | |
| ı | 12 | 12.00 | 0.21 | 12.00 | 0.26 | 12.00 | | 11.99 | | 12 | |
| | | 13.00 | | 13.00 | 0.28 | 13.00 | | 12.99 | | 13 | |
| 1 | | 14.00 | 0.24 | 14.00 | 0.31 | 14.00 | | 13.99 | | 14 | |
| į | | 15.00 | | 15.00 | | 15.00 | | 14.99 | | 1 3 | |
| | | 16.00 | | 16.00 | | 15.99 | | 15.99 | | | |
| | 1 | 17 00 | | 17.00 | | 16.99 | 0.45 | 16.99 | 0.52 | - 1 | |
| ı | | 18.00 | | 18.00 | | 17.99 | 0.43 | 17.99 | 0.55 | 1 1 | |
| ı | 1 | 19.00 | | 19.00 | | 18.99 | | 18.99 | | | |
| ı | | 20.00 | | 20.00 | | 19.99 | 0.50 | 19.99 | 0.61 | | |
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| i | | 23.00 | | 22.99 | | 22.99 | | 22.99 | 0.70 | 23 | |
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| | | 30.00 | | 29.99 | I _ | 29.99 | 0.79 | 29.99 | 0.92 | 30 | |
| | 31 | 31.00 | 0.54 | 30.99 | 0.68 | 30.99 | 0.81 | 30.99 | 0.95 | 31 | |
| | 32 | 32.00 | 0.56 | 31.99 | 0.70 | 31.99 | 0.84 | 31.99 | | | |
| | 33 | 33.00 | 0.58 | 32.99 | 0.72 | 32.99 | 0.86 | 32.98 | | | |
| | | 33.99 | 0.59 | 33.99 | 0.74 | 33.99 | | 33.98 | | | |
| | | 34.99 | 0.61 | 34.99 | 0.76 | 34.99 | 0.92 | 34.98 | | | |
| | | 35.99 | 0.63 | 35.99 | 0.79 | 35.99 | | 35.98 | | | |
| | 37 | 36.99 | 0.65 | 36.99 | 0.81 | 36.99 | 0.97 | 36.98 | | | |
| | 1 | 37,99 | 0.66 | 37.99 | 0.83 | 37.99 | 1 | 37.98 | | | |
| | • | 38.99 | 0.68 | 38.99 | 0.85 | 38.99 | 1 | 38.98 | | | |
| | _ | 39.99 | 0.70 | 39.99 | 0.87 | 39.99 | | 39.98 | 3 | | |
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| | | 45.99 | | 45.99 | | 45.98 | 1.20 | 45.98 | | | 1 |
| | | 46.99 | | 46.99 | 1.03 | 46.98 | 1.23 | 46.98 | | 4 47 | 1 |
| | | 47.99 | | 47.99 | 1.05 | 47.98 | 1.26 | 47.98 | | | 1 |
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| ŀ | 11 | i0.98 |).58 | 10.98 | 0.62 | 10.98 | 0.67 | 10.98 | 0.72 | |
| ١ | 12 | 11.98 | 0.63 | 11.98 | 0.68 | 11.98 | 0.73 | 11.97 | 0.78 | |
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| | 24 | 33.97 | 1.26 | 23.96 | 1.36 | 23.96 | 1.47 | 23.95 | 1.57 | 24 |
| | 25 | 4.97 | 1.31 | 24.96 | 1.42 | 24.95 | 1.53 | 24.95 | 1 64 | 25 |
| | 26 | 25.96 | 1.36 | 25.96 | 1.47 | 25.95 | 1.59 | 25.94 | 1.70 | 26 |
| | 27 | 26.96 | 1.41 | 26.96 | 1.53 | 26.95 | 1.65 | 26.94 | 1.77 | 27 |
| | 28 | 27.96 | 1.47 | 27.95 | 1.59 | 27.95 | 1.71 | 27.94 | 1.83 | 28 |
| | 29 | z8.96 | 1.52 | 28.95 | 1.64 | 28.95 | 1.77 | 28.94 | 1.90 | 29 |
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| 1 | | 0.21 | | 0.22 | | 0.24 | | 0.25 | | |
| 4. | 3.99 | 0.28 | | 0.30 | | 0 31 | | 0.33 | | |
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| _ | | 0.42 | | 0.44 | | 0.47 | 5.98 | 0.50 | 6 | |
|) | | 0.49 | | 0.52 | | 0.55 | 6.98 | 0.58 | 7 | |
| - 1 | | 0.56 | | 0.59 | | 0.63 | 7.97 | 0.66 | | |
| 1 | | 0.63 | | 0.67 | | 0.71 | | 5.75 | | |
| - | - | 0.70 | | 0.74 | | 0.78 | | 0.83 | | |
| | 1 10.97 | 1 | 10.97 | 0.82 | 10.97 | 9.86 | 10.96 | 0.91 | 11 | |
| 1 | 211.97 | 0.84 | 11.97 | 0.89 | 11.96 | 0.94 | 11.96 | 0.99 | 12 | |
| 1 | 3 12.97 | 0.91 | 12.96 | 0.96 | 12.96 | 1.02 | 12,96 | 1.08 | 13 | |
| 1 | 413.97 | 1.05 | 13.96 | 1.01 | 13.96 | 1.10 | 13.95 | 1.16 | 1-1 | |
| 1 | 5 14.96 6 15.96 | 1.12 | 14.95 | 4 40 | 15 05 | 1.18 | 14.95 | 1.24 | 10 | |
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| 2 | 0 19.95 | 1.40 | 19.95 | 1.48 | 19.94 | 1.57 | 19.93 | 1.66 | 20 | |
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| 2: | 221.95 | 1.53 | 21.94 | 1.63 | 21.93 | 1.73 | 21.92 | 1.82 | 22 | ı |
| 2. | 3 32.94 | 1.60 | 22.94 | 1.70 | 22.93 | 1.80 | 22.92 | 1.90 | 23 | |
| 2 | 433.94 | 1.67 | 23.93 | 1.78 | 23.93 | 1.88 | 23.92 | 1.99 | 24 | |
| 2. | 34.94 | 1.74 | 24.93 | 1.85 | 24.92 | 1.96 | 24.91 | 2.07 | 25 | |
| 2 | 35.94 | 1.81 | 25.93 | 1.93 | 25.92 | 2.04 | 25.94 | 2.15 | 26 | |
| 2 | 26.93 | 1.88 | 26.93 | 2.00 | 26.92 | 2.12 | 26.91 | 2.24 | 27 | |
| 2 | 27.93 | 1.95 | 27.92 | 2.08 | 27.91 | 2.20 | 27.90 | 2.32 | 28 | |
| 2 | 925.93 | 2.02 | 28.92 | 2.15 | 28.91 | 2.28 | 28.90 | 2.40 | 29 | |
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| 3 | 938.90 | 2.72 | 38.89 | 2.89 | 38.88 | 3.06 | 38.87 | 3.23 | 39 | |
| 4 | 039 90 | 2.79 | 39.89 | 2.96 | 39.88 | 3.14 | 39.86 | 3.31 | 40 | |
| 4 | 140.90 | 2.86 | 40.89 | 3.04 | 40.87 | 3.22 | 40.86 | 3.40 | 41 | |
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| 5 | 5 | 50 | ' 0 | , 5° | 15' | 5° | 30' | 5° | 45' | | r |
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| 1 | 1 | | 0.09 | | 0.09 | | 0.10 | | 0.10 | | |
| | 2 | | 0.17 | | 0.18 | | 0.19 | | | 2 | |
| | 3 | | 0.26 | | 0.27 | | 0.29 | | | | |
| | 4 | 3.98 | 0.35 | 3.98 | 0.37 | | 0.38 | | 0.40 | | |
| | 5 | 4.98 | 0.44 | 4.98 | 0.46 | 4.98 | 0.48 | 4.97 | 0.50 | 5 | |
| - 1 | 6 | 5. 98 | 0 52 | 5.97 | 0.55 | 5.97 | 0.58 | 5.97 | J.60 | 6 | |
| | 7 | | 0.61 | 3 | 0.64 | 6.97 | 0 67 | 6.96 | 0.70 | 7 | |
| | 8 | | 0.70 | 1 | 0.73 | | 0.77 | | | 8 | |
| - 1 | 9 | | 0.78 | 1 | 0.82 | | 0.86 | | | 9 | |
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| | 5 | 24.90 | 2.18 | 24.90 | 2.29 | 24.89 | 2.40 | 24.87 | 2.50 | 25 | |
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| | - | | 1. | 34.85 | | | | | 0 -1 | 34 | |
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| 37 | 7 | 36.86 | 3.22 | 36.84 | 3.39 | 36.83 | 3.55 | 36.81 | 3.71 | 37 | |
| | | | | 37.84 | | | | | 3.81 | 38 | |
| | | | | 38.84 | | | | | 3.91 | 39 | |
| 40 |) | 39.85 | 3.49 | 39.83 | 3.66 | 39.82 | 3.83 | 39.80 | 4.01 | 40 | |
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| St. | Lat. | Dep | Lut. | De, | المالية | Den | La. | Le, | ist |
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| 4 | | 0.42 | | 0.44 | | 0.45 | | 0.47 | 4 |
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| 10 | 9.95 | 1.05 | 9.94 | 1.09 | 9.94 | 0.13 | 9.93 | 1.18 | 10 |
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| | 16.91 | | | | | | | | |
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| 8 | 18.90 | | 5 | | | | | | |
| 20 | 19.89 | 2.09 | 19.88 | 2.18 | 19.87 | 2.26 | 19.86 | 2.35 | 20 |
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| 14 | 37.79. | | | | | 9 1 | | | - 4 |
| 39 | 38.79 | 4.08 | 38 77 | 4.25 | 38 75 | 4.41 | 38 73 | 1.58 | 39 |
| | 39.78 | Residence of the last of the l | - | - | - | - | - | | |
| | 40.78 | | | | | | | | |
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| 3 1 | 48.73 | | | | | | | | 1 1 |
| 50 | 49.73 | 5.23 | 49.70 | | | 5.66 | 49.65 | 5.88 | 50 |
| St. | Dep. | Lat. | Dep. | | | Lat. | Dep. | Lat | 3.5. |
| | 84° | 0' | 830 | 45' | 83° | 30' | 830 | 15' | 101 |

| 2.0 | 70 | | 70 | | 70 | ool. | . 70 | 1 2 | 1 1 1 |
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| 12. | 70 | 0' | 7 | 15' | | 30 | | 45' | |
| st. | Lat. | Dep | Lat. | Dep | Lat. | Dep | Lat. | Dep | st. |
| 1 | 0.99 | 0.12 | 0.99 | 0.13 | 0.99 | 0.13 | 0.99 | 0.13 | 1 |
| 2 | | 0.24 | | 0.25 | | 0.26 | | 0.27 | 1 1 |
| 3 | | 0.37 | 4 | 0.38 | 4 | 0.39 | _ | 0.40 | |
| 4 | | 0.49 | | 0.50 | | 0.52 | | 0.54 | 1 1 |
| 5 | | 0.61 | S | 0.63 | | 0.65 | | 0.67 | 5 |
| 6 | | 0.73 | 3 | | | | | | 6 |
| 7 | | 0.85 | | | | | | 0.94 | _ |
| 8 | | 0.98 | • | | | 1.04 | , | 1.08 | 1 |
| 9 | | 1 | 8.93 | | | 1.17 | | | 9 |
| 10 | | 1.22 | | 1.26 | | 1.31 | | 1.35 | |
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| | | | | 1 4 | 10.91 | | | | |
| | , | 1 1 | | | 11,90 | | | | |
| | | | | | 12.89 | | | | |
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| 8 | | | 4 | | 14.87 | | | | |
| 3 | | | | | 15.86 | | Σ | | |
| 17 | 16.87 | 2.07 | 16.86 | 2.15 | 16.85 | 2.22 | 16 84 | 2.29 | 17 |
| 18 | 17.87 | 2.19 | 17.86 | 2 27 | 17.85 | 2.35 | 17.84 | 2.43 | 18 |
| 19 | 18.86 | 2.32 | 18 85 | 2.40 | 18.84 | 2.48 | 18 83 | 2.56 | 19 |
| 20 | 19.85 | 3.44 | 19.84 | 2.52 | 19.83 | 2.61 | 19.82 | 2.70 | 20 |
| 21 | 20.84 | 2.56 | 20.83 | 2.65 | 20.82 | 2.74 | 20.81 | 2.83 | 21 |
| 3 3 | | | | | 21.81 | 1 | 4 | | |
| 1 1 | | | | | 22.80 | , | 3 | | 1 1 |
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| 9 | | | / | 1 | 38.67 | | 2 | | 1 |
| 40 | 39.70 | 4.87 | 39.68 | 5 05 | 39.66 | 5.22 | 39.63 | 5.39 | 40 |
| 41 | 40.69 | 5.00 | 40.67 | 5.17 | 40.65 | 5.35 | 40.63 | 5.53 | 11 |
| 2 | | | | | 41.64 | 1 | 5 | | |
| 1 1 | | | | | 42.63 | 1 6 | | | |
| 8 3 | | | | | 43.62 | | | | |
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| ist | Dep. | Lat. | Dep. | Lat. | Dep. | Lat | Dep. | Lat. | 151. |
| 19 | 83° | 0' | 820 | 45' | 820 | 30' | 820 | 15' | |
| | | | | | | | | | |

| 10 | 1 8° | 0′, | 8° | 15' | 80 | 30' | 80 | 45 | |
|------|--------|-------|----------|-------|----------------|-------|-------|--------|------|
| 181, | Lat. | Dep | Lat. | Dep | Lat. | Dep | Lat | Dep | ist |
| | 0.99 | 0.14 | | 0.14 | | 0.15 | 3 | 0.15 | 1 |
| 0 | | 0.28 | | 0.29 | 1.98 | 0.30 | H | 0.30 | 2 |
| 3 | 3 2.97 | 0 42 | 2.97 | 0.43 | 2.97 | 0.44 | 2.97 | 0.46 | 3 |
| 4 | 3 9 8 | 0.56 | 3.96 | 0.57 | 3.96 | 0 5 9 | 3.95 | 0.61 | 4 |
| 1 5 | 4.95 | 0.70 | 4.95 | 0.72 | 4.95 | 0.74 | 4.94 | 0.76 | |
| 1 6 | 5.94 | 0.84 | £ | 0.86 | 6 | 0.89 | | 0.91 | 6 |
| 7 | 6.93 | 0.97 | 2 | 1.00 | | 1.03 | ¥ | 1.06 | |
| 8 | | 1.11 | i | 1.15 | | 1.18 | | 1.22 | 8 |
| | 8.91 | | 5 | 1.29 | 9 | 1.33 | | 1.37 | |
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| 111 | | | | | 10.88 | | | | 1 11 |
| 12 | | | | _ | 11.87 | 2 | | | [|
| 113 | | | 2 | | 12.86 | 2 | * | 2 6 | 13 |
| 14 | | | | | 13.85 | 2 1 | , | ? | 15 |
| 11.5 | | | | | 14.84 | | | | / 1 |
| 116 | 15.84 | 2.23 | 1600 | 2.30 | 15.82 | 2.30 | 15.81 | 2.43 | 17 |
| 17 | 16.83 | 2.37 | 17 91 | 9 58 | 16.81 17.80 | 2 66 | 10.00 | 2.39 | 18 |
| 18 | 10 00 | 2.51 | 18 80 | 973 | 18.79 | 2.81 | 18.78 | 2 80 | 19 |
| 20 | 100 | 2.04 | 19.00 | 2.87 | 19.78 | 2.96 | 19 77 | 3.04 | 20 |
| - | 1 | | | | | | | - | _ |
| 21 | 20,80 | 2 92 | 20.78 | 3.01 | 20.77 21.76 | 2 75 | 20.76 | 3.19 | 22 |
| 22 | 21.79 | 3.00 | 2976 | 3.10 | 22.75 | 3.40 | 21.74 | 3.50 | 23 |
| 23 | 22.78 | 3.20 | 23.75 | 3.4.4 | 23.74 | 3 55 | 22.13 | 3.65 | 24 |
| 24 | 24.76 | 2 1 9 | 24.74 | 3.59 | 2473 | 3.70 | 24.71 | 0.00 | |
| 25 | 25.75 | 3.40 | 25.73 | 3.73 | 25.71 | 3 84 | 25.70 | 3.96 | 26 |
| 27 | 26.74 | 3.02 | 26.72 | 3.87 | 26.70 | 3.99 | 26.69 | 4.11 | 27 |
| 28 | 27.73 | 3.90 | 27.71 | 4.02 | 27.69 | 4.14 | 27.67 | 4.26 | 28 |
| 29 | 28.72 | 4.04 | 28.70 | 4.16 | 28.68 | 4.29 | 28.66 | 4.41 | 29 |
| 30 | 29.71 | 4.18 | 29.69 | 4.30 | 29.67 | 4.43 | 29.65 | 4.56 | 30 |
| 31 | | | | | 30.66 | | | | |
| 32 | 31.69 | 4.45 | 31.67 | 4.59 | 31.65 | 4.73 | 31.63 | 4.87 | 32 |
| 33 | 132 68 | 4.59 | 32.66 | 4.74 | 32.64 | 4.88 | 32.62 | 5.02 | 33 |
| 34 | 33.67 | 4.73 | 33.65 | 4.88 | 33.63 | 5.03 | 33.60 | 5.17 | 34 |
| 35 | 34.66 | 4.87 | 34.64 | 5.02 | 34.62 | 5.17 | 34.59 | 5.32 | 35 |
| 36 | 35.65 | 5.01 | 35.63 | 5.17 | 35.60 | 5.32 | 35.58 | 5.48 | 36 |
| 37 | 36.64 | 5.15 | 36.62 | 5.31 | 36.59 | 5.47 | 36.57 | 5.63 | 37 |
| 38 | 37.63 | 5.29 | 37.61 | 5.45 | 37.58 | 5.62 | 37.56 | 5.78 | 38 |
| 39 | 38.62 | 5.43 | 38.60 | 5.60 | 38.57 | 5.76 | 38.55 | 5.93 | 39 |
| 40 | 39.61 | 5.57 | 39.59 | 5.74 | 39 56 | 5.91 | 39.53 | 6.08 | 40 |
| 41 | 40.60 | 5.71 | 40.58 | 5.88 | 40.55 | 6.06 | 40.52 | 6.24 | 41 |
| 42 | 41.59 | 5.85 | 41.57 | 6.03 | 41.54 | 6.21 | 41.51 | [6.39] | 42 |
| 43 | 42.58 | 5.98 | 42.56 | 6.17 | 42.53 | 6.36 | 42.50 | 6.54 | 43 |
| 44 | 43.57 | 6.12 | 43.54 | 6.31 | 43.52 | 6.50 | 43.49 | 5.69 | 44 |
| 45 | 44.56 | 6.26 | 44.53 | 6.45 | 44.51 | 5.05 | 44.48 | 5.85 | 45 |
| 46 | 45.55 | 6.40 | 45.52 | 6.60 | 45.49 | 6.0 | 45.46 | 7.10 | 17 |
| 1 | 46.54 | 6.54 | 46.51 | 0.74 | 46.48 | 7.00 | 40.45 | 7 30 | 1 |
| 48 | 47.53 | 6.68 | 47.50 | 7.03 | 47.47 | 7 94 | 47.44 | 7.45 | 19 |
| | 48.52 | 6.82 | 48.49 | 7.03 | 48.46 | 7 20 | 40.43 | | |
| 50 | 49.51 | | | | | | | | 一 |
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| Ü | 820 | 0' | 819 | 45' | 81° | 30' | 810 | 15' | = |

92

4.51 Dep Lit Lat. 0.99 0.99 0.16 016 0.99 () 1; 0.99 0.17 2 1.97 0.32 1.98 0 31 1.97 0.33 1.97 0.342 3 2.96 0.48 2.96 0.47 2.96 0 50 2 96 0.51 3 3 95 0.63 3.95 0 66 4 3.95 0.64 3.94 0.68 4 5 4.94 0.78 4.94 0 80 4.93 0.83 4.93 0.85 5 6 5.93 0 94 5.920.96 5.92 0.99 5.91 1.02 6 1.10 7 6.91 6.91113 1 16 6.90 6.90 1.19 7 7.90 1.25 8 7.90 | 1.29 |7.89 1.32 7 88 1.35 8 9 3.89 1.41 3.88 1.45 8.88 1.49 1.52 8.87 9 10 9.88 1.56 9.87 1.61 9.86 1.69 1 65 9.86 10 1.72 10.86 1.77 :0.86 1.86 :0.85 ₹32 10.84 1.88 11.84 1.93 11.84 12 11.85 1.98 1.83 2.03 12 13 12.84 2.03 12.83 2.09 12.82 2,15 12.81 2.20 13 -.19 13.82 2.25 13.81 2:31 13.80 2.37 14 14 13.83 2.35 14.81 2.41 14.79 4.82 2.48 4.78 2.54 5.80 2.50 15.79 2.57 15.78 16 2.64 15.77 2.71 16 2.66 16.78 2.73 16.77 17 6.79 2.81 16.75 2.88 17 17.78 2.82 17.77 2.89 17.75 2.97 17.74 3.05 18 18 2.97 18.75 3.05 18.74 1877 19 3.14 18.73 3.22 19 19.75 3.13 19.74 3.21 19.73 3.30 19.71 20 3.39 20 3.29 20.73 3.38 20.71 20:4 3.47 20.70 3.56 21 3.44 21.71 3.54 21.70 3.63 21.68 3.73 22 22 21.73 23 22.72 3.60 22.70 3.70 22.68 3.80 22.67 3.90 23 24 23.70 3.75 23.69 3.86 23.67 3.96 23.65 4.06 24 25|24|64|3.91|24.68|4.02|24.66|4|13|24.64|4.23|2526 25.68 4.07 25.66 4.18 25 64 4.29 25.62 4.40 26 27 26.67 4.22 26.65 4.34 76.63 4.46 26.61 4.57 27 28|27.66|4.38|27.64|4.50|27.62|4.62|27.60|4.74|2829|28.64|4.54|28.62|4.66|28.60|4.79|28.58|4.9i|2929 63 4.69 29.61 4.82 29.59 4.95 29.57 5.08 30 30 30 62 4.85 30.60 4.98 30 58 5 12 30.55 5.25 31 31 32 31.61 5.0 31.58 5. 4 31.56 5.28 31.54 5.42 32 33 32.59 5 16 32.57 5.30 32.55 5.45 32 52 5:59 33 34 33.58 5.32 33.56 5.47 33.53 5.6 1 33.51 5.76 34 35 34.57 5.48 34.55 5.63 34.52 5.78 34.49 5.93 35 36 35.56 5.63 35.53 5.79 35.51 5.94 35.48 6.10 36 37 36.54 5.79 36.52 5.95 36.49 6.11 36 47 6.27 37 38 37 53 5 94 37 51 6 11 37 48 6 27 37 45 6 44 38 38.52 6.10 38.49 6.27 38.47 6.44 38,44 6.60 39 39 6 26 39.48 6.43 39.45 39 51 6.60 39.42 40 6.77 40 6.41 40.47 6.59 40.44 6.77 40.41 40 50 6.94 41 42 41.48 6.57 41.45 6.75 41.42 6.93 41.39 7.11|4243 42 47 6.73 42.44 6.91 42.41 7 10 42.38 7.28 43 44 | 43 | 46 | 6.88 | 43.43 | 7.07 | 43 | 40 | 7.26 | 43.36 | 7.45 | 4445 44.45 7.04 44.42 7.23 44.38 7.43 44.35 7.62 45 46 45.43 7.20 45.40 7.39 45.37 7.59 45.34 7.79 46 47 46 42 7.35 46.39 7.55 46.36 7.76 46.32 7.96 47 48 47.41 7 51 47.38 7.72 47.34 7.92 47.31 8.13 48 49 48.40 7.67 48.36 7.88 48.33 8.09 48.29 8.30 49 49.38 7.82 49.35 8.04 49.31 8.25 49.28 8.47 50 50 Lat. Dep. Dep. Lat Dep. Dep 800 800 451 30' 80° 15'

| £ | 0 1 | Jeg. | | IKAV | | | | | | 93 |
|---|-------|---------|-----------------|------------------|--------|--------|--------|--------|--------|--------|
| 1 | C | 100 | 0' | 10° | 15' | 100 | 30' | 100 | 45' | 5 |
| - | Jist. | Lat. | Dep | Lat. | Dep | Lat. | Dep | Lat | Dep | 18. |
| i | 1 | | J. 17 | 0.98 | | | | | 0.19 | 1 |
| | 2 | | 0.35 | | | 1.97 | _ | | 0.37 | 2 |
| | 5 | | 0.52 | _ | | 2.95 | | | 0.56 | 9 |
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| | 8 | | 1.39 | | | 7.87 | | | 1.49 | 8 |
| | 9 | 1 | 1 56 | | 1.60 | 8.85 | 1.64 | | 1.68 | |
| | 16 | 9.85 | 174 | 9.84 | 1.78 | 9.83 | 1.82 | 9.82 | 1.87 | 10 |
| | 11 | 10.83 | 1.91 | 19.82 | 1.96 | 10.83 | 2.00 | 10.81 | 2.05 | 11 |
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| | 17 | | | 16.73 | | | | | | |
| | 18 | 17.73 | 3.13 | 17.71 | 3 20 | 1770 | 3.28 | 17.68 | 3.36 | 18 |
| | 19 | | | 18.70 | | | | | | |
| | 20 | 19.70 | 3.47 | 19.68 | 3.55 | 19.67 | 3.64 | 19.65 | 3.73 | 20 |
| | 2: | 20.68 | 3.65 | 20.66 | 3.74 | 20.65 | 3.83 | 20.63 | 3.92 | 21 |
| | 22 | | | 21.65 | | | | | | |
| | 23 | | | 22.63 | | | | | | |
| | 24 | | | 23.62 | | | | | | |
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| | 20 | 25.6 | 4 51 | 25.59 | 4.63 | 25.56 | 4.74 | 25.54 | 4.85 | 26 |
| | 27 | 26 59 | 4.69 | 26.57 | 4.80 | 26.55 | 5.92 | 26.53 | 5.04 | 27 |
| | | | | 27.55 | | | | | | |
| | 29 | | | 28.54 | | | | | | |
| | 30 | 29 54 | $\frac{1}{5.2}$ | 29.52 | [5.34] | 29.50 | 5.47 | 29.47 | 5.60 | 30 |
| | 131 | 30.53 | 5.38 | 30.51 | 5.52 | 30.48 | 3 5.65 | 30.40 | 5 5.78 | 31 |
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| 9 | Ą | T | RAVE | RSE | TAB | LE. | | 11 1 |)eg |
|------------|---------|-------------------|-------------------|---|--------|--------|-------|--|-------|
| 15 | | 12 0' | 11 | 0 15 | 11 | ° 30′ | 1 11 | ° 45′ | 10 |
| 3 | Lat. | De | p Lat. | De | p.Lat. | De | Lat. | Dep. | ist. |
| | | 8 0.1 | 9 0.9 | 80.2 | 0 0.9 | 8 0.20 | | - | |
| | 2 1.9 | 60.3 | 88, 1.9 | 6,0.3 | 9 1.9 | 5 0.40 | | | 1 1 |
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| | 1 | 30.7 | | | 8 3.99 | 1 | | 0.81 | 4 |
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| - 2 | | $\frac{5}{3}$ 1.7 | 3 7.8 | | 2 | 1 1.60 | | |) -) |
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| 1: | 1.0.0 | | 0 10.7 9 11.7 | | | | | 1 | 11 |
| 13 | | | 8,12.7 | | | | | | 1 1 |
| 14 | | | 7 13.7 | | | | | | 1 |
| 11.5 | | | 6 14.7 | | | | | | 3 |
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| 17 | | | 4 16.6 | | .4 | | 2 | | |
| 18 | 3 17.6 | 1 | 3 17.6 | | | | | | 2 |
| 19 | 1.0.0 | | 3.18.6 | | | | | | 19 |
| 20 | 19.6 | 3 3.8 | 2 19.6 | 3.90 | 19.60 | 3.99 | 19.58 | 4.07 | 20 |
| 21 | 10.0 | 1 4.0 | 1 20 6 | 4.10 | 20.58 | 4.19 | 20.56 | 4.28 | 21 |
| 22 | 1~1.00 | 0 4.20 | 0 21.58 | 3 4.29 | 21.56 | 4.39 | 21.54 | 4.48 | 22 |
| 23 | 1-7.0 | | 22.56 | | | | | | 23 |
| | | | 3 23.54 | | | | | | 24 |
| 25 | 24.54 | 4.77 | 24.52 | 24.88 | 24.50 | 4.98 | 24.48 | 5.09 | 0.4 |
| 27 | | | 5 25.50 | | | | | | 3 |
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| 29 | 28 47 | 5.54 | 1 27.46 28 44 | 5 66 | 22.44 | 5 78 | 28 20 | 5.70 5.91 | 1 |
| 30 | 29.45 | 5.72 | 29.42 | 5.85 | 29 40 | 5.98 | 29 37 | 6.11 | - 1 |
| 31 | | | 30.40 | | | | | 6.31 | |
| 32 | | | 31.39 | | | | | | |
| 33 | 32.39 | 6.30 | 32.37 | 6.44 | 32.34 | 6.58 | 32 31 | 6.72 | |
| 34 | 33.38 | 6.49 | 33.35 | 6.63 | 33.32 | 6.78 | 33.29 | 6.92 | |
| 35 | | | 34.33 | | | | | 7.13 | |
| 36 | 35.34 | 6.87 | 35.31 | 7.02 | 35.28 | 7.18 | 35.25 | 7.33 | |
| 37 | 36.32 | 7.06 | 36.29 | 7.22 | 36.26 | 7.38 | 36.22 | 7.53 | 37 |
| 38 | 37.30 | 7.25 | 37.27 | 7.41 | 37.24 | 7.58 | 37.20 | 7.74 | 38 |
| 10 | 38.28 | 7.44 | 38.25 | 7.61 | 38.22 | 7.78 | 38.18 | 7.94 | 39 |
| 40 | 39.27 | - | 39.23 | | | | | 8.15 | 4 - 6 |
| 41 | | | 40.21 | | | | | 8.35 | 81 |
| 42 43 | | | 41.19 | | | | | 8.55 | 2 |
| 44 | | | 42.17 | | | | | 8.76 | 3 |
| 45 | 10.15 | | 43.15 | | | | | 8.964 | 4 |
| 46 | | | 44.14 | | | | | 9.16 | 5 |
| 47 | | | 45.12 46.10 | | | | | 9.37 | 6 |
| 4 8 | 20.11 | | 47.08 | | | | | 9.57 | 7 |
| 49 | | | 48.06 | | | | | 9.77 ₄ 9.98 ₄ | 8 |
| 50 | | | | | | | | 10.18 5 | 9 |
| | Dep. | Lat | 49.04 Dep. 78° | Eat ! | Den | [2] | Den | | |
|)is | 700 | 0/ | 700 | 45' | 78° | 30' | 78° | Lat. 5 | 201 |
| 1 | 1 1 3 | | 10 | 43 1 | 10 | 20, | 150 | 151 10 | 11 |

| 7- | 1 12° | 0' | 120 | 15' | 120 | 301 | 120 | 4.5' | 90 |
|------|----------------|------|----------------|------|----------------|-------|----------------|-------------------|-------|
| 1810 | • | | | | 1 | - | | | 12:1 |
| 1- | _! | Dep. | | Dep. | - | Dep. | | Dep. | Si. |
| - 1 | 0.98 | | | | | | | | , 1 |
| | 1.96 3 2.93 | | 1 | 1 | | | | | |
| 4 | | | | | | | | | 1 3 |
| 5 | | 1 | | | | | _ | | |
| - 1 | 5.87 | | 1 | 1 | | 1 | | | 1 2 |
| 7 | | | | | | | 4 | 1 | |
| 8 | | 1 | | | 1 | | | | 1 |
| 2 | | | | | | | | | |
| 10 | 9.78 | 2.08 | | | | | 9.75 | | 10 |
| 111 | 110.76 | 2.29 | 10.75 | 233 | 10.74 | 2.38 | 10.73 | 2.43 | 11 |
| p. | 11.74 | | 11.73 | | 11.72 | | 11.70 | | 1 3 |
| 113 | 12.72 | | 12.70 | | 12.69 | | 12.68 | | : (|
| 114 | 13.69 | | 13.68 | | 13.67 | | 13.65 | | 1 1 |
| 15 | 14.67 | | 14.66 | | 14 64 | 3.25 | 14.63 | | |
| | 15.65 | 3.33 | 15.64 | | 15.62 | 3.46 | 15.61 | 3,53 | 16 |
| | 16.63 | 3.53 | 16.61 | | 16.60 | 3.68 | 1658 | | |
| | 17.61 | | 17.59 | 3.82 | 17.57 | 3.90 | 17.56 | 3.97 | 18 |
| 119 | 18.58 | | 18.57 | | 18.55 | | 18.53 | 4.19 | 19 |
| 20 | 19.56 | 4.16 | 19.54 | 4.24 | 19.53 | 4.33 | 19.51 | 4.41 | 20 |
| 21 | 20.54 | 4.37 | 20.52 | 4.46 | 20.50 | 4.55 | 20 48 | 4.63 | 1 - 1 |
| 22 | | 1 | 21.50 | | 21.48 | | 21.46 | 4.86 | 22 |
| 23 | | | 22.48 | | 22.45 | | 22.43 | 5.08 | 23 |
| 24 | 23.48 | 4.99 | 23.45 | 5.09 | 23.43 | 5.19 | 23.41 | 5.30 | 24 |
| | 24.45 | 3 | 24.43 | | 24.41 | | 24.38 | 5.52 | 1 7 |
| * | 25.43 | | 25.41 | | 25.38 | | 25.86 | 5.74 | 1 1 |
| | 26.41 | | 26.39 | | 26.36 | | 26.33 | 5.96 | 1 1 |
| - 1 | 27.39 | • | 27.36 | | 27.34 | | 27.31 | 6.18 | 1 |
| 1 | 28.37 | | 28.34 | | 28.31 | | 28.28 29.26 | 6.40 | 1 1 |
| - | 29.34 | | 29.32 | - | 29.29 | | | 6.62 | |
| 14 | 30.32 | | 30.29 | | 30.27 | | 30.24 | 6.84 | |
| | 31.30 | | 31.27 | | 31.24 | | 31.21 | 7.06 | |
| | 32.28 | | 32.25 | 1 | 32.22 | | 32. 19 | 7.28 7.50 | 1 |
| | 33.26 34.24 | | 33.23 34.20 | | 33.19 34.17 | | 34.14 | 7.72 | |
| | 35.21 | | 35.18 | | 35.15 | | 35.11 | 7.95 | 3 |
| | 36.19 | | 36.16 | | 36.12 | | 36.09 | 8.17 | |
| | 37.17 | | 37.13 | | 37.10 | | 37.06 | | |
| | 38.15 | | 38.11 | | 38.08 | | 38.04 | 8 61 | 39 |
| | 39.13 | | 39.09 | | 39.05 | | 39.01 | 8.83 | |
| - | 40.10 | | 40.07 | | 40.03 | | 39.99 | 9.05 | 41 |
| | 41.08 | 4 | 41.04 | | 41.00 | | 40.96 | 9.27 | 42 |
| L 1 | 42.06 | | 42.02 | | 41.98 | | 41.94 | 9.49 | 43 |
| | 43.04 | | 43.00 | | 42.96 | | 42.92 | 9.71 | 4.4 |
| | 44.02 | | 43.98 | | 43.93 | | 43.89 | 9.93 | 45 |
| 1 | 44.99 | | 44.95 | | 44.91 | 9.96 | 44.87 | 10.15 | 46 |
| | 45.97 | 9.77 | 45.93 | | | 10.17 | | 10.37 | 47 |
| | 46.95 | 9.98 | 46.91 | | _ | 10.39 | | 10.59 | 48 |
| | 47.93 | | 47.88 | | 47.84 | 10.61 | | | 49 |
| 3 | 48.91 | | 48.86 | | | 10.82 | | | 50 |
| st. | Dep. | Lat. | Dep. | Lat | ep. | Lat. | Dep. | Lat. | st. |
| O | 78° | 0' | 770 | 45'. | 770 | 30' | 770 | 15' | |
| - | | | | | - | | - | Marie Committee (| - |

| <u>}</u> | 96 | 2 | | TRA | VEI | RSI | ET | ABLI | 2. | | 13] | Deg |
|----------|-------|--------------|-------|----------------|-------|------------|--------------|-------|-----|--------------------------|-------------|----------------|
| | Dist. | 1 | 3° 0′ | 1. | 3° 1. | 5 | 13 | ° 30′ | 1 | 13 | 45' | 10 |
| 1 | | Lat | De | p. La | t. D | υp. | Lat | . De | p | Lat | Dej | St. |
| | 1 | 0.9 | 7 0.2 | 23 0.9 | 7 0 | .23 | 0.9 | | - | 0.9 | - | - 1 |
| | 2 | 1.9 | | | 5 0. | 46 | 19 | | _ | 1.9 | | |
| | 3 | 2.9 | | | | .69 | | 2 0.1 | 70 | 2.9 | 1 0.7 | 1 3 |
| | 4 5 | 3.9 | | | | 92 | | | | 3.8 | 9 0.9 | 5 4 |
| | 6 | 4.8 | | | | 15 | | | | 4.8 | 1 | |
| | 7 | 5·8 6-8 | 1 | | - 1 | .38 | | | | 5.8 | 1 1 | |
| | 8 | 7 8 | 1 | | | .60 .83 | | | 3 | 6.8 | | 1 1 |
| 1 | 9 | 8.7 | Ş. | | _ | .06 | | | 37 | 7.7° 8.7° | | |
| 1 | 0 | 97 | | 14 | - 40 | 29 | | 1 - | | 97 | 1 | |
| 1 | 1 | 10.79 | | 7 10.7 | | | | _ | - 1 | | | |
| - 1 | | 11.69 | 9 2.7 | 011.6 | - 1 | | 10 7 11 6 | | | 10.68 11.6 | | |
| 1 | | 12.67 | | 212.6 | | | 12.6 | | | 12.63 | | 5 12 13 |
| 1. | | 13.64 | , | 5 13.6 | | | 13.6 | | | 13.60 | | |
| | | 14.62 | 2 | 7 14 6 | | | 14.5 | | | 14.57 | | |
| 1 | | 15 59 | | 0 15.5 | | | 15.5 | | | 5.5 | | |
| 17 | 1 | 16.56 | | 2 16.5 | 1 | | 16.53 | | 7 | 6 5 | 4 04 | 117 |
| 118 | | 17.54 | 4.0 | 5 17.5 | , | | 17.50 | | | 17 48 | | |
| 19 | | 8.51 | ă | 7 18.4 | 9 4. | | 18.48 | | | 18.46 | • | |
| 20 | | 9.49 | 4.5 | 0 19.4 | 7 4. | 58 | 19.45 | | | 9 45 | | |
| 21 | | 20.46 | | 2 20.4 | 4 4. | 81 | 20.45 | 4.9 | 0 2 | 0.40 | 4-95 | $\frac{1}{21}$ |
| 22 | 2 2 | 21.44 | 4.9 | 5 21.4 | | | 21.39 | | _ | | | 1 - 1 |
| 23 | 3 2 | 22.41 | 5.17 | 7 22.39 | | | 22,36 | | | 2 34 | | |
| | , | 23.38 | | 23.3 | 5. | | 23.34 | | 0,2 | 23.3 | 5.70 | |
| | | 4.36 | 1 | 2 24.3 | | 73.2 | 24.31 | | | 4 28 | | 25 |
| | | 5.33 | | 5 25.3 | | _ | 25.28 | | 7 2 | 5 25 | 6.18 | 26 |
| | - | 6.31 | | 7 26.28 | | | 26.25 | | | 6.23 | | 27 |
| | | 7.28 | | 27-25 | | | 27.23 | | | 7-20 | | |
| | | 8.26 | | 28-23 | | | 8.20 | • | | 8.17 | 1 | 1 1 |
| - | | 9.23 | | 29 20 | - | - | 9.17 | | 0 2 | 9 14 | 7.13 | 30 |
| | | 0.21 | | 30.17 | | | 0 14 | 1 | | 0.11 | 7.37 | 31 |
| | | 1.18 | | 31.15 | | _ | 1.12 | | | 1 08 | 1 | 32 |
| | | 2.15 | | 32 12 | 1 | | 2.0 | | | 2 05 | | |
| | | 5.13 4.10 | | 33.09 | 1 | _ | 3 06 | | | 3.08 | | |
| | _ | 5 08 | | 34.07 35 04 | | _ | 4.03 | | | 4-00 | | 1 |
| | | 6.05 | | 36 02 | | | 5,01 | | | 4.97 | | 1 |
| | • | 7 03 | | 36.99 | | | 5.98 6 95 | | | 5.94 | 8.79 | |
| | | 8.00 | | 37 96 | | - 14 | 7 92 | | | 6.9 ₁ 7 88 | | |
| | | 8.97 | | 38.94 | | - 4 | 8 89 | | | 8 85 | 9.27 9.51 | 39 |
| | 1- | 9.95 | | 39 9 1 | | <u> </u> | 9 87 | | 1 | | | |
| | | 0.92 | | 40.88 | | | 0 84 | | | | 9.75 | 41 |
| | | 1 90 | | 41 86 | | | | | | | 9 98 | _ |
| | ł | 2.87 | | 42 83 | | 2 1 | 9 78 | 0.97 | 4 | 7 | 10.22 | 44, |
| | | | | 43 80 | 10.3 | 1 4 | 3 76 | 10 51 | 15 | 2 7 1 | 10.40 | 1.5 |
| 45 | 4. | 4.82 | 10.35 | 44.78 | 10.5 | 4.4 | 473 | 10 74 | 11/ | 1.68 | 10.70 | 4.6 |
| 47 | 4. | 5.80 | 10.57 | 45.75 | 10 7 | 74 | 5 70 | 10:97 | 24. | 5.65 | 11.17 | 47 |
| 48 | 4 | 6 77; | 10.80 | 46.72 | 11.0 | 04 | 6 67 | 11.21 | 4.9 | 1.62 | 11.41 | 48 |
| 49 | 4 | 7.74 | 11:02 | 147.70 | 11.2 | 34 | 7.65 | 11.44 | 47 | 60 | 11.65 | 49 |
| 5 W | 4 | 8.72 | 11.25 | 48.67 | 11.4 | 64 | 8.62 | 11.67 | 48 | 3 57 | 11.88 | 50 |
| Dist. | D | ep. | Lat. | Dep. | Las | - 65 | ep, | Lat | D | (-D) | Lat | 11 |
| Ä | | 770 | 0' | Dер. 76° | 45' | -1- | 760 | 30' | - | 769 | 15/ | 115 |
| | | | | | | 4 | - | | | U | 13 | - |

| 100 | 4 | Deg. | | TRA | VERS | SE T | ABLE | | | 9.7 |
|-----|-----------------|---|-------|----------|-------|----------------|-------|----------------|-----------------|--------|
| ١ | D | 140 | 0' | 140 | 15' | 14° | 30' | 140 | 45' | TEN |
| | st. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | 138. |
| | 1 | 0 97 | 0.24 | 0.97 | 0.25 | 0.97 | 0.25 | 0.97 | 0.25 | 1 |
| | 2 | 1.94 | 0.48 | 1.94 | 0.49 | 1.94 | 0.50 | 1.93 | | 2 |
| | 3 | 2.91 | 0.73 | 2.91 | 0.74 | 2.90 | 0.75 | 2.90 | 0.76 | 3 |
| 1 | 4 | 3.88 | 0.97 | 3.88 | 0.98 | 3.87 | 1.00 | 3.87 | 1.02 | 4 |
| Ì | 5 | | 1.21 | | 1.23 | 3 | | | 1.27 | |
| ı | 6 | (| | | 10 | a . | | | | 5 |
| 1 | 7 | | 1.69 | | | CR CR | 1 | | | 7 |
| | 8 | | 1.94 | | 1.97 | 8 | | | | 8 |
| ۱ | 9 | | 2.18 | | | 2 | 1 | | | 9 |
| 1 | 10 | | 2.42 | | 2.46 | 1 | | | $\frac{2.55}{}$ | 10 |
| 1 | - 1 | 10.67 | | 10.66 | 2.71 | | 2 | 10.64 | 2.80 | 11 |
| | | 11.64 | | 11,63 | | 11.62 | | 11.60 | 3.06 | . ~ |
| 1 | | 12.61 | 1.5 | 12.60 | | 12.59 | | 12.57 | | 1 1 |
| | | 13.58 | | 13,57 | | 13 55 | | 13.54 | | |
| 1 | | 14.55 | | 14.54 | | 14.52 | | 14.51 | 3.82 | |
| 1 | | 15.52 16.50 | | 15.51 | | 15.49 16.46 | | 15.47 | | 16 |
| | | 17.47 | | 17.45 | | 17.43 | | 16.44 17.41 | | |
| - | | 18.44 | | 18.42 | | 18.39 | (') | 18.37 | 4.58 | - LE 1 |
| 1 | | 19.41 | | 19.38 | | 19.36 | | 19.34 | 4.84 5.09 | 19 |
| -1 | $\frac{20}{21}$ | | | 20.35 | | 20.33 | | í ——— | | 465 |
| - 1 | الكا | 21.35 | | 21.32 | | 21.30 | | 20.31 | 5.35 | 21 |
| - | | $\begin{array}{c} 21.35 \\ 22.32 \end{array}$ | | 22.29 | | 22.27 | ' | 21.28 | 5.60 | |
| - 1 | | 23.29 | | 23.26 | | 23.24 | | 22.24 23.21 | 5.86 | - 1 |
| - 1 | | 24.26 | | 24.23 | | 24.20 | | 24.18 | 6.11 | 24 |
| | | 25.23 | | 25,20 | | 25.17 | | 25.14 | | ~ • ; |
| -1 | - 1 | 26,20 | | 25.17 | | 26.14 | | 26.11 | 6.87 | |
| | - | 27.17 | | 27.14 | | 27.11 | | 27.08 | | 7 1 |
| | | 28.14 | | 28.11 | | 28.08 | | 28.04 | | |
| - | | 29.11 | | 29.08 | 7.38 | 29 04 | | 29.01 | 7.64 | |
| Ì | 31 | 30.08 | 7.50 | 30.05 | 7.63 | 30.01 | | 29.98 | 7.89 | |
| | | 31.05 | | 31.02 | | 30.98 | | 30 95 | | |
| | | 32.02 | | 31.98 | | 31.95 | | 31.91 | 8.40 | |
| - | | 32.99 | | 32.95 | | 32.92 | | 32.88 | 8.66 | |
| ¥ | - | 33.96 | | 33.92 | 8.62 | 33.89 | | 33.85 | 8.91 | 35 |
| | 36 | 34.93 | 8.71 | 34.89 | 8.86 | 34.85 | 9.01 | 34.81 | 9.17 | |
| | 37 | 35.90 | 8.95 | 35.86 | 9.11 | 35.82 | 9.26 | 35.78 | | 37 |
| 1 | 38 | 36.87 | 9.19 | 36.83 | 9.35 | 36.79 | 9.51 | 36.75 | 9.67 | 38 |
| | | 37.84 | 9.43 | 37.80 | | 37.76 | | 37.71 | 9.93 | 39 |
| 1 | 40 | 38.81 | 9.68 | 38.77 | 9.85 | 38.73 | 10.02 | 38.68 | 10.18 | 40 |
| | 41 | 39.78 | 9.92 | 39.74 | 10.09 | 39.69 | 10.27 | 39.65 | 10.44 | 41 |
| ı | 42 | 40.75 | 10.16 | 49.71 | | | 10.52 | | | 42 |
| ١ | 43 | 41.72 | 10.40 | 41.68 | | | 10.77 | | | 43 |
| ł | | 42.69 | | 42.65 | | | 11.02 | , , | | 44 |
| 7 | | 5 | | 43.62 | | | 11.27 | | | 45 |
| | | | | 44.58 | | | | | | 4.6 |
| | | | | 45.55 | | | | | | 47 |
| - 5 | | | | 46.52 | | | | | | 48 |
| | | | , , | 47.49 | | | | | | |
| | | 48.51 | 12.10 | 48.46 | 12.31 | 48,41 | 12.52 | 48.35 | 12.73 | 50 |
| - | Jist | Dep. | Lat. | Dep. 75° | Lat. | Dep. | Lat. | D p. | Lat. | ist |
| - | 7 | 760 | 0' | 75° | 45' | 750 | 30' | 750 | 15' | Al. |

| 1 | U | 1 1.5 | | 1 | 150 | 15' | 15 | | 30' | 1150 | 45 | 10 |
|--|----------|------------------------|---------------------------------------|------------|------|------|-----------------|------|----------|----------------|--------------|-------------|
| 1 | ist. | Lat. | | D. 8 | Lat. | Dep | 100 | | Dep. | - | | 181 |
| - | <u> </u> | 0.9 | | _ | 0.90 | | - | J· | 0.27 | 1 | | 1 |
| and the second | 2 | 1.9 | - 1 | 15 | 1.93 | | | 1 | 0.53 | | | 1 1 |
| | S | | | | 2.89 | 1 | | - 1 | 0.80 | | | 2 |
| | 4 | 3.8 | | - 8 | 3.86 | | | 5 | 1.07 | 3.88 | | 1 1 |
| | 5 | 4.8 | | 29 | 4.82 | 1.3 | 2 4.8 | 2 | 1.34 | 4.81 | 1.36 | 5 |
| The state of the s | 6 | 5.80 | 0 1.5 | 55 | 5.79 | 1.5 | 8 5.7 | 8 | 1.60 | 5.77 | 1.63 | 6 |
| | 7 | 6.7 | 6 1.8 | 1 | 6.75 | 1.8 | 4 6.7 | 5 | 1.87 | 6.74 | 1.90 | 1 1 |
| 1. | 3 | 7.73 | 1. | | 7.72 | 1 | - 5 | 1 | 2.14 | | | 1 5. |
| | 9 | 8.69 | 1 | - 2 | 8.68 | | 3 | - 1 | 2.41 | 1 | | 1 6 |
| 1 | 0 | 9.66 | $\begin{bmatrix} 2 & 5 \end{bmatrix}$ | 9 | 9.65 | 2.6 | $\frac{3}{9.6}$ | 4 | 2.67 | 9.62 | 2.71 | 10 |
| 1 | 1 | 10.63 | $3 \left[2.8 \right]$ | 5 1 | 0.61 | 2.8 | 9 10.6 | | | 10.59 | | E . |
| - 1 | - | 11.59 | | | 1.58 | | 6 11.5 | 1 | 3.21 | 1 | | 1 1 |
| - 1 | - 1 | 12.56 | | 2 | 2.54 | 1 | 212.5 | - 1 | , | 12.51 | 1 | 1 Es |
| 100 | - 1 | 13.52 | | 2 | 3.51 | | 3113.4 | | | 13.47 | | |
| | ٠. | 14.49 | | | 4.47 | 1 | 14.4 | | | 14.44 | | 1 1 |
| | - 6 | 15.45 | 1 | 5 | 5.44 | 1 | 15.4 | - i | - 4 | 15.40 | | . 5 |
| | - 1 | 16.42 | | H | | 1. | 116.3 | - | | 16.36 | | ii |
| - | - 1 | 17.39 | 1 . | - 2 | | | 317.3 | | | 17.32 18.29 | | 1 5 |
| | -1 | 18.3 <i>5</i> 19.32 | | | 9.30 | t | 18.3 | - 1 | | 19.25 | | 1 5 |
| - | -i · | | - | . ž | | | \$ | - 1- | | | - | |
| | - | 20.28 | 3 1 | 3 | 0.26 | | 20.24 | | | 20.21 21.17 | 5.70 5.97 | |
| j . | - 2 | 21.25 22.22 | | | .23 | | 21.20 | ì | | 22.14 | | 1 5. |
| 1.0 | 1 | 3.18 | | - | .15 | | 23.13 | | | 23.10 | 1 | |
| 1 | 1 - | 4.15 | 1 | 8 _ | .12 | | 24.09 | -1 | | 24.06 | | |
| ÿ - | | 5.11 | 1 | 延 | .08 | | 25.03 | | | 25.02 | | 1 4 |
| 1 | | 6.08 | 1 | B | | | 26.02 | | | 25.99 | 1 | 1 21 |
| i i | | 7.05 | 1 | 18 | | | 26.98 | - | 7.48 | 26.95 | 1 | |
| 29 | 2 | 8.01 | 7.5 | 127 | .98 | | 27.9 | _ | 7.75 | 27.91 | 7.87 | 29 |
| 30 | 1,2 | 8.98 | 7.76 | 5 28 | .94 | 7.89 | 28.91 | | 8.02 | 28.87 | 8.14 | 30 |
| 31 | 2 | 9.94 | 8,02 | 29 | 91 | 8.15 | 29.87 | - | 8.28 | 29.84 | 8.41 | 31 |
| 32 | 3 | 0.91 | 8.28 | 3,30 | 87، | 8.42 | 30.84 | Į. | 8.55 | 30.80 | 8.69 | 32 |
| 33 | 3 | 1.88 | 8.54 | 3.1 | .84 | 8.68 | 31.80 | | | 31.76 | | 33 |
| 1 | 1 | 2.84 | . 8.80 | 132 | .80 | 8.94 | 32.76 | | | 32.72 | 11 | a. |
| 1 | 1 | 3.81 | 9.06 | 5 | | 9.21 | 33.73 | | | 33.69 | | - 4 |
| | 1 | 4 77 | | | | | 34.69 | - 1 | | 34.65 | | |
| | 10 | 5.74 | | - 10 Y | | | 35.65 | 1 | | | 10.04 | |
| 1 | .i | 6.71 | 9.84 | 7 | | | 12 | | | | 10.31 | |
| Ý. | 1 | 7.67 | | R . | | | -0 | | | | 10.59 | |
| ļ | . | 8.64 | | 5 | | - | | . ! | <u> </u> | | 10.86 | |
| • | | | | | | | | 5.0 | 13 | | | 114 |
| 1 | | | | | | | , | | | | 11.40 | |
| | | | | | | | | | | | 11.67 | - 4 |
| | | | | | | | (| | | | 11.94 | |
| | | | | - | | | | | | | 12.21 | |
| | | | | - RG | | | | | | | 12.49 | |
| | • | | | 3 | | | 46.25 | 1 | 2 | - 1 | 13.03 | |
| | | | | R 6 | | | | 1 | E . | | 13.30 | |
| | . 5 | | | | | | | | | 48.12 | | 50 |
| 11 | | - | - | i | i . | | Dep. | 1 | | Dep. | | ٠ |
| Dis | - | 750 | | 74 | | 45' | 740 | | 30' | | 15' | 018 |
| Samuel of | - | | | | | | | _ | | • • | 13 | The same of |

| ,16 | Deg | • | TRA | VER | SE T | ABLE | | 100 | 99 |
|------|-----------------------|----------------|----------------|--------------|----------------|-------------|----------------|--------------|----------|
| 10 | 160 | 0'. | 16° | 15' | 16° | 30' | 16° | 45' | Di |
| ist | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | st. |
| 1 | 0.96 | 0.28 | 0.96 | 0.28 | 0.96 | 0.28 | 0.96 | 0.29 | 1 |
| 2 | 1.92 | | | 13 | 9 | 0.57 | | 0.58 | 2 |
| 3 | | | | | | 100 | | 0.86 | |
| 4 | | j . | X | | | | | 1.15 | 4 |
| 5 | 4.81 | | | 1.40 | | | | 1.44 | 5 |
| 6 | | f | | 1.68 | | 7 | | 1.73 | |
| 7 | | | | 1.96 2.24 | | | | 2.02 2.31 | 8 |
| 8 9 | 8.65 | | | | | 2.27 2.56 | | 2.59 | |
| 30 | | 2.76 | | 2.80 | | 2.84 | | 2.88 | |
| | 10.57 | | 10.56 | | 10.55 | | 10.53 | 3.17 | 11 |
| 11 | 11.54 | | 11.52 | | 11.51 | | 11.49 | 3.46 | |
| 13 | | | 12.48 | | 12.46 | | 12.45 | 3.75 | 13 |
| 14 | 13.46 | | 13.44 | | 13.42 | | 13.41 | 4.03 | |
| 15 | 14.42 | | 14.40 | | 14.38 | | 14.36 | 4.32 | |
| 16 | 15.38 | | 15.36 | | 15.34 | | 15.32 | 4.61 | |
| 17 | 16.34 | | 16.32 | | 16.30 | N N | 16.28 | 4.90 | |
| 18 | 17.30 | 4.96 | 17.28 | 5.04 | 17.26 | 5.11 | 17.24 | 5.19 | |
| 19 | 18.26 | 5.24 | 18,24 | | 18.22 | 5.40 | 18.19 | 5.48 | 19 |
| 20 | 19.23 | 5.51 | 19.20 | 5.60 | 19.18 | 5.68 | 19.15 | 5.76 | 20 |
| 121 | 20.19 | 5.79 | 20.16 | 5.88 | 20.14 | 5.96 | 20.11 | 6.05 | 6 |
| 22 | | | 21.12 | | 21.09 | 6.25 | 21 07 | 6.34 | |
| 23 | 22.11 | | 22.08 | | 22.05 | | 22.02 | 6 63 | |
| | 23.07 | | 23.04 | | 23.01 | | 22.98 | 6.92 | |
| 1 1 | 24.03 | | 24.00 | | 23.97 | | 23.94 | 7.21 | |
| | 24.99 | | 24.96 | | 24.98 | | 24.90 | 7.49 | |
| 1 | 25.95 | | 25.92 | | 25.89 | | 25 85 | 7.78 | 7 |
| 1 1 | 26.92 | | 26.88 | | 26.85 | | 26.81 | 8.07 8.36 | |
| 4 1 | 27.88 | . 1 | 27.84 28.80 | | 27.81 28.76 | 2 | 27.77 28.73 | 8.65 | |
| | $\frac{28.84}{28.84}$ | | | | | | | - | |
| 10-1 | | | 29.76 | | 29.72 | | 29.68 | 8.93 9.22 | - |
| | 30.76 | | 30.72 31.68 | | 30.68 31.64 | i i | 30.64 31.60 | 9.51 | - 1 |
| | 31.72 32.68 | | 32.64 | | 32.60 | | 32,56 | 9,80 | |
| | 33.64 | | 33.60 | | 33.56 | | 33.51 | 10.09 | |
| | 34.61 | | 34.56 | | | | 34.47 | 10.38 | |
| 1. 1 | 35.57 | 0.00 | | | 35.48 | | | 10.66 | |
| | 36.53 | | | | 36.44 | | | 10.95 | 38 |
| | 37.49 | | 37.44 | | | 11.08 | | 11.24 | |
| | 38.45 | | 38.40 | 11.19 | 38.35 | 11.36 | 38.30 | 11.53 | 40 |
| 4 4 | | and the second | 39,36 | 11.47 | 39.31 | 11.64 | 39.26 | 11.82 | 41 |
| 42 | 40.37 | 11.58 | 40.32 | 11.75 | 40.27 | 11.93 | 40.22 | 12.10 | |
| 43 | 41.33 | 11.85 | 41.28 | 12.03 | 41.23 | 12.21 | 41.18 | 12.39 | 43 |
| 44 | 42.30 | 12.13 | 42.24 | 12.31 | 42.19 | 12.50 | 42.13 | 12.68 | 44 |
| 45 | 43.26 | 12.40 | 43.20 | 12.59 | 43.15 | 12.78 | 43.09 | 12.97 | 45 |
| 46 | 44.22 | 12.68 | 44.16 | 12.87 | 44.11 | 13.06 | 44.05 | 13.26 | 46 47 |
| | | | | | 45.06 | | | 13.55 | 48 |
| | | | | | 46.02 | | 45.96 | 13.83 | 49 |
| | | | | | 46.98 | | 46.92 | 14.41 | 50 |
| 50 | 48.06 | 13.78 | 48.00 | 13.99 | 47.94 | 14.20 | Don | | 3 |
| ist. | Dep. | Lat. | Dep. | Lat. | Dep. 73° | Lat. | 700 | 152 |)is |
| 10 | 740 | 01 | 730 | 45' | 73 | 30' | 113 | | handy! |

| 100 | | | RAVI | | | | . =0 | $\frac{17}{2}$ | eg. |
|---------|----------------|-------|-------|-------|----------|-------|--------|----------------|------|
| 10 | 170 | U' | 170 | 15' | 17° | 30' | 170 | 45' | |
| ist. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | De p. | 18 |
| 1 | 0.96 | 0.29 | 0.96 | 0.30 | 0.95 | 0.30 | 0.95 | 0.30 | 1 |
| 2 | 1.91 | 0.58 | 1.91 | 0.59 | 1.91 | 0.60 | 1.90 | 0.61 | 2 |
| 3 | | 0.88 | 2.87 | 0.89 | 2.86 | 0.90 | 2.86 | 0.91 | 3 |
| 4 | | 1.17 | | | | 1.20 | | 1.22 | 4 |
| 5 | | 1.46 | | | | | 2 1 | 1.52 | 5 |
| 6 | | | | | | | | 1.83 | 6 |
| 7 | 1 . | 2.05 | | 2.08 | 4 | | 3 | 2.13 | 7 |
| 8 | 7.65 | 2.34 | | 2.37 | 9 | | | | 8 |
| 9 | 8.61 | 2.63 | | | 3 | | 3 5 | | 9 |
| 110 | 9.56 | 2.92 | | 2.97 | | | | | 10 |
| <u></u> | | | | | | | 10.48 | | 11 |
| 111 | 10.52 | | 10.51 | | 10.49 | | | 0.00 | 12 |
| 12 | 11.48 | | 11.46 | | 11.44 | | 11.43 | | |
| 13 | | | 12.42 | | 12.40 | | 12.38 | | 13 |
| 14 | 13.39 | | 13.37 | k: | 13.35 | | 13.33 | | 14 |
| 115 | 14.34 | | 14.35 | 3 | 14.31 | | 14.29 | | 15 |
| 16 | 15.30 | | 15.28 | | 15.26 | | 15.24 | | 16 |
| | 16.26 | | 16.24 | | 16.21 | | 16.19 | 4 | 17 |
| 118 | | | 17.19 | , | 17.17 | | 17.14 | 4 | 18 |
| 19 | 18.17 | | 18.15 | | 18.12 | | 18,10 | į . | 19 |
| 20 | 19.13 | 5.85 | 19.10 | 5.93 | 19.07 | 6.01 | 19.05 | 6.10 | 20 |
| 21 | 20.08 | 6.14 | 20.06 | 6.23 | 20.03 | 6.31 | 20.00 | 6.40 | 21 |
| 22 | 21.04 | 6.43 | 21,01 | 6.52 | 20.98 | 6.62 | 20.95 | 6.71 | 22 |
| 23 | 21.99 | 6.72 | 21.97 | 6.82 | 21.94 | 6.92 | 21.91 | 7.01 | 23 |
| 24 | 0000 | | 22.92 | | 22.89 | | 22.86 | | 24 |
| 25 | 00 01 | | 23.88 | 1 . | 23.84 | | 23.81 | | 25 |
| | 24.86 | | 24.83 | | 24.80 | | 24.76 | | |
| | 25.82 | | 25.79 | | 25.75 | | 25.71 | | |
| 28 | 0 | | 26.74 | | 26.70 | | 26.67 | | - 1 |
| | 27.75 | | 27.70 | | 27.66 | | 27.62 | | 1 |
| 30 | 28.69 | 5 | 28.65 | | 28.61 | | 28.57 | | SO, |
| 31 | 29,65 | | 29.61 | | 29.57 | - | 29.52 | - | 31 |
| 32 | | | 30.56 | | | | 30.48 | | 32 |
| | 31.56 | | 31.52 | | 30.52 | | | | 33 |
| | 32.51 | | | | 31.47 | | 31.43 | | 1 1 |
| | 33.47 | | ę , | | | | \$2.38 | | 34 |
| | 34.43 | | 54.38 | | | | 33,33 | | 35 |
| - | | | | | | | 34,29 | | 36 |
| 37 | 35.38 36.34 | | | | | | | | 37 |
| 1 | | | | | | | 36.19 | | 38 |
| 39 | | | 37.25 | 11.57 | 37.20 | 11.73 | 37.14 | 11.89 | 39 |
| 40 | | | | | | 7 | 38.10 | | 40 |
| 41 | 39.21 | | | | | | 39.05 | | 41 |
| 42 | 40.16 | | | | | | | | 2 . |
| 43 | 41.12 | 12.57 | 41.07 | 12.75 | 41.01 | 12.93 | 40.95 | 13,11 | 43 |
| 44 | 42 08 | 12.86 | 42.02 | 13.05 | 41.96 | 13,23 | 41.91 | 13.41 | 44 |
| 45 | 43.03 | 13.16 | 42.98 | 13.34 | 42.92 | 13.53 | 42.86 | 13.72 | 45 |
| 46 | | 13.45 | 43.93 | | | | 43,81 | | 46 |
| 47 | 44.95 | 13.74 | 44.89 | | | | 44.76 | | 47 |
| 48 | 45.90 | 14.03 | 45.84 | 14.23 | 45.78 | 14.43 | 45.79 | 14 63 | |
| 49 | 46.86 | 14.33 | 46.80 | 14.53 | 46.73 | 14.73 | 46.67 | 14.94 | 49 |
| 50 | 47.82 | 14.62 | 47.75 | | | | 17.62 | | |
| 17 | Dep. | Lat. | | | Dep. | | Dep. | Lat. | |
| Dist | 730 | 0, | 720 | 45' | 720 | 201 | 700 | 12/ | Dist |
| | | | - ~ | TJ | 12 | 30' | 4 | 15' | 1 |

| | 0. | Deg. | | | LRSE | | BLE: | | | 01 | : |
|---|-------|---|--|-------|--|----------|--|--------|------------|-----------------|-----|
| 1 | ·Di | 180 | ()/ | 180 | 15' | 18° | 30' | 150 | 45' | DI | |
| 1 | St. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | 31. | |
| 1 | 1 | 095 | 0.31 | 0.95 | 0.31 | 0.95 | 0.32 | 0.95 | 0.32 | 1 | |
| | 2 | 1.90 | 0.62 | 1.90 | 0.63 | 1.90 | 0.63 | 1.89 | 0.64 | 2 | |
| I | 3 | 2.85 | 0.93 | 2.85 | 0.94 | 2.84 | 0.95 | | | 3 | |
| 1 | 4 | 3.80 | 1.24 | 3 80 | | 3.79 | 1.27 | | | 4 | |
| | 5 | 4.76 | 1.55 | 4.75 | 1.57 | | | | 1 1 | 5 | |
| - | 6 | 5.71 | 1.85 | 5.70 | 1.88 | | | | 3 1 | 6 | |
| 1 | 7 | 6.66 | 2.16 | | 2.19 | | | | | 7 | |
| 1 | 8 | 7.61 | 2.47 | 7.60 | 2.51 | | | | | 8 | |
| | 9 | 8.56 | 2.78 | 8.55 | 2.82 | | 100 | _ | 1 | 9 | ۰ |
| | 10 | | 3.09 | 9.50 | 3.13 | | | 9.47 | | 10 | |
| 1 | | | | | | | | - | | | 1 |
| 1 | | 10.46 | | 10.45 | | 10.43 | | 10.42 | | | |
| | | 11.41 | | 11.40 | | 11.38 | | 11.36 | | | |
| | | 12.36 | | 12.35 | | 12.33 | | 12.31 | | . , | 1 |
| | | 13.31 | | 13.30 | | 13.28 | | 13.26 | | | ŧ. |
| | | 14.27 | | 14.25 | | 14.22 | | 14.20 | 1 | 1 | k. |
| | | 15.22 | | 15.20 | | 15.17 | | 15.15 | | | |
| ľ | | 16.17 | | 16.14 | | 16.12 | | 16.10 | | | |
| 1 | | 17.12 | | 17.09 | | 17.07 | | 17.04 | 1 | 18 | 1 |
| | | 18.07 | | 18.04 | | 18.02 | | 17.99 | | 19 | 1 |
| d | 20 | 19.02 | 5.18 | 18.99 | 6.26 | 18.97 | 6.35 | 18.94 | 6.43 | 20 | 1 |
| | 21 | 19.97 | 6.49 | 19.94 | 6.58 | 19.91 | 6,66 | 19.89 | 6.75 | $\overline{21}$ | - |
| | 22 | 20.92 | 6.80 | 20,89 | 6.89 | 20.86 | 6.98 | 20.83 | 7.07 | 22 | ŀ |
| | 23 | 21.87 | | 21.84 | 7.20 | 21.81 | 7.30 | 21.78 | | 1 | 1 |
| | 24 | 22.83 | | 22.79 | 1 1 | 22.76 | | 22.73 | | 24 | 1 |
| | | 23.78 | 1 | 23.74 | | 23.71 | | 23.67 | | 1 | 1 |
| | | 24.73 | | 24.69 | | 24.66 | | 24.62 | 1 | 1 | 7 |
| | | 25.68 | | 25.64 | | 25.60 | | 25.57 | 1 | 1 | 1 |
| | | 26.63 | | 26.59 | | 26.55 | | 26.51 | | 1 | |
| | | 27.58 | 4 | 27.54 | | 27.50 | | 27.46 | | | ŧ. |
| | | 28.56 | | 28.49 | - 1 | 28.45 | | 28.41 | | 1 | 1 |
| | - | 39.48 | 1 | | | * | - | ž | | - | . [|
| | | 30.43 | | 29.44 | | 29.40 | | 29.35 | 9.96 | 1 | 1 |
| 1 | | 31.38 | | | | 4 | 1 | | | 1 | 1 |
| - | | 1 | | | | | | | 10.61 | | 1 |
| | 35 | 22.34 | 10.51 | 32.29 | 10.05 | 202.29 | 10.79 | 02.1 | 111.93 | 34 | |
| | 36 | 34.24 | | | | | | | 11.25 | | |
| | | 1 | 2 1 | | | | | | 11.57 | | 1 |
| | 3.8 | 36.14 | 11.43 | 35.14 | 11.59 | 35.08 | 11.74 | 125.04 | 111.89 | 37 | 1 |
| | 39 | 37.00 | 19.05 | 30.09 | 11.90 | 26.00 | 112.06 | 32.95 | 12.21 | 38 | - 1 |
| | 40 | 36 01 | 12.05 | 37.04 | 12.21 | 30,93 | 12.57 | 130.91 | 12.54 | 39 | - |
| | | - | | | | 3 | | 9 | 12.86 | | -1 |
| | 41 | 38.99 | 12.67 | 38.94 | 12.84 | 38.88 | 13.01 | 38.82 | 13.18 | 4] | 3 4 |
| | 42 | 39.94 | 12,98 | 39.89 | 13.15 | 39.83 | 13.33 | 39.77 | 13.50 |) 42 | - 1 |
| | 43 | 40.90 | 13.29 | 40.84 | 13.47 | 40.78 | 13.64 | | 2 13.82 | | . 1 |
| | 44 | 41.85 | 13.60 | 11.79 | 13.98 | 41.73 | 13.96 | | 5 14.14 | | - { |
| | 45 | 42.80 | 13.91 | 42.74 | 14.09 | 42.67 | 14.28 | 42.6 | 1 14.46 | 45 | ٠. |
| | 46 | 43.75 | 14.21 | 43.69 | 14.41 | 43.62 | 14.60 | 43.5 | 5 14.79 | 46 | 7 |
| | 47 | 44.70 | 14.52 | 44.64 | 14.72 | 44.57 | 14.91 | 44.5 | 1 [5.1] | 4.7 | |
| | 48 | 1450.00 | 14.89 | 45.59 | 15.03 | 45.52 | 15.23 | 100 | 15.43 | | - # |
| | 149 | 46.60 | 15.14 | 46.54 | 15.34 | 46.47 | 15.55 | | 15.75 | | |
| | 50 | 47.55 | 15.45 | 47.48 | 15.66 | 47.42 | 15.86 | 47.35 | 5 16.07 | 50 | 1 |
| | 1 | Dep. | | Dep. | 1 | | . 1 | Dep. | | st. | 1 |
| | Dist. | 720 | | | 45' | - | | 710 | The second | . Sig | 1 |
| | 1-4 | CONTRACTOR OF THE PARTY OF THE | STATE OF THE PARTY | y A | To the same of the | - | and the second s | - | - | Managaran A. | * |

| 1:20 | | | | PESI | | DLE | | | CS. |
|-------|--------|------|-----------------|-------|----------------|-------|----------|--------------|-----|
| Dist | 199 | 0' | 19 | | 190 | इ0' | 10 | 45' | 5 |
| 138 | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | st |
| 1 | 0.95 | 0.33 | 0.94 | 0.33 | 0.94 | - | | 0.34 | 1 |
| 2 | 1.89 | 0.65 | 1.85 | 0.66 | 1.89 | | ij . | 0.68 | 2 |
| 3 | 2.84 | 0.98 | 2.83 | 0.99 | 2.83 | 1.00 | 0 2.82 | 1.01 | 3 |
| 4 | 3.78 | 1.30 | 3.78 | 1.32 | 3.77 | 1 34 | 4 | | 4 |
| 5 | 4.73 | | G . | 1.65 | 4.71 | 1.67 | 4.71 | 1.69 | 5 |
| . 6 | 5.67 | 1.95 | 5.66 | 1.98 | 5.66 | 2.00 | 5.65 | 2 03 | 6 |
| 7 | 6.62 | 2,28 | 6.61 | 2.31 | 6.60 | 2.34 | 6.59 | 2.37 | 7 |
| 8 | 7.56 | 2.60 | 7.55 | 2.64 | 7 54 | 2.67 | 7.53 | 2.70 | 8 |
| 9 | 8,51 | 2.93 | 8.50 | 2.97 | 8 48 | 3.00 | 8.47 | 3.04 | 9 |
| 10 | 9.46 | 3.26 | 9.44 | 3.30 | 9.43 | 3.34 | 9.41 | 3.38 | 10 |
| 11 | 10.40 | 3.58 | 10.38 | 3.63 | 10.37 | 3.67 | 10.35 | 3.72 | 11 |
| | 11.35 | | 11.33 | 1 | 11.31 | | 11.29 | i | 1 1 |
| 1 | 12.29 | | 12.27 | | 12.25 | - 1 | 12.24 | | 1 1 |
| | 13.24 | | 13.22 | 1. | 13.20 | | 13.18 | 1 | 1 1 |
| 3 1 | 14.18 | | 14.16 | | 14.14 | | 14.12 | 1 | |
| 1. 1 | 15.13 | | 15.11 | 1 | 15 08 | 1. | 15.06 | | 16 |
| 1 | 16.07 | | 16.05 | | 16.02 | | 16.00 | | 1 1 |
| 1 | 17.02 | | 16.99 | | 16.97 | | 16.94 | 6.08 | 1 2 |
| | 17.96 | | 17.94 | | 17.91 | | 17 88 | | 3 6 |
| 1 1 | 18.91 | | 18.88 | | 18 85 | | 18.82 | 6.76 | 1 1 |
| | | | 19.83 | | 19.80 | - | <u> </u> | | |
| 3 1 | 19 86 | | 20.77 | 1 | 20.74 | | 19.76 | 7.10 7.43 | - 1 |
| 1. 9 | 20.80 | | 21.71 | | 21.68 | | 20.7 | 7.77 | 23 |
| | 21.75 | | 22.66 | | 21.68 22.62 | | 21.65 | | 24 |
| 1 | 22.69 | | | | | | 22.59 | 8.11 | 1 1 |
| | 23.64 | | 23.60 24.55 | | 22.57 | | 23.53 | 8.79 | |
| | 24.58 | | | | 24.51 25.45 | | 24.47 | 9.12 | |
| | 25.53 | | 25.49 26.43 | | | | 25.41 | | |
| | 26.47 | R | 20.43 27.38 | | 26.39 | | 26.35 | 9.46 | 29 |
| 1 7 | 27.42 | | 27.36 28:35 | | 27.34 28.28 | | 27.29 | | 30 |
| | 8.37 | | | ~ | | 10.01 | | | |
| 5 | 9.31 | | | 10.22 | | | 29.18 | 10.48 | |
| 3 | - 1 | | | 10.55 | | 10.68 | | | 32 |
| 1 | | | | 10.88 | | 11.02 | | | 33 |
| ž . | | | | Ö | 32.05 | N N | 32.00 | | 34 |
| | 3.09 | h. | 1 | 11.54 | | 11.68 | | 11.83 | 35 |
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| | | 2 | 1 | | 34 88 | | | 12,50 | |
| | 3 | R | | 12.53 | 4 | | 35.76 | | , |
| | 1 | - 4 | | 12.86 | | ï | | | 39 |
| 40.3 | 7.82 1 | 3.02 | 37.76 | 13.19 | 37.71 | 13.35 | 37 65 | 13.52 | 40 |
| 413 | 8.77 1 | 3.35 | 38.71 | 13.52 | 38.65 | 13.69 | 38.59 | 13.85 | 41 |
| 423 | 9.711 | 3.67 | 39.65 | 13.85 | 39.59 | 14.02 | 39.53 | 14.19 | 42 |
| 43 4 | 0.661 | 4.00 | 40.60 | 14.18 | 40.53 | 14.35 | 40.47 | 14.53 | 43 |
| | | | | | | 14.69 | | | 44 |
| | | | | _ | 4 | | 42.35 | 15.21 | 45 |
| 46 4: | 3.491 | 4.98 | 43,43 | 15.17 | 43.36 | 15.36 | 43.29 | 15.54 | 4.6 |
| | | 100 | | | | 15.69 | | 15.88 | 47 |
| . 1 | 1 | B. | | - 2 | | | 45.18 | | 48 |
| 49 4 | 6.33 1 | 5.95 | | | | 16.36 | | | 49 |
| | | - 4 | | 16.48 | | 16.69 | | | 50 |
| | Dep. | | | Lat: | Dep. | Lat. | Dep. | Lat. | st. |
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| | | | | | , , | , | | | -1 |

| 360 | | | | VER | ISE 1 | ABL | 15. | | 103 |
|-------|---------------|-------|-------|-------|--------|-------|---------|--------|--------|
| | Z) 20° | () | 200 | 151 | 20 | ° 30' | 200 | 45' | J |
| | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | 181. |
| - (- | 1 0.94 | - | | | | | M | - | - |
| | 2 1.88 | | | 1 | | | 7 | 0.35 | 1 |
| 1 | 3 2.82 | | | | | | 1 | 0.71 | 2 |
| - 1 | | | | | 1 | | 9 | 1.06 | 1 8 |
| - } | 4 3.7€ | | _ | _ | | | 3 | | 1 1 |
| - 1 | 5 4.70 | 1 | 74 | | | 1.75 | 2 | | 1 2 |
| - 1 | 6 5 64 | 2.05 | 5.63 | | n o | 2.10 | 5.61 | 2.13 | |
| L | 6.58 | 2.39 | 6.57 | 2.42 | 6 56 | 2.45 | 6.55 | 2.48 | 7 |
| r | 8 7.52 | 2.74 | 7.51 | 2.77 | 7.49 | 2.80 | 7.48 | 2.83 | 8 |
| | 9 8.48 | 3.08 | 8.44 | 3.12 | | | 8.42 | 3.19 | 9 |
| 11 | 9.40 | 3.42 | 9.38 | 3.46 | | | 9.35 | 3.54 | 10 |
| 1 | - | - | 10.32 | 3 81 | 10.30 | 1 | 10.29 | 3.90 | 11 |
| 1: | 1 2 | 1 | 11.26 | | 11.24 | | 9 | | |
| | | | | | | | 11.22 | | 1 8 |
| 12 | | | 12.20 | | 12.18 | | 12.16 | | 13 |
| 3 | | 1 | 13.13 | | 113.14 | 4,90 | 13.09 | | 1 . 6 |
| 13 | | | 14.07 | 5.19 | 14.05 | 5.25 | 14.03 | | 15 |
| 110 | | | 15.01 | 5.54 | 14.99 | 5.60 | 14.96 | | 1 1 |
| 17 | 1 - 5 - 5 - 1 | 1 | 15.95 | 5.88 | 15.92 | 5.95 | 15.90 | | 1 5 |
| 118 | | | 16.89 | 6.23 | 16.86 | 6.30 | 16.83 | 6.38 | . 3 |
| 113 | 17.85 | _ | 17.83 | 6.58 | 17.80 | 6.65 | 17,77 | 6.73 | 19 |
| 20 | 18.79 | 6.34 | 18.76 | 6.92 | (8.73) | 7.00 | 18.70 | 7.09 | 20 |
| 2 | 19.73 | 7 18 | 19.70 | | 19.67 | | 19.64 | 7.44 | 21 |
| 22 | 1 | | 20.64 | | 20.61 | | 20.57 | 7.79 | |
| 23 | | 1 | 21.58 | | 21.54 | | 21.51 | 8.15 | 3 |
| 1 | 22.55 | : | 22.52 | | 22.48 | | 22.44 | 8.50 | |
| 1_ | | - 3 | 23.45 | | 23.42 | | | 8.86 | 42 |
| | 23.49 | | | | | | 23,38 | 9.21 | 26 |
| | 24.43 | | | | 24.35 | 9.11 | 24.31 | | 2 |
| 1 | 25.37 | - 1 | | 0.60 | 25.29 | 9.40 | 25.25 | 9.92 | 28 |
| 1 | 26.31 | E | 26.27 | | 26.23 | | 26.18 | | 29 |
| | 27.25 | - 4 | 27.21 | | | | 27.12 | 10.27 | 1 |
| 30 | 28.19 | | | | | | 28.05 | 10.63 | 30 |
| 31 | 39.13 | 10.60 | 29.08 | 10.73 | 29.04 | | | | 31 |
| 32 | 30.07 | 10.94 | 30.02 | 11.08 | 29,97 | 11.21 | 29.92 | 11.34 | |
| 33 | 31.01 | 11.29 | 30.96 | 11.42 | 30,91 | 11,56 | 30.86 | 11.69 | 33 |
| 34 | 31.95 | 11.63 | 31,90 | 11.77 | 31.85 | | 31.79 | 12.05 | 34 |
| | 32.89 | 14 | | | | | 32.73 | | 35 |
| | 33.83 | | | | | | | 12.75 | 36 |
| | 34.77 | | | | | | 34.60 | 13.11 | 37 |
| | 35.71 | | | | | | 35.54 | | 38 |
| 39 | | 100 | 36.59 | | | | | 13.82 | 39 |
| 40 | | | 37.53 | | | | | 14.17 | 40 |
| - | | | | | | | | | 41 |
| 41 | | 13 | 38.47 | | | | 38.34 | | 42 |
| | 39.47 | 2 | | | , | 9. | 39.28 | 1 1.00 | 4 |
| 143 | 40.41 | N. | | | | 2 | | 15.23 | 43 |
| 44 | | 19 | 41.28 | - | | | | | 4.4 |
| 45 | 42,29 | 15.39 | 42.22 | 15.58 | 42.15 | 15.76 | التناشا | 15.94 | 45 |
| 46 | 43.23 | 15.73 | 43,16 | 15.92 | 43.09 | 19 | | - 0.00 | 46 |
| 47 | 44.17 | 16.07 | 44.09 | 16.27 | 44.02 | 16.46 | | 16.65 | 47 |
| 48 | 45.11 | 13 | 45.03 | | | | | 17.01 | 48 |
| 49 | | 2 | 45.97 | 16.96 | 45.90 | | | | 49 |
| 50 | | | , , | 15 | | 9 | 46.76 | 17.71 | 50 |
| | Dep. | 3 | Dep. | 6 | | | Dep. | Lat. | 3.t. |
| ist. | | | | | | | | | 0.15 |
| 12 | 70° | 0 | 69° | 45 | . 69 | 30' | 690 | 15′ i | prod I |
| 1 | | | | | | | | | |

| 10 | | | TRAVERSE | | | | | | |
|-----|----------------|-------|----------------|-------|---------------|--------------|----------------|--------------|----------|
| 15 | | 0' | 210 | 15' | 210 | 30' | 21° | 45' | |
| St | - | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | St |
| | 1 0.50 | 1 | | | 0.93 | 0.37 | 0.93 | 0.37 | 1 |
| 2 | | | | | 1.86 | 0.73 | 1.86 | 0.74 | 2 |
| 4 | | | | | 1 | 1.10 | 2.79 | 1.11 | 3 |
| 5 | | | | | | | 3.72 | 1.48 | 4 |
| 6 | | | | | | 1.83 2.20 | 4.64 5.57 | 1.85 | 5. |
| 7 | | | _ | | | 2.57 | | 2.59 | 7 |
| 8 | 1 | 100 | | | | 2.93 | | 2.96 | 8 |
| 9 | • | | | | | 3.30 | | 3.34 | 9 |
| 10 | 9.34 | | | 1 | | 3:67 | 9.29 | | 10 |
| 11 | 10.27 | 3.94 | 10.25 | 3.99 | 10.23 | 4.03 | 10.22 | 4.08 | 11 |
| 12 | | • | 11:18 | | 11.17 | 4,40 | | 4.45 | 12 |
| 13 | 12.14 | | 12.12 | | 12.10 | | 12.07 | 4.82 | 13 |
| 14 | 13.07 | 5.02 | 13.05 | 5.07 | 13.03 | 5.13 | 13.00 | 5.19 | 14 |
| 15 | | 5.38 | 13.98 | 5.44 | 13.96 | 5.50 | 13.93 | 5.56 | 15 |
| 16 | 11 | | 14.91 | 1 | 14.89 | | 14.86 | 5.93 | 16 |
| 17 | | | 15.84 | | 15.82 | | 15.79 | 6.30 | 17 |
| 18 | | | 16.78 | | 16.75 | | 16.72 | 6.67 | 18 |
| 119 | 1 | | 17.71 | 1 | 17.68 | | 17.65 | 7.04 | 19 |
| 20 | | 1 | 18.64 | | 18.61 | · | 13.58 | 1 1 4 4 | 20 |
| 21 | | | 19.57 | | | | 19,51 | 7.78 | 21 |
| 22 | | | 20.50 | | 20.47 | | 20.43 | 8.15 | 22 |
| 23 | | 1 | 21.44 | | 21.40 22.33 | | 21.36 | 8.52 8.89 | 201 |
| | 22.41 | | 22 37 23.30 | | 23.26 | | 22.29 | | 25 |
| | 24.27 | | 24.23 | | 24.19 | | 23 22 24.15 | | 26 |
| | 25.21 | 1 | | | | | 25.08 | | 27 |
| | 26.14 | | | | | | | | |
| 29 | 27.07 | 10.39 | 27.03 | 10.51 | 26.98 | 10.63 | 26.94 | 10.75 | 29 |
| | 28.01 | 10.75 | 27.96 | 10.87 | 27.91 | 11.00 | 27.86 | 11.12 | 30 |
| 31 | 28.94 | 11.11 | | | | | 2 | | 31 |
| 32 | 29.87 | 11.47 | 29.82 | 11.60 | 29.77 | 11.73 | 29.72 | 11.86 | 32 |
| 33 | 30.81 | 11.83 | 30.76 | 11.96 | 30.70 | 12.09 | 30.65 | 12.23 | 33 |
| | 31.74 | | | | | | | | 34 |
| | 32.68 | | | | | | | | 35 |
| | 33.61 | | | | | | | 13.34 | 36 |
| | 34.54 | | | | | 3 | | 13.71 | 37 |
| | 35.48 | | | | | | | | 38 |
| | 36.41 | | | | 6 | | | | 39 40 |
| 40 | | 14.33 | | | | | | 1 | 1 |
| 41 | | 14.69 | | | | | 38.08 | 15.19 | 41 |
| | 39.21 | | | | | | 39.01 | 15.56 | 42 |
| | 40.14 | | | | | | | | |
| 44 | 41.08 42 01 | | | | | | 40.87 41.80 | | 45 |
| 46 | | 16.13 | | | | | | | |
| 47 | | 16.49 | | | | | | | 1 1 |
| 48 | 44.81 | 17.20 | 44.74 | 17.40 | 44.60 | 17.59 | 44.5 8 | 17 70 | 48 |
| 49 | | 17.56 | | | | 17.96 | 45.51 | 18-16 | |
| 50 | | 17.92 | | | | | 46.44 | | 50 |
| | Dep. | i | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | 回 |
| Dis | 69° | 0' | 68° | 45' | 68° | 30' | 68° | 15' | 15t |
| - 0 | · | | | | | | 00 | | *** |

| | 22 | Deg | | TRA | VER | SE T | ABLE | I. | _1 | 95 |
|---|------------|----------------|--------|-------|-------|-------|-------|--------|-------|------|
| | _ | | - | 22° | 15' | 220 | 301 | 220 | 15' | 0 |
| | Dist. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | 181 |
| 4 | _ | | | | - | - | 0.38 | 0.92 | | 1 |
| | 1 2 | 0.93 | | | | | 0.77 | 1.84 | | 2 |
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| | 8 | | 3.00 | | | | | | 3.09 | 8 |
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| | 10 | | 3.75 | | 3.79 | 9 | 3.83 | 9,22 | 3.87 | 10 |
| | | | | | 4.17 | 10.16 | | 10.14 | 4.25 | |
| | | 10.20 | | 11.11 | | 11.09 | | 11.07 | | 12 |
| | | 11.13 | | 12.03 | | 12.01 | | 11.99 | 5.03 | 13 |
| | | 12.05 12.98 | | 12.96 | | 12.93 | | 12.91 | 5.41 | 14 |
| į | | | | 13.88 | | 13.86 | | 13.83 | | 15 |
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| 1 | | 17.62 | | 17.59 | | 17.55 | | 17.52 | 7:35 | 19 |
| | 20 | | | 18.51 | | 18.48 | | 18.44 | 7.73 | 20 |
| 1 | | | | 19.44 | | 19,40 | | 19.37 | 8.12 | 21 |
| | 21 | 19.47 | | 20,36 | | 20.33 | | 20.29 | 8.51 | 22 |
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| | 90 | 25.03 | 10.11 | 25.92 | 10.22 | 25.87 | 10.72 | 25 82 | 10.83 | 28 |
| | 20 | 25.96 | 10.49 | 26.84 | 10.00 | 26.79 | 11.10 | 26.74 | 11.21 | 29 |
| | 30 | 20.89 | 11 94 | 27.77 | 11.36 | 27.72 | 11.48 | 27.67 | 11.60 | 30 |
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| | 32 | 29.67 | 11.99 | 30.54 | 19.50 | 30 49 | 12 63 | 30 43 | 12.76 | 133 |
| | 33 | 30.60 | 12,36 | 31.47 | 19 97 | 31.41 | 13.01 | 31.35 | 13.15 | 34 |
| | 34 | 31.52 | 12.7 1 | 32.39 | 12 95 | 32.34 | 13.39 | 32.28 | 13.53 | 35 |
| 1 | 35 | 32.45 | 13.11 | 33.32 | 13.23 | 33 26 | 13.78 | 35 20 | 13.92 | 36 |
| | 36 | 33.38 | 13.49 | 34.24 | 14.01 | 34.18 | 14 16 | 34.12 | 14.31 | 37 |
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| 38 34.98 14.85 34.91 15.00 34.85 15.15 34.78 15.30 38 39 35.90 15.24 35.83 15.39 35.77 15.55 35.70 15.71 39 40 36.82 15.63 36.75 15.79 36.68 15.95 36.61 16.1 40 41 37.74 16.02 37.67 16.18 37.60 16.35 37.53 16.5 41 42 38.66 16.41 38.59 16.58 38.52 16.75 38.44 15.92 42 43 39.58 16.80 39.51 16.97 39.43 17.15 39.36 17.32 43 44 40.50 17.19 40.43 17.37 40.35 17.54 40.27 17.72 44 45 41.42 17.58 41.35 17.76 41.27 17.94 41.19 18.12 45 46 42.34 17.97 42.26 18.16 42.18 18.34 42.10 18.53 46 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 47 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 12.7 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. | | | | | | | | | | . , |
| 39 35.90 15.24 35.83 15.39 35.77 15.55 35.70 15.71 39 40 36.82 15.63 36.75 15.79 36.68 15.95 36.61 16.11 40 41 37.74 16.02 37.67 16.18 37.60 16.35 37.53 16.5 41 42 38.66 16.41 38.59 16.58 38.52 16.75 38.44 15.92 42 43 39.58 16.80 39.51 16.97 39.43 17.15 39.36 17.32 43 44 40.50 17.19 40.43 17.37 40.35 17.54 40.27 17.72 44 45 41.42 17.58 41.35 17.76 41.27 17.94 41.19 18.12 45 46 42.34 17.97 42.26 18.16 42.18 18.34 42.10 18.53 46 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 47 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12. | | | | | | | | | | |
| 40 36.82 15.63 36.75 15.79 36.68 15.95 36.61 16.11 40 41 37.74 16.02 37.67 16.18 37.60 16.35 37.53 16.5 11 42 38.66 16.41 38.59 16.58 38.52 16.75 38.44 15.92 42 43 39.58 16.80 39.51 16.97 39.43 17.15 39.36 17.32 43 44 40.50 17.19 40.43 17.37 40.55 17.54 40.27 17.72 44 45 41.42 17.58 41.35 17.76 41.27 17.94 41.19 18.12 45 46 42.34 17.97 42.26 18.16 42.18 18.34 42.10 18.53 46 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 47 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 19.00 10.00 1 | | | | | | | | | | |
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| 42 38.66 16.41 38.59 16.58 38.52 16.75 38.44 15.92 42 43 39.58 16.80 39.51 16.97 39.43 17.15 39.36 17.32 43 44 40.50 17.19 40.43 17.37 40.55 17.54 40.27 17.72 44 45 41.42 17.58 41.35 17.76 41.27 17.94 41.19 18.12 45 46 42.34 17.97 42.26 18.16 42.18 18.34 42.10 18.53 46 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 47 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 19.15 12.15 | | | - | | - | ļ | | | - | |
| 43 39.58 16.80 39.51 16.97 39.43 17.15 39.36 17.32 43 44 40.50 17.19 40.43 17.37 40.35 17.54 40.27 17.72 44 45 41.42 17.58 41.35 17.76 41.27 17.94 41.19 18.12 45 46 42.34 17.97 42.26 18.16 42.18 18.34 42.10 18.53 46 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 47 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 19.00 10.00 | | | | | | 3 | | | | |
| 44 40.50 17.19 40.43 17.37 40.35 17.54 40.27 17.72 44 45 41.42 17.58 41.35 17.76 41.27 17.94 41.19 18.12 45 46 42.34 17.97 42.26 18.16 42.18 18.34 42.10 18.53 46 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 47 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 50 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. | | | | | | | | | | |
| 45 41.42 17.58 41.35 17.76 41.27 17.94 41.19 18.12 45 46 42.34 17.97 42.26 18.16 42.18 18.34 42.10 18.53 46 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 47 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 19.15 10.15 | 3 | | | | | | | | | |
| 46 42.34 17.97 42.26 18.16 42.18 18.34 42.10 18.53 46 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 47 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 19.00 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. | 45 | | | | | | | | | |
| 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 47 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 19.15 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. | | | | | | | | | | |
| 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 48 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 49 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 19.10 Dep. Lat. Dep. Lat | | | | | | | | | | - 7 |
| 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 50 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. Dep. | | | | 44.10 | 18.95 | 44.02 | 19.14 | 43.93 | 19.33 | 48 |
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| | - | | | | | | | | 20.14 | 50 |
| 12 67° 0' 66° 45′ 66° 30′ 66° 15′ 2 | ist. | | 5 | THE RESERVE AND ADDRESS OF THE PERSON NAMED IN | Lat. | | | | Lat. | |
| | 10 | 67 | O, | 66° | 45' | 66° | 30' | 66° | 15' | |

65°

30'

65°

45'

650

66° · 0'

15'

| 100 | 5 ' | | RAV | ERSI | E TA | BLE. | 1 | 25 I | eg |
|-------|----------------|----------|----------------|--------|----------------|----------------|----------------|--------------------|-------|
| | 250 | • O' | 25° | 15' | 25° | 30' | 250 | | |
| 38 | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | isi |
| -1 | 0.91 | 0.42 | 0.90 | 1.0.45 | 0.9 | _ | | | - |
| 2 | 1.81 | 0.85 | 1.81 | 0.85 | 1.8 | | | 1 | 1 |
| 3 | 2.72 | 1.27 | 2.7,1 | 1.28 | 2.7 | 1 1.29 | 2.70 | , | |
| 4 | 3.63 | 1.69 | 3.62 | 1.7 | 3.6 | 1 1.75 | 3.60 | 1.74 | 4 |
| 5 | | | | 1 | | 1 2.1 | 4.50 | 2.17 | 5 |
| 6 | | | | 5 | | - | 5.40 | 2.61 | |
| 7 | 6.34 | 3 | 6 | | | | | | 7 |
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| 10 | | 1 | | | <u></u> | 3 4,3 | 9.01 | 4.34 | 10 |
| 1 1 3 | 9.97 | | E | | 4 | | | | • |
| 12 | | 1 | 10.85 | | 10.8 | | 10.83 | | |
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| 14 | | | 12.66 | | 12.6 | | 12.61 | | |
| 1/ | 13.59 | | 13 57 | , | 13.5 | | 13.51 | | |
| 17 | | | 14.47 | | 14.4 | | 4.41 | 1 | |
| 1,5 | 16.31 | | 15.38 16,28 | | 15.3 | | 15.31 | | |
| 19 | 17.22 | | 17.18 | | 16.2. 17.1. | | 16.21 | | |
| 4 1 | 18.13 | | 18.09 | | 18.03 | | 13.01 | | |
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| 1 | 19.03 19.94 | | 18.99 | | 18.95 | | 18.91 | 9.12 | |
| 3 4 | 20.851 | | 19.90 20.80 | | 19.86 20.67 | 1 | 19.82 | | |
| | | | | | | | 20.72 21.62 | | |
| 25 | 22.66 | 10.14 | 22 61 | 10.66 | 99.56 | 10.33 | 22.52 | | |
| | | | | | | | 23.42 | | |
| 3 2 | | | 24.42 | | | 1 | 24.32 | | |
| 3 | | | 25 32 | | | 1 | 45.22 | 1 | |
| | | | 26.23 | | | | 26.12 | | |
| 30/2 | 27.19 | 12.68 | 27.15 | 12.80 | 27.08 | | 27.02 | | |
| 3! | 28.10 | 13.10 | 28.04 | 3.22 | 27.98 | 13.35 | 27.92 | 13.47 | 31 |
| | | | 28.94 | | | | ₹8.82 | 13.90 | |
| 33 2 | 29.91 | 13.95 | 29.85 | 4.08 | 29.79 | , . | 29.72 | | |
| 343 | 30.81 | 14.37 | 30.75 | 4.50 | 30.69 | 1 , " | | | |
| | | | 31.66 | | | | 31.52 | 15.21 | |
| | | | | | | | 32.43 | | |
| 37 3 | 33.53 | | | | | 1 | 33,33 | | |
| | | | 34.37 | | | | 34.23 | 16.51 | |
| 100 | 55.35 | 16.48 | 35.27 | 6.64 | 35,20 | 16.79 | | 16.94 | _ |
| 100 | | - | 36.18 | | | | 36.03 | 17.38 | } î |
| 413 | 37.16 | 7.33 | 37.08 | 7.49 | 37.01 | 17.65 | | 17.81 | |
| 423 | 88.07 | 7.76 | 37.99 | 7.92 | 37.91 | | | 18.25 | |
| | | | 38.89 1 | | | | | 8.68 | - 1 |
| | | | 39.801 | | | | 0000 | 19.12 | |
| 46 4 | 1 60 | 9 02 4 | 10.701 | 9.20 | 40.62 | | -0.00 | 19.55 | |
| 47 4 | 2.60 | 0.96 | 1611 | 9.02 | 40.40 | 19.80 | | 19,984 | |
| 1 1 - | 3,5019 | 0.004 | 3 4119 | 0.05 | 42.42 | 20.23 | 42.53 | 20.42 4 20.85 4 | |
| 49 4 | 4.4.1.9 | 0.29 4 | 4.399 | 0.481 | 11 90 | 20.66 21.09 | 43.23 | 20.85 | |
| 50 4 | 5.32 9 | 1 15/4 | 5.299 | 1 33 | 15 19 | 21.09 | 44.13 | 21.72 | |
| ١٠٠١ | | .at. |)en | Lat | Dos: | | | Lot | |
| | 65° | 0' | 64° | 1.5! | Dep. 64° | Lat. | Dep. | 15' | \$21£ |
| | | <u> </u> | U T | ŦJ | 04 | 30' | 64° | 15 | 3 |

| 27° 0′ 27° 15′ 27° 30′ 27° 15′ 27° 30′ 27° 15′ 1 0.89 0.45 0.89 0.46 0.89 0.46 0.88 | 45' Dep. 0.47 0.93 | Dist. |
|---|--------------------|-------|
| 1 0.89 0.45 0.89 0.46 0.89 0.46 0.88 | 0.47 | 181 |
| | | |
| | 0.02 | 1 |
| 2 1.78 0.91 1.78 0.92 1.77 0.92 1.77 | 0.93 | 2 |
| 3 2.67 1.36 2.67 1.37 2.66 1.39 2.65 | 1.40 | |
| 4 3.56 1.82 3.56 1.83 3.55 1.85 3.54 | 1.86 | 4 |
| 5 4.46 2.27 4.45 2.29 4.44 2.31 4.42 | 2.33 | |
| 6 5.35 2.72 5.33 2.75 5.32 2.77 5.31 | 2.79 | 6 |
| 7 6.24 3 18 6.22 3.21 6.21 3.23 6.19 | 3.26 | 7 |
| 8 7.13 3.63 7.11 3.66 7.10 3.69 7.08 | | 8 |
| 9 8.02 4.09 8.00 4.12 7.98 4.16 7.96 | | 9 |
| 10 8.91 4.54 8.89 4.58 8.87 4.62 8.85 | 4.66 | 10 |
| 11 9.80 4.99 9.78 5.04 9.76 5.08 9.73 | 5.12 | 11 |
| 12 10.69 5.45 10.67 5.49 10.64 5.54 10.62 | 5.59 | 12 |
| 13 11.58 5.90 11.56 5.95 11.53 6.00 11.50 | 6.05 | i 3 |
| 14 12.47 6.36 12.45 6.41 12 42 6.46 12 39 | 6.52 | 14 |
| 15 13.37 6.81 13.34 6.87 13.31 6.93 13 27 | 6.98 | 15 |
| 16 14.26 7.26 14.22 7.33 14.19 7.39 14.16 | 7.45 | 16 |
| 17 15.15 7.72 15.11 7.78 15.08 7.85 15.04 | | |
| 18 16.04 8.17 16.00 8.24 15.97 8.31 15.93 | | 1 1 |
| 19 16.93 8.63 16.89 8.70 16.85 8.77 16.81 | | |
| 20 17.82 9 08 17.78 9.16 17.74 9.23 17.70 | 9.31 | 20 |
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| 22 19.60 9.99 19.56 10.07 19.51 10.16 19 47 | 10.24 | 22 |
| 23 20.49 10.44 20.45 10.53 20.40 10.62 20.35 | 10.71 | 23 |
| 24 21.38 10.90 21.34 10.99 21.29 11.08 21.24 | 11.17 | 24 |
| 25 22.28 11.35 22.23 11.45 22.18 11.54 22.12 | 11.64 | 25 |
| 26 23.17 11.80 23.11 11.90 23.06 12.01 23.01 | 12.11 | 26 |
| 27 24.06 12.26 24.00 12.36 23.95 12.47 23.89 | 12.57 | 27 |
| [28]24.95[12.71]24.89[12.82]24.84[12.93]24.78 | | , , |
| 29 25.84 13.17 25.78 13.28 25.72 13.39 25.66 | | : 1 |
| 30 26.73 13.62 26.67 13.74 26.61 13.85 26.57 | 13.95 | 30 |
| 31 27.62 14.07 27.56 14. (3) 27.50 14.31 27.43 | 14.43 | 31 |
| 32 28.5 1 14.5 3 28.4 5 14.65 28.38 14.78 28.32 | 14.90 | 32 |
| 33 29.40 14.98 29.34 15.11 29.27 15.24 29.20 | 15.37 | 33 |
| 34 30.29 15.44 30.33 15.57 30.16 15.70 30.09 | | |
| 35 31.19 15.89 31.12 16.03 31.05 16.16 30.97 | | |
| 36 32.08 16.34 32.00 16.48 31.93 16.62 31.86 | | |
| 37 32.97 16.80 32.89 16.94 32.82 17.08 32.74 | | 9 |
| 38 33.86 17.25 33.78 17.40 33.71 17.55 33.63 | | |
| 39 34.75 17.71 34.67 17.86 34.59 18.01 34.51 | | |
| 40 35.64 18.16 35.56 18.31 35.48 18.47 35.40 | | |
| 41 36.53 18.61 36.45 18.77 36.37 18.93 36.28 | | |
| 42 37.42 19.07 37.34 19.23 37.25 19.39 37.17 | | 1 1 |
| 43 38.31 19.52 38.23 19.69 38.14 19.86 38.05 | | |
| 44 39.20 19.98 39.12 20.15 39.03 20.32 38.94 | | • |
| 45 40.10 20.43 40.01 20.60 39.92 20.78 39.82 | | 1 1 |
| 46 40.99 20.88 40.89 21.06 40.80 21.24 40.71 | | |
| 47 41.88 21.34 41.78 21.52 41.69 21.70 41.59 | | |
| 48 42.77 21.79 42.67 21.98 42.58 22.16 42.48 | | 1 9 |
| 49 43.66 22.25 43.56 22.44 43.46 22.63 43.36 | | |
| 50 44.55 22.70 44 45 22.89 44.35 23.09 44.25 | | 50 |
| Dep. Lat. Dep. Lat. Dep. Lat. Dep. 62° 45′ 62° 30′ 62° | | Ist. |
| 5 63° 0′ 62° 45′ 62° 30′ 62° | 15' | |

| F | 5 | 28 | o 0' | 1 280 | 15' | 1 28 | 30' | 28 | 0 45' | ID |
|-----|--------|--------------|-------|-------|--------|-------|-------------|---------|-----------|------------|
| 100 | 7 - | Lat. | Dep. | Lat. | Dep | Lat | . I Dep | Lat. | Dep. | ist. |
| | ij | 0.88 | - | - | | - | - | -1 | - | - |
| | 2 | 1.77 | 0.94 | 1.76 | | | | | | 1 1 |
| | 3 | 2.65 | 1.4 | 2.64 | | | | - | 1 | |
| 1 | 4 | 3.53 | | | | | | A . | | 4 |
| | 5 | 4.41 | 2.3 | 4.40 | 2.37 | | | 4.38 | 2.40 | |
| | 6 | 5.30 | 2.89 | 5.29 | | | | 5. 5.26 | 2.89 | |
| | 7 | 6.18 | 3.29 | 6.17 | 3.3 | 6.1 | 3.34 | 6.14 | 3.37 | 7. |
| - | 8 | 7.06 | 3.76 | 7.05 | 3.79 | 7.03 | 3.82 | 7.01 | 3.85 | 1 1 |
| | 9 | 7.95 | 4.23 | 7.93 | 4.26 | 7.9 | 4.29 | 7.89 | | 29 |
| | 0 | 8.83 | 4.69 | 8.81 | 4.78 | 8.79 | 4.7.7 | 8.77 | 8 - 1 - 8 | 10 |
| 1 | 1 | 9.71 | 5.16 | 9.69 | 5.2 | 9.67 | | - | | |
| 1: | $2 _1$ | 0.60 | 5.63 | 10.57 | | 10.55 | 11 2 . 7 | 10.52 | 0.27 | 12 |
| 13 | 31 | 1.48 | 6.10 | 11.45 | | 11,49 | 114 7 0 7 2 | 11.40 | 1176, 117 | 13 |
| | | 2.36 | | 12.33 | | 12.30 | 1 1 1 1 2 2 | 27 | 11 | 14 |
| 1. | 5 1 | 3.24 | 7.04 | 13.21 | | 13.18 | 1. 6n 1 5 3 | 1. 15 | 14 | 15 |
| 11 | 6 1 | 4.13 | 7.51 | 14.0 | 7.57 | 14.06 | 5 3. | 33 | | 16 |
| 17 | 7 1 | 5.01 | | 14.98 | 8.05 | 14.94 | 9.11 | 14.90 | 8.13 | 17 |
| 118 | 1 ~ | 5 ·89 | 8.45 | 15.86 | 8.52 | 15.82 | \$.59 | 15.78 | 8.66 | i.8 |
| 119 | 1 ^ | 6.78 | 8.92 | 16.74 | 8.99 | 16.70 | 9.07 | 16.66 | 9.14 | 19 |
| 20 | 71 | 7.66 | 9 39 | 17.62 | 9.47 | 17.58 | 9.54 | 17.53 | 9.62 | 20 |
| 2 | | 8.54 | 9.86 | 18.50 | 9.94 | 18.46 | 10.02 | 18.41 | 10.10 | 21 |
| 22 | 211 | 9.42 | 10.33 | 19.38 | | | | 19.29 | | 22 |
| 23 | | 0.31 | | 20.26 | | | | 20.16 | | 23 |
| 24 | 12 | 1.19 | 11.27 | | | | | 21.04 | | |
| 25 | 2 | 2.07 | 11.74 | 22.02 | 11.83 | 21.97 | 11.93 | 21.92 | 12.02 | 25 |
| 126 | 2 | 2.96 | 12.21 | 22.90 | 12.31 | 22.85 | 12.41 | 22.79 | 12.51 | 26 |
| 27 | 2 | 3.84 | 12.68 | 23.78 | 12.78 | 23.73 | 12.88 | 23.67 | 12.99 | 27 |
| 128 | 2 | 4.72 | 13.15 | 24.66 | 13.25 | 24.61 | 13.36 | 24.55 | 13,47 | 28 |
| 29 | 2. | 5.61 | 13.61 | 25.55 | 13.73 | 25.49 | 13.84 | 25.43 | 13.95 | 29 |
| 30 | 2 | 6.49 | 14.08 | 26.43 | | | | 2,6.30 | | 30 |
| 31 | 2 | 7.37 | 14.55 | 27.31 | 14 67 | 27.2. | 14.79 | 27.18 | 14.9: | 31 |
| 32 | 2 | 8.25 | 15.02 | 28.19 | | 6 | | 28.06 | | 32 |
| 33 | 3 2 | 9.14 | 15.49 | 29.07 | 15.62 | 29.00 | 15.75 | 28.93 | 15.87 | 33 |
| 134 | 3 | 0.02 | 15.96 | 29.95 | 16.09 | 29 88 | 16.22 | 29.81 | 16,35 | 34 |
| 35 | 30 | 0.90 | 16.43 | 30.83 | 16 57 | 30.76 | 16.70 | 30.69 | 16.83 | 35 |
| 36 | 3 | 1.79 | 16.90 | 31.71 | 17.04 | 31.64 | 17.18 | 31.56 | 17.32 | 36 |
| 37 | 13 | 2.67 | 17.37 | 32.59 | i7.51 | 32.52 | 17.65 | 32.4 | 17.80 | 37 |
| 138 | 3 | 3.55 | 17.84 | | | | | | | 38 |
| 39 | 10. | 4.44 | 18.31 | 34.35 | 18.46 | 34.27 | 18.61 | 34.19 | 1876 | 39 |
| 40 | 3. | 5.32 | 18.78 | 35 24 | 18.93 | 35.15 | 19.09 | 35.07 | 10.24 | 40 |
| 41 | 3 | 5.20 | 19.25 | 36.12 | 14.41 | 35.03 | 19.5 | 35.90 | 13.72 | 41 |
| 42 | 37 | 7.08 | 19.72 | 37.00 | 1.9.88 | 36.91 | 20.04 | 36.82 | 20.20 | 42 |
| 43 | 37 | 7.97 | 20.19 | 37.88 | 20.35 | 37.79 | 20.52 | 37.70 | 20.63 | 43 |
| 44 | 38 | 3.85 | 20.66 | 38.76 | 20.83 | 38.67 | 21,00 | 38.58 | | 44 |
| 45 | 39 | 7.73 | 21.13 | 39.64 | 21.30 | 39.55 | 21.47 | 39.45 | | 45 |
| 46 | 40 | 0.62 | 21.60 | 40.52 | 21.77 | 40.43 | 21.95 | 40.33 | 22.13 | 46 |
| 47 | 4 | 1.50 | 22.07 | 41.40 | 22.25 | 4130 | 22.43 | 41.21 | 22.61 | 47 |
| 48 | 4 | 2.38 | 22.53 | 42 28 | 22.72 | 42.18 | 22.90 | 42.08 | 23.09 | 48 |
| 49 | 43 | 3 26 | 23.00 | 43.16 | 23.19 | 43.06 | 23.38 | 42.96 | 23.57 | 49 |
| 50 | | | | | | | | 43.84 | | 50 |
| st. | | Dep. | | | Lat. | | Lat. | | Lat. | St. |
| 515 | - | 32° | | 610 | | 61° | | - | 15' | isi Sis |
| - | 1_ | | | | | | - | | | 1 |

| اقا | 290 | 0' | 4 29° | 15' | 290 | 30' | 290 | 45' | D |
|-----------|------------|-------|--------------|-------|----------|----------------|----------|--------|------|
| ist. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | st. |
| 1 | 0.87 | 0.48 | U.87 | 0.49 | 0.87 | 0.49 | 0.87 | 0.50 | 1 |
| 2 | 1 7.5 | 0.97 | 1.75 | 0.98 | 1.74 | 0.98 | 1.74 | 0.99 | 1 |
| 3 | 2.62 | , | # . | | a | | 8 | | 1 1 |
| 4 | | 1 | | | 2 | | 4 | | 1 4 |
| 5 | | | | | a . | | 2 | | |
| 6 | lug to the | | | (| | | 73 | | 1 1 |
| 37 | | 3:39 | 6.11 6.98 | 1 | | | <u> </u> | | 1 4 |
| 29 | 7:00 | 4.36 | - | | | | 2 | | 1 1 |
| 10 | 1 4 . 6 | 4:85 | | | | | | L _ | i 1 |
| | - | | | | | | | 5.46 | - |
| \$ 100 10 | i are in m | F | 10.47 | | í0.44 | | 10.42 | | 1 |
| 1 2 7 | 11.37 | | 11.34 | | 11.31 | | 11 29 | | |
| ľ | 12 24 | | 78.22 | 2 | 12.19 | | 12.15 | 6.95 | 1. 1 |
| | 13.12 | C | 13999 | | 13.06 | | 13.02 | 7 44 | |
| | 15.99 | 7 | 13.96 | , | 13.93 | | 13.89 | | 16 |
| 17 | 14.87 | 8.24 | 14.33 | 8.31 | 14.80 | 8.37 | i4.76 | 8.44 | |
| 18 | 15.74 | 8.73 | 15.71 | 8.80 | 15.67 | | 15.63 | | 18 |
| | 16.62 | | 16.38 | | 16.54 | | 16.50 | | |
| 120 | 17.49 | 9.70 | 17.15 | 9.77 | 17.41 | 9.85 | 17.36 | 9.92 | 20 |
| | 18.37 | | 18.32 | [| 1.8 | 10.34 | 2 | | 21 |
| | 4 . | | 19.20 | | | 10.83 | 4 | 10.92 | 22 |
| | • 2/ | | 20.07 | 1 | 2. | 11.33 | | 11.41 | 23 |
| 24 | 20.99 | 11.64 | 20.94 | 11.73 | 20,89 | i 1.82 | 20.84 | 11.91 | 24 |
| 25 | 21.87 | 12:12 | 21.81 | 12.22 | 21,76 | i 2-31 | 21 70 | 12.41 | 26 |
| 26 | 22.74 | 12.61 | 22.69 | 12.70 | 22.03 | 12 80 | 22.57 | 12-90 | 27 |
| 27 | 23.61 | 13.09 | 23.30 | 13,19 | 23,30 | 13 30 13 79 | 23.44 | 13.40 | 28 |
| 20 | 24,49 | 14.06 | 25.30 | 14 17 | 25 24 | 14.48 | 25.18 | 14-39 | 29 |
| | | | | | | 14.77 | | | 30 |
| | | 1 | | | - | 15.27 | | | |
| 23 | 27 00 | 15,03 | 27.92 | 15.64 | 27.85 | 15.76 | 27.78 | 15.88 | 32 |
| 33 | 28.86 | 16.00 | 28.79 | 16.12 | 28.72 | 16.25 | 28.65 | 16.38 | 33 |
| 34 | 29.74 | 6 48 | 29.67 | 16.61 | 29.59 | 16.74 | 29.52 | 16.87 | 34 |
| | | | | | | 17.23 | | | |
| 36 | 31.49 | 17.45 | 31.41 | 17.59 | 3i.33 | 17.73 | 31.25 | 17.86 | 36 |
| 37 | 32.36 | 17.94 | 32.28 | 18.08 | 32-20 | 18.22 | 32-12 | 18.36 | 37 |
| 38 | 33.24 | 18.42 | 33.16 | 18.57 | 33.07 | 18.71 | 32.99 | 8.86 | 38 |
| | | | | | | 19.20 | | | |
| f | | | 2 . | , 5 | | 19.70 | | | |
| 41 | 35.86 | 19.88 | 35.77 | 20.03 | 35.68 | 20.19 | 35.60 | 20.35 | 41 |
| 42 | 36.73 | 20.36 | 36.65 | 20.52 | 36.56 | 20.68 | 36.46 | 20.84 | 43 |
| | | | | | | 21 17 | | | |
| | | | | | | 21.67 | | | |
| | | | | | | 22.16 22.65 | | | 3 |
| 40 | 40.23 | 22.30 | 41.01 | 29 07 | 40.04 | 23.14 | 40-81 | 23.32 | |
| 4.8 | 41.11 | 23 27 | 41.88 | 23.45 | 41.78 | 23.64 | 41.67 | 23.82 | 48 |
| | | | | | | 24.13 | | | 49 |
| 50 | 43 73 | 24.24 | 43.63 | 24.43 | 43.52 | 24.62 | 43.41 | 24 8 i | 50 |
| | | | | | | Lat. | | Lat. | st |
| is | | | 600 | | | | 60~ | 15' | 5 |

| 30 | Deg. | | | | | | | | |
|-----|--------|-------------------|----------------|-------|----------|-------|----------------|------------------|-------|
| { 5 | • • • | 0' |] 30° | 15' | 30° | 30' | 30° | 45' | 101 |
| 31. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | ist |
| | 0.87 | 0.50 | 0.86 | 0.50 | 0.86 | 0.51 | 0.86 | 0.51 | 1 |
| | 2 1.73 | 1 | 2 | | 1.72 | | 1.72 | 1.02 | 2 |
| | 2.60 | | | | | 1 | 2.58 | 1.53 | 3 |
| - 1 | 3.46 | | | 4 | | | | 2.05 | 4 |
| 1 | | | 4 | 4 | | 2.54 | | 2.56 | 5 |
| 17 | | | | 1 | 5 | 3.05 | | 3.07 | 6 |
| 8 | 1 | 1 | | ă | | 3.55 | | 3.58 4.09 | |
| 9 | | | 4 | i | | | | 4.60 | 9 |
| 10 | 1 | T . | | 100 | | | 5 11 | 5.11 | |
| 11 | 9.53 | | | 5.54 | 9.48 | 5.58 | | 5.62 | |
| 12 | | | 10.37 | 1 | 10.34 | 1 | | 6.14 | - 4 |
| 13 | 11.26 | 6.50 | 11.23 | 6.55 | 11.20 | | 11.17 | 6.65 | |
| 14 | 12.12 | 7.00 | 12.09 | 7.05 | 12.06 | 7-11 | 12.03 | , | |
| 4 . | 12.99 | • | 12.96 | d I | 12.92 | 7.61 | 12.89 | 7.67 | 15 |
| 116 | . | | 13.82 | 4 | 13.79 | | 13.75 | 8.18 | |
| 17 | | 1 | 14.69 | | 14.65 | | 4.61 | 8.69 | 1 . L |
| 18 | | | 15.55 | | 15.51 | | 15.47 | 9.20 | |
| 20 | 1.0.10 | | 16.41 17.28 | | 16.37 | | 16.33 | 9.71 | 1 |
| [| | | 1 | - | | | 17.19 | $\frac{10.23}{}$ | |
| 21 | 1 a | | 18 14 | | | 10.66 | | 10.74 | |
| 22 | 1.000 | | 19.00 19.87 | | | | | 11.25 | |
| 23 | 20 70 | 12.00 | | | 19.82 | | 19.77 20.63 | 11.76 | |
| 24 | 10. | | 21.60 | | | | 21.49 | | |
| 26 | 00 40 | 1 | 22 46 | | | | 22.34 | | |
| 27 | 100 00 | 1 | 23.32 | | | | 23.20 | 13.80 | |
| 28 | 24.25 | 14.00 | 24.19 | 14.11 | 24.13 | | 24.06 | | ŧ |
| | 25.11 | | 25.05 | | | 14.72 | 24.92 | 14.83 | 29 |
| 30 | 25.98 | 15.00 | 25.92 | 15.11 | 25.85 | 15.23 | 25.78 | 15.34 | 30 |
| 31 | 1 | 15.50 | | | X | 15.73 | 26.64 | 15.85 | 31 |
| 3 | 27.71 | | 27.64 | | | | 27.50 | 16.36 | 32 |
| 1 | 28.58 | | 28.51 | | | | 28.36 | 16.37 | i i |
| I. | | 17.00 | | 4 | | | | 17.38 | |
| 1 | 30.31 | 18.00 | 30.23 | | | | | 17.90 | i |
| | 1 | 18.50 | | | | | 30.94 | 18.41 | |
| | 1 | 19.00 | | | | | 32.66 | | |
| 1 | | 19.50 | - | 2 | | 9 | 33.52 | | |
| | | 20.00 | | | | 20.30 | | 20.45 | |
| / | | $\frac{1}{20.50}$ | | | | | 35,24 | | |
| | | 21 00 | | | | | 36.10 | 21.47 | i |
| 43 | 37.24 | 21.50 | 37.15 | 21.66 | 37.05 | | 1 | 21.99 | |
| 44 | 38.11 | 22.00 | 38.01 | 22.17 | 37.91 | 22.35 | 37.81 | 22,50 | 44 |
| 45 | 38.97 | 22.50 | 38.87 | 22.67 | 38.77 | 22.84 | 38.67 | 23.01 | 45 |
| 46 | | 23.00 | | 5 | | | 39.53 | | 1 |
| 47 | | 23.50 | | | | | 40.39 | | 1 |
| 49 | | 24.00 | | | | | 41.25 | | 1 |
| | | 24.50 25.00 | | | | | G. | 25.05 | |
| | | Lat. | | | 43.08 | | 42.97 | | 30 |
| Dis | 60° | 0' | Dep. 59° | Lat. | Dep. 59° | | Dep. | Lat. | ist |
| | 000 | 0, | 59 | 45' | 59 | 30′ | 59 | 15' | 0 |

| 1.14 | Į. | TRA | AVEF | SE 7 | - | | 1 | 31 De | g. |
|-------|--|-------|--------------|-------|-------------------|--------------|--------------|--------------|-------|
| Di | 310 | 0' | 31° | 15' | 3,0 | 30' | 310 | 45' | D |
| st 1s | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | 二 |
| 1 | 0.86 | 0.52 | 0.85 | 0.52 | | 0.52 | 0.85 | 0.53 | 1 |
| 2 | 1.71 | 1,03 | 1.71 | 1.04 | 1.71 | 1.04 | 1.70 | 1.05 | 20 00 |
| 3 | 2.57 | 1.55 | 2.56 | 1.56 | 2.56 | 1 57 | 2.55 | 1.58 | 4 |
| 4 | 3.43 | 2.06 | | _ | 3.41 | 2.09 | 3.40 | 2.10 | 5 |
| 5 | 4.29 | 2.58 | 4 27 | 2.59 | 4.26 5.12 | 2.61 3.13 | 4.25 5.10 | 2.63 3.16 | 6 |
| 6 7 | 5.14 | 3.09 | 5.13 | | | | 5.95 | 3.68 | 7 |
| 8 | 6.00 | 3.61 | 5.98 6.84 | 4.15 | 6.82 | | 6.80 | 4.21 | 8 |
| 9 | 6.86 | 4.12 | | | *** | | | 4.74 | 9 |
| 10 | 8.57 | 1 | | | | | 8.50 | 5.26 | 10 |
| 111 | | 5.67 | | | 9.38 | | 9,35 | | 11 |
| 12 | 9.43 | | 10.26 | | 10.23 | | 10.20 | | 12 |
| 13 | 11.14 | 6.70 | | | 11.08 | | 11.05 | | 13 |
| 14 | 12.00 | | 11.97 | | 11.94 | | 11,90 | | 14 |
| 15 | | / | 12.82 | | 12.79 | 7.84 | 12.76 | | 15 |
| 16 | | | 13.68 | , | 13,64 | | 13.61 | | 16 |
| 17 | 14.57 | 8.76 | 14.53 | | 14.49 | | 14.46 | | 17 |
| 18 | 15.43 | | 15.39 | | 15.35 | 9.40 | 15,31 | 9.47 | 18 |
| 19 | 16.29 | 9.79 | 16.24 | 9.86 | 16.20 | 9.93 | 10.10 | 10.00 | 19 |
| 20 | 17.14 | | 17.10 | | | - | | | 20 |
| 21 | 18.00 | 10.82 | 17.95 | 10.89 | 17.91 | | | 11.05 | |
| 22 | 18.86 | 11,33 | 18.81 | 11.41 | 18.76 | 11.50 | 10.11 | 11,58 | 22 |
| 23 | 19,71 | 11.85 | 19.66 | 11.93 | 19.61 | 12.02 | 20 11 | 19.63 | |
| 24 | 20.57 | 12.36 | 20,52 | 12.45 | 20.40 | 12.54 | 21.26 | 12.03 | 25 |
| 25 | 21.43 22.29 | 12.88 | 21.37 | 12.96 | 99 17 | 13.00 | 22.11 | 13.68 | 26 |
| 26 | $\begin{bmatrix} 22.29 \\ 23.14 \end{bmatrix}$ | 13.39 | 22.23 | 13.49 | 23.09 | 14.1 | 22.96 | 14.21 | 27 |
| 27 | $\begin{vmatrix} 23.14 \\ 24.00 \end{vmatrix}$ | 13.91 | 93 04 | 14.01 | 23.87 | 14.63 | 23.81 | 14.73 | 28 |
| 128 | 24.00 24.86 | 14,4~ | 24.79 | 15.04 | 24.73 | 15.16 | 24.66 | 15.26 | 29 |
| 30 | 25.72 | 15.45 | 25,65 | 15.56 | 25.58 | 15.68 | 25 51 | 15.79 | 30 |
| 30 | $\frac{25.72}{26.57}$ | 15.45 | 26.50 | 16.08 | $\frac{1}{26.43}$ | 16.20 | 26.36 | 16.31 | 31 |
| 29 | 97 12 | 16 19 | 27.36 | 16.60 | 27.28 | 16.72 | 27.21 | 16.84 | 32 |
| 29 | 124 20 | 17 00 | 128.21 | 17.12 | 28.14 | 117.24 | 28.06 | 17.30 | 33 |
| 21 | 190 14 | 17 51 | 29.07 | 17.6 | 28,99 | 117.77 | 28°91 | 17.89 | 34 |
| 25 | 30 00 | 18 03 | 29.92 | 18.16 | 29.84 | 118,29 | 29.76 | 18.42 | 33 |
| 20 | 20 06 | 10 51 | 30.78 | 13.68 | 30.70 | 118.81 | 30.61 | 18.94 | 30 |
| 37 | 31 79 | 19.06 | 31.63 | 19.19 | 31.55 | 119.33 | 31.46 | 119.47 | 31 |
| 13.0 | 29 57 | 10 57 | 32.49 | 19.7 | 32.40 | 119.86 | 32.31 | 20.00 | 30 |
| 39 | 33.43 | 20.09 | 33 34 | 20.23 | 33.25 | 20.38 | 34.01 | 20.32 | 40 |
| 40 | 34.29 | 20,60 | 34.20 | 20.75 | 34.1 | 20.90 | 34,01 | £1.05 | 41 |
| 41 | 35.14 | 21 12 | 35.05 | 21.27 | 34.96 | 21.42 | 34.80 | 21.57 | |
| 42 | 36.00 | 21 63 | 35.91 | 21.79 | 26.66 | 21.95 | 36 57 | 22.10 | 4.3 |
| 43 | 36.86 | 22.15 | 30.70 | 22.31 | 37.59 | 22.47 | 37 49 | 23 1-5 | 44 |
| 44 | 37.72 38.57 | 22.66 | 37.62 | 22.03 | 38 37 | 44.99 | 38.27 | 23.68 | 45 |
| 45 | 38.57 39.43 | 23.18 | 30.26 | 23.34 | 39 22 | 24 04 | 39.12 | 24.21 | 46 |
| 40 | 39.43 40.29 | 23.09 | 40 19 | 24.38 | 40.07 | 24.56 | 39.97 | 24.73 | 47 |
| 47 | 40.29 | 94.21 | 41.04 | 24.90 | 40 93 | 25.08 | 40.82 | 25.26 | 48 |
| 10 | 42.00 | 25 94 | 41.89 | 25.42 | 41.78 | 25.60 | 41.67 | 25.78 | 43 |
| 50 | 42.86 | 25.75 | 42.75 | 25.94 | 42.63 | 26.12 | 42.55 | 26.31 | 50 |
| (| | | Dep. | | | | | Lat. | st. |
| Jist | 59° | | 58° | 45' | 58° | 30' | 58° | 15' | D |
| I | 1 39 | | 30 | 10 | | | | | |

| 52 | Deg. | | T ,R | AVE | RSE ' | L ABI | E | | 115 |
|------|--------------|-------|-------------|---------------------|----------------|---------------------|-------------------------|--------------|-------|
| D | 4 | 0' | 320 | 15' | 320 | | 320 | 45' | D |
| ıst. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | 181 |
| 1 | 0.85 | | 0.85 | 0.53 | | 0.54 | | 0.54 | 1 |
| 2 | | | | 1.07 | | 1.07 | 1.68 | 1.08 | |
| 3 | 2.54 | | | 1.60 | | 1.61 | 2.52 | 1.62 | 7 |
| 4 | | | | 2.13 | | 2.15 | | | -1 |
| 5 | 4.24 5.09 | | | $\frac{2.67}{3.20}$ | | $\frac{2.69}{3.22}$ | | 2.70 3.25 | |
| 7 | 5.94 | | , | 3.20 | | 3.76 | | | |
| 8 | | | | | | 4.30 | | | |
| 9 | | 3.5 | | 4.80 | | 4.84 | | _ | |
| 10 | | | | 5.34 | | 5.37 | | 5.41 | 10 |
| III | 9.33 | 5.83 | 9,30 | 5.87 | 9.28 | 5.91 | 9.25 | 5.95 | |
| | 10.18 | | 10.15 | | 10.12 | - | 10.09 | | |
| 13 | 11.02 | 6.89 | 10.99 | 6 94 | 10 96 | 6.98 | 10.93 | | |
| 14 | 11.87 | 7.42 | 11.84 | 7 47 | 11 81 | 7.52 | 11.77 | | 1 9 |
| | 12.72 | | 12.69 | 8.00 | 12.65 | 8.06 | 12.62 | 8.11 | 15 |
| | 13 57 | | 13.53 | | 13.49 | | 13.46 | | |
| | 14.42 | | 14.38 | | 1,4 34 | | 14.30 | | |
| • | 15.26 | | 15.22 | , | 15.18 | | 15.14 | | |
| 4 | 16 11 | F | 16.07 | | 16 02 | | | | |
| | - | | 16.91 | | 16.87 | | | | |
| | 17.81 | | 17.76 | | | | 17.66 | 1 | |
| | (| | 18.61 | | 18.55 | | | | |
| | | | | | 19 40 20.44 | | | | |
| | | | _ | 3 | 21.08 | | | | - |
| | | | _ | | 21.93 | | 1 | | |
| | | 2 | | | 22 77 | 1 | a a | | 3.4 |
| 7 | , | | | | 23.61 | | • | | |
| | | | | | 24 46 | | | • | |
| 30 | 25.44 | 15 90 | 25.37 | 16.01 | 25.30 | 16 12 | 25.23 | 16.23 | 30 |
| 31 | 26.29 | 16.43 | 26.22 | 16.54 | 26.15 | 16.66 | 26.07 | 16.77 | 31 |
| 32 | 27.14 | 16.96 | 27.06 | 17.08 | 26.99 | 17.19 | 26,91 | 17.31 | 32 |
| 33 | 27.99 | 17.49 | 27.91 | 17.61 | 27.83 | 17.73 | 27 7 5 | 17.85 | 33 |
| | | | | | 28.68 | 2 | | 1 | 1 -1 |
| | | 9 . | | | 29.52 | | | ŧ | 1 - 6 |
| 8 : | | | | | 30.36 | | | 1 | 1 1 |
| | | | | | 31.21 | | | 1 | 1 . 3 |
| | | 1 1 | | | 32.05 32.89 |) | | 1 | 1 |
| | | | | | 33.74 | | | 1 | |
| - | | · | | - | | | S annual profession and | | 1 |
| | | | 4 | | 34.58 35.42 | | * | 5 | 1 2 |
| | | (| * 19 | | 36.27 | 1 | 6 | | 1 1 |
| | | 4 | | 1 | 37.11 | | | 1 | |
| | _ | | | 1 | 37.95 | 2 | | | 1 1 |
| | | | | | 38.80 | | | 1 | 1 1 |
| | | | | | 39.64 | | | 1 | |
| | | 1 | • | • | 40.48 | | | 1 | 1 . |
| | | | | | 41.33 | | 2 | • | |
| 50 | 42 40 | | | | 42.17 | 26.86 | 42.05 | 27.0 | 50 |
| st. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | | st. |
| | 58° | 0' | 57° | 45' | 57° | 30' | 57° | 15' | Ö |

| 11 | δ | TR | AVER | RSE | TABI | LE. | | 33 D | eg, |
|------|--------|-------|----------------|-------|-----------------------|-------|-------|-------|--------|
| E | 339 | 0' | 1 33° | 15' | 33° | 30' | 330 | 45' | U, |
| 181. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | Dep. | st. |
| 1 | 0.84 | | 0.84 | | 1 | - | 0.83 | 0.56 | 1 |
| 1 | 2 1.68 | | | | | ŧ | | 1 11 | 2 |
| | 3 2.52 | 1 | | i | | | 2.49 | 1.67 | 3 |
| 3 | 4 3.35 | | | | | | 3.33 | 2.22 | 4 |
| ₹ | 4.19 | | | | 4 | | | 1 | 5 |
| | 5.03 | | 1 | | 5.00 | 3.31 | 4.99 | 3.33 | |
| | 5.87 | | | 3.84 | 5 84 | 3.86 | 5.82 | 3.89 | 7 |
| il. | 6.71 | | 1 ' | | 6.67 | 4.42 | 6.65 | 4.44 | 8 |
| - 1 | 7.55 | 1 | | t e | 7.51 | 4.97 | 7.48 | 5.00 | 9 |
| 10 | | | | 5.48 | 8.34 | 5.52 | 8.31 | 5.56 | 10 |
| i | | | | 5.03 | 9.17 | 6.07 | 9.15 | 6.11 | 11 |
| | 10.06 | | 10.04 | | 10.01 | 6.62 | R | 6.67 | 1 1 |
| | 10.00 | | 10.87 | | 10.84 | | 10.81 | 7.22 | 1 |
| . 1 | 11.74 | 1 | 11.71 | | 11.67 | | 11.64 | 7.78 | 14 |
| | 12.58 | | 12.54 | | 12.51 | | 12.47 | | |
| 1 | 13.42 | 1 | 13.38 | | 13.34 | | 13.30 | | 16 |
| | 13.42 | | 14.22 | | 14.18 | | 14.13 | | 17 |
| | 15.10 | | 15.05 | | 15.01 | | 14.97 | | 18 |
| 1 | 15.93 | | 15.89 | | 15.84 | 1 | 15.80 | | 19 |
| 1 | 16.77 | | 16.73 | | 2 | | 16.63 | | 20 |
| - | | | | | $\frac{17.51}{17.51}$ | | 17.46 | | ${21}$ |
| 1 | 17.61 | | 17.56 18.40 | | | | 1 | | 22 |
| , | 18.45 | 1 2 | 19.23 | 19.00 | 10.33 | 19.60 | 10.23 | 12.78 | 23 |
| 23 | 19.29 | 12.53 | 20.23 | 12.01 | 20.01 | 12.05 | 19.12 | 13 33 | |
| 24 | 20.13 | 13.62 | 20.07 | 10.10 | 20.01 | 13.23 | 20.79 | 13.89 | 25 |
| 25 | 20.97 | 13.62 | 20.91 | 14.96 | 21.69 | 14.35 | 21.69 | 14 44 | 26 |
| | | 14.71 | | | | | | | |
| 27 | 22.64 | 15 25 | 22.30 | 14.00 | 99 35 | 15 45 | 23.28 | 15.56 | 28 |
| | | 15.79 | | | | | | 16.11 | 29 |
| 29 | 24.32 | 15.79 | 24.43 | 16.50 | 25.09 | 16.56 | 24.94 | | 30 |
| 30 | | • | | | | | | | |
| 31 | 26.00 | 16.88 | 25.92 | 17.00 | 25.85 | 17.11 | 25.78 | 17.78 | 32 |
| 32 | 26.84 | 17.43 | 26.76 | 17.55 | 26.68 | 17.00 | 20.01 | 18.33 | 33 |
| 33 | 27.68 | 17.97 | 27.60 | 18.09 | 27.52 | 18.21 | 00 07 | | |
| 34 | 28.51 | 18.52 | 28.43 | 18.64 | 28.35 | 18.77 | 20.27 | 19.44 | |
| 35 | 29.35 | 19.06 | 29.27 | 19.19 | 29.19 | 19.33 | 29.10 | 20.00 | 36 |
| 36 | 30.19 | 19.61 | 30.11 | 19.74 | 30.02 | 19.87 | 30.76 | | |
| 37 | 31.03 | 20.15 | 30.94 | 20.29 | 30.85 | 20.42 | 31.60 | 21 11 | 38 |
| 38 | 31.87 | 20.70 | 31.78 | 20.84 | 31.09 | 20.97 | 32 43 | 21.67 | 39 |
| 39 | 32.71 | 21.24 | 32.02 | 21.08 | 22.52 | 22.53 | 33.26 | 22 22 | 40 |
| 40 | | 21.79 | | | | | | | |
| 41 | 34.39 | 22.33 | 34.29 | 22.48 | 34.19 | 22.63 | 34.09 | 22.78 | 41 |
| 42 | 35.22 | 22.87 | 35.12 | 23.03 | 35.02 | 23.18 | 34.92 | 23.33 | 42 |
| 43 | 36.06 | 23.42 | 35.96 | 23.58 | 35.86 | 23.73 | 35.75 | 23.89 | 43 |
| 44 | 36.90 | 23.96 | 36.80 | 24.12 | 36.69 | 24.29 | 36.58 | 24.45 | 44 |
| 45 | 37.74 | 24.51 | 37.63 | 24.67 | 37.53 | 24.84 | 37.42 | 25.00 | 45 |
| 46 | 38.58 | 25.05 | 38.47 | 25.22 | 38.36 | 25.39 | 38.25 | 25.56 | |
| 47 | 39.42 | 25.60 | 39.31 | 25.77 | 39.19 | 25.94 | 39.08 | 26.11 | 47 |
| 48 | 40.26 | 26.14 | 40.14 | 26.32 | 40.03 | 26.49 | 39.91 | 26.67 | |
| 4.9 | 41.09 | 26.69 | 40.98 | 26.87 | 40.86 | 27.05 | 40.74 | 27.22 | |
| 50 | 41.93 | 27.23 | 41.81 | 27.41 | 41.69 | 27.60 | 41.57 | 27.78 | 50 |
| St | Dep. | Lat. | Dep. | Lat. | Dep. | Lat. | D ep. | Lat. | ist. |
| IĀ | 570 | 0' | 56° | 45'. | 56° | 30' | 56° | 15' | Dis |
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| 9 | 6.89 | 5.79 | 6.87 | 5.82 | | | 6.82 | | 9 |
| 10 | 7.66 | 6.43 | 7.63 | 6.46 | 7.60 | 6.49 | 7 58 | 6.53 | 10 |
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| 23 | 22.22 | 18.64 | 22.13 | 18.74 | 22.05 | 18.83 | 21.97 | 18.93 | 29 |
| 30 | 22.98 | 19.28 | 22.90 | 19.38 | 22.81 | 19.48 | 22.73 | 19.58 | 30 |
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| st. | Dep. | Lat. | Dep. | Lat. | | Lat. | | | st. |
| Dis | 50° | U' | 490 | 45' | 490 | 30' | 49° | 15' | 151 |
| 1 | The San Person Name of Street, or other Designation of the Owner, where the Person of the Owner, where the Owner, which the Owner, where the Owner, which the O | District of the last | - | | - | - | | m. main in | 113 |

| | 24 | | RAVE | ERSE | TAB | LE. | | 41 D | egz |
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| 16 | 11.32 | 9.84 | 11.28 | 9.89 | 11.23 | 10.60 | 11.19 | 9.99 | 15 |
| 17 | 12.83 | 10.50 11.15 | 12.78 | 11.21 | 12.73 | 11.26 | 12.68 | 11.32 | 17 |
| 101 | 13.58 | 11.81 | 13.53 | 11.87 | 13.48 | 11.93 | 13.43 | 11.99 | 18 |
| 119 | 14.34 | 12.47 | 14.28 | 12.53 | 14.23 | 12.59 | 14.18 | 12.65 | 19 |
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| 23 | 17 36 | 14.43 | 16.54 | 14.51 | 17.93 | 14.58 | 16.41 | 14.65 | 22 |
| 24 | 18.11 | 15 75 | 18 04 | 15.82 | 17.98 | 15.90 | 17 91 | 15.98 | 24 |
| 23 | 18.87 | 16.40 | 18 80 | 16.48 | 18.72 | 16.57 | 18.65 | 16.65 | 25 |
| 105 | 19.62 | 17.06 | 19.55 | 17.14 | 19.47 | 17.23 | 19.40 | 17.31 | 26 |
| 1~ 12 | 40.381 | 17.718 | 20 SOL | 17 801 | 20.221 | 17.891 | 20.141 | 17.98 | 271 - |
| 29 | 21.13 | 18.37 | 21.05 | 18.45 | 20.97 | 18.55 | 20.89 | 18.64 | 28 |
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| 10212 | 24.15 | 20.99 | 24.06 | 21.100 | 23.97 | 21.20 | 23.87 | 21.31 | 39 |
| 33/2 | 24.91 | 21.65 | 24.81 | 21.76 | 24.72 | 21.87 | 24.62 | 21.97 | 32 |
| 24/2 | 25.66 | 22.311 | 25.56 | 22.42 | 25.461 | 22.53 | 25.37 | 22.64 | 31 |
| 362 | 7.17 | 23.69 | 20.31 | 23.08 23.74 | 26.21 | 23.19 | 26.11 | 23.31 | 35 |
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| 13012 | 8.68 | 24.93 | 28.578 | 25.06 | 28.46 | 25.18 | 28.35 | 25.30 | 38 |
| 13912 | 9.435 | 25.59 | 29.321 | 25.711 | 29.211 | 25.84 | 29.10 | 25.97 | 30 |
| 41 3 | 0.19 | 36.24 | 30.07 | 26.37 | 29.96 | 26.50 | 29.84 | 26.64 | 40 |
| 42 2 | 1 70 | 26.90 | 30.83 | 27.03 | 30.71 | 27.17 | 30.59 | 27.30 | 41 |
| 433 | 2.45 | 28.21 | 32 339 | 28.35 | 31.40 | 27.83 | $\frac{31.33}{20.08}$ | 27.97 | 42 |
| 17.73 | 3.2112 | 8.87 | 33.08 | 29.0 II; | 32.951 | 29.16 | 39.83 | 29 300 | 1.1. |
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| 50 3 | 7.74 | 32.80 | 37.59 | 32.97 | 37.45 | 33 13 | 37 30 | 32.03 | 49 |
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| | 15 | 4: | 3° 0' | | 3° 15′ | 43 | • 30′ | 43 | 45' | מ |
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| 9 | 22 | 16.09 | | 0 16.02 | 12 | _ | | 15.89 | 15.21 | 22 |
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| 1 | - 1 | | | 33.51 | | | | | | |
| 4 | 7 3 | 4.37 | 32.05 | 34.23 | 32.20 | 34.09 | 32,35 | 33.95 | 32.50 | 17 |
| | - 1 | 5.10 | | 34.96 | | 34.82 | | | 33.19 | |
| | | | | 35.69 | | 35.54 | | | 33.88 | |
| 3 | | | | 36.42 | | 36.27 | | - | 34.58 | - |
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| - | | 47. | 0' | 46° | 45' | 46° | 30' | 46° | 15' | 1 |

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| | 449 | 00 | 440 | 15' | 440 | 30 | 44 | 45' | 45° | |
| ist. | Lat | VDen. | Lat. | Den. | Lat. | IDen. | Lat | Den | Den | ist. |
| 1 | | - | | | | | - | | | - |
| 1 | 0.72 | 0.69 | 0.72 | 0.70 | 0.71 | 0.70 | | | 0.71 | 1 |
| 2 | 1.44 | 1.39 | 1.43 | 1.40 | 1.43 | 1.40 | 1.42 | 1.41 | 1:41 | 2 |
| 3 | 1 | 2.08 | 2.15 | 2.09 | 2.14 | 2.10 | 2.13 | 2.11 | 2.12 | 3 |
| 1 | | 1 | | | | | | | | |
| 4 | | 1 | | | | | | | | |
| 5 | | 1 | | | | | | 1 1 | | |
| 1 6 | 4.32 | 4.17 | 4.30 | 4.19 | 4.28 | | | | | 6 |
| 17 | 5.04 | 4.86 | 5.01 | 4.88 | 4,99 | 4.91 | 4.97 | 4.93 | 4.95 | 7 |
| 1 8 | | 5.56 | 5.73 | 5.58 | 5.71 | 5.61 | 5.68 | 5.63 | 5.66 | 8 |
| 9 | | | | | | | | 1 | | |
| | | | | | | | | 1 | | 1 |
| 10 | 7.19 | 6.95 | | | | | _ | 1 | | |
| 111 | 7.91 | 7.64 | 7.88 | 7.68 | 7.85 | 7.71 | 7.81 | 7.74 | 7.78 | 11 |
| 112 | t | 8.34 | 8.60 | 8.37 | 8.56 | 8.41 | 8.52 | 8.45 | 8.49 | 12 |
| 13 | 1 | | | | | 1 | | 1 . | 9.19 | 13 |
| 1 | 1 | | | | | | | | | |
| 114 | | | 10.03 | | | | | | | |
| | | | 10.74 | | | | | | | 15 |
| 16 | 11.51 | 11.11 | | | 11.41 | | 11.36 | | | 16 |
| 17 | 12.23 | 11.81 | 12.18 | 11.86 | 12.13 | 11.92 | 12.07 | 11.97 | 12.02 | 17 |
| | | | 12.89 | | | | | | | |
| | | | 13.61 | | | | | | | |
| 119 | 13.07 | 13.20 | 13.01 | 19.40 | 14.00 | 13.32 | 14.00 | 14.00 | 14 14 | 90 |
| 20 | 14.39 | 13.89 | 14.33 | 13.96 | 4.26 | 14.02 | 14.20 | 14.08 | 14.14 | 20 |
| 21 | 15.11 | 14.59 | 15.04 | 14.65 | 14.98 | 14.72 | 14.91 | 14.78 | 14.85 | 21 |
| | | | 15.76 | | | | | | | |
| | | | | | | | | | | 23 |
| | | | 16.47 | | | | | | | |
| 24 | 17.26 | 16.67 | 17.19 | 16.75 | 17.12 | 16.82 | 17.0 | 16.90 | | 24 |
| 25 | 17.98 | 17.37 | 17.91 | 17.44 | 17.83 | 17.52 | 17.75 | 17.60 | 17.68 | 25 |
| 26 | 18.70 | 18.06 | 18.62 | 18.14 | 18.54 | 18.22 | 18.46 | 18.30 | 18.38 | 26 |
| 97 | 10 19 | 1876 | 19.34 | 18.84 | 19.26 | 18.92 | 19.18 | 19.01 | 19.09 | 27 |
| 100 | 90 14 | 10.10 | 20.06 | 10.54 | 10 07 | 10.62 | 10 80 | 10 71 | 19.80 | 28 |
| | | | | | | | | | | 29 |
| | | | 20.77 | | | | | | | |
| 30 | 21.58 | 20.84 | 21.49 | 20,93 | 21.40 | 21.03 | 21.31 | [21,12] | 21.21 | 30 |
| 21 | 22 30 | 2153 | 22.21 | 21.63 | 22.11 | 21.73 | 22.02 | 21.82 | 21.92 | 31 |
| 131 | 00.00 | 99 99 | 22.92 | 29 22 | 99 99 | 22 12 | 29 73 | 99 53 | 99.63 | 3 2 |
| 32 | 23.02 | 32.23 | 22.94 | 22.00 | 00.54 | 00.10 | 00 44 | 00 00 | 0000 | 33 |
| 33 | 23.74 | 22.92 | 23.64 | 23.03 | 23.54 | 23.13 | 23.44 | 23,23 | 23.33 | |
| 34 | 24.46 | 23.62 | 24.35 | 23.72 | 34.25 | 3.83 | 24.15 | 23.94 | 24.04 | 34 |
| 135 | 25.18 | 24.31 | 25.07 | 24.42 | 34.9€ | 4.53 | 24.86 | 24.64 | 24.75 | 35 |
| 136 | 25 90 | 25.01 | 25.79 | 25.12 | 35 68 | 25,23 | 25.57 | 25.34 | 25.46 | 36 |
| | | | 26.50 | | | | | | | |
| 37 | 20.02 | 25.70 | 97.90 | 96 50 | 97.10 | 96.60 | 26.00 | 26.75 | 26.97 | 38 |
| 38 | 27.33 | 26.40 | 27.22 | 20.52 | 27.10 | 20.08 | 20.99 | 20.75 | 20.07 | |
| 139 | 28.05 | 27.09 | 27.94 | 27.21 | 27.82 | 27.34 | 27.70 | 27.46 | 27.58 | 39 |
| 40 | 28.77 | 27.79 | 28.65 | 27.91 | 28.53 | 28.04 | 28.41 | 28.16 | 28.28 | 40 |
| | | | $\frac{1}{29.37}$ | | | | | | | 41 |
| | | | | | | | | | | 42 |
| | | | 30.08 | | | | | | | |
| | | | 30.80 | | | | | | | 43 |
| 4.4 | 31.65 | 30.57 | 31.52 | 30.70 | 31,38 | 30.84 | 31.25 | 30.98 | 31.11 | 44 |
| | | | 32.23 | | | | | | | 45 |
| | | | 32.95 | | | | | | | 46 |
| | | | | | | | | | | 47 |
| 47 | 33.81 | 32.65 | 33.67 | 32.80 | 33,52 | 32.94 | 33.38 | 33.09 | 33.43 | 48 |
| 48 | 34.53 | 33.34 | 34.38 | 33.49 | 34.24 | 33,64 | 34.09 | 33.79 | 33.94 | |
| 4.9 | 35.25 | 34.04 | 35.10 | 34.19 | 34 95 | 34 34 | 34.80 | 34.50 | 34.65 | 49 |
| 50 | 35 97 | 34.73 | 35.82 | 34.89 | 35 66 | 35.05 | 35.51 | 35.20 | 35.36 | 50 |
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| st. | Dep. | Lat. | Dep. | | | | | | | Dis |
| 10 | 460 | 3 | | | 45° | | 45° | | 45° | st. |
| - | 10 | | - | | | | - | | - | - |

II. A TABLE of NATURAL SINES, calculated to five places of figures, for every Minute.

NATURAL SINES are Decimals bearing the same proportion to Unity or 1 that the Sine of the corresponding number of Degrees and Minutes bears to Radius or Sine of 90°. That is, 1 is assumed as the Nat. Sine of 90°, and the Table calculated accordingly.

Explanation of the Table.

To find the Natural Sine of any number of Degrees and Minutes.

If the Degrees be less than 45, look for them at the Top of the Columns, and for the Minutes at the left hand; but if more than 45, look for them at the Bottom, and for the Minutes at the Right hand; under or over the Degrees and against the Minutes will be the Natural Sine required.

The reverse of this will give the Degrees and Minutes corresponding to any Natural Sine.

Note. As the size of the Type on which this Table is printed did not admit of putting 60 Minutes on a page, it will be observed that some of the Degrees begin at the Top and some below the Top of the page; and the Minutes are placed accordingly.

To calculate the Northing or Southing, &c. for any Course and Distance, by Nat. Sines.

Find the Nat. Sine and Co-Sine of the Course, and into each of these multiply the Distance; the Products will be the Latitude and Departure required.

EXAMPLE.

Required the Latitude and Departure for 6 Chains and 22 Links, on a Course N. 38° 27' W.

Nat. Sine of 38° 27, 0.62183 Nat. Co-Sine 0.78315

| | 6.22 | 6 22 |
|--------|-------------|--------------|
| | 10/000 | 1,0000 |
| | , 124366 | 156630 |
| | 124366 | 156630 |
| | 373098 | 469890 |
| | 3.8677826 | 4.8711930 |
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Answer. Northing 4.87 Westing 3.87.

| | , | AIA | | | LON | ALL OF | NES. | | 129 |
|-----|---------|-------|--|-----------------|----------|-----------------------------|----------|-------|-------|
| | 0 | Deg. | 1 | Deg. | 2 | Deg. | 3 | Deg. | |
| M | | | | | | | | | M |
| - | Nat. | N.Co- | Nat. | N.Co- | Nat. | N.Co. | Nat. | N·Co- | |
| | Sine | Sine | Sine | Sine | Sine | Sine | Sine | Sine | |
| - | - | | - | | | - | | | |
| 0 | 00000 | Unit. | 01745 | 99985 | 03490 | | | 99863 | 60 |
| 1 | 29 | 00 | 774 | 84 | 519 | 38 | 263 | 61 | 59 |
| 2 | | 00 | 803 | 84 | 548 | 37 | 292 | 60 | 58 |
| 3 | 87 | 00 | - 832 | 83 | 577 | 36 | 321 | 58 | 57 |
| 4 | 116 | 00 | 3 | | 86 | 1 | 350 | 57 | 56 |
| 1 5 | | 00 | 3 | 82 | | 9- | | 1 | 55 |
| 6 | - 10 | | | | 2 | | | 1 | 54 |
| 7 | | | 4 | | 9 | 1 | 12 | | |
| 8 | 1 -0. | | | 81 | | 1 | 8 | 1 | 53 |
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| £ | 1 202 | | 02007 | 80 | ta. | 4 | 9 | 1 | 51 |
| 10 | ~ , | 00 | | 79 | 731 | 1 | 50 | 1 | 50 |
| 111 | 020 | 99999 | 065 | 79 | 810 | 27 | 553 | 46 | 49 |
| 112 | 0 10 | 99 | 094 | 78 | 839 | 26 | 582 | 44 | 48 |
| 113 | | 99 | | 77 | A | q | 8 | 42 | 47 |
| 14 | | 99 | | 77 | | 4 | - | | 46 |
| 15 | 1 2 | 99 | 181 | 76 | | | 3 | | 45 |
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| 18 | , U~T | 99 | 269 | 74 | 04013 | 19 | 756 | 34 | 42 |
| 19 | 553 | 98 | 298 | 74 | 042 | 18 | 785 | 33 | 41 |
| 20 | 582 | 98 | | 73 | 3 | 17 | 814 | 31 | 40 |
| 21 | | 98 | 4 | 72 | | ,16 | 844 | 3 | 39 |
| 22 | 640 | 98 | | 72 | | 15 | - | 1 | 38 |
| 23 | | | | | 34 | 13 | | 26 | |
| 24 | , ,,,,, | 98 | 9 | 71 | | 2 | | 2 | |
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| 27 | , 00 | 97 | 530 | 68 | 275 | 09 | 06018 | 19 | 33 |
| 28 | U . 1 | 97 | 560 | 67 | 304 | 07 | 047 | 17 | 32 |
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| 36 | | 95 | | 61 | | 97 | 279 | 03 | 24 |
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| 39 | 134 | 94 | | | | | 1 | 3 | 21 |
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| 41 | 164 | 93 | | | | | | | 19 |
| | 193 | 93 | | 1 | | 3 9 | | | |
| 42 | 222 | 93 | | | | | 3 | | 18 |
| 43 | 251 | 92 | 996 | - | | | 9 | | 17 |
| 44 | 280 | 92 | 03025 | 54 | 769 | 86 | | , 88 | 16 |
| 45 | 309 | 91 | 054 | _. 53 | 798 | 85 | 540 | 86 | 15 |
| | N.Co- | | N-Co- | Nat. | N:Co- | Nat. | N:Co- | Nat. | |
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| N | 1 | 4 | Deg. | 5 | Deg. | 6 | Deg. | <u> </u> | leg. | M |
| 1 | | N.S. | NCS, | N.S. | NCS. | N.S. | NCS. | N.S | NCS. | |
| | 0 | 06976 | 99756 | 08716 | 99619 | 10453 | 99452 | 12187 | 99255, | 60 |
| 1 | 1 | 07005 | 54 | 745 | 17 | 482 | 49 | 216 | 51 | 59 |
| | 2 | 034 | 5 2 | 774 | 14 | 511 | 46 | 245 | 4.8 | 58 |
| 1 | 3 | 063 | | | 12 | . 540 | 43 | 274 | 44 | 57 |
| - 1 | 4 | 092 | | | | | | 302 | . 40 | 56 |
| 3 | 5 | 121 | 46 | | 07 | 597 | 37 | 331 | | 55 |
| 4 | 6 | 150 | 44 | | 04 | 626 | 34 | 360 | 33 | 54 |
| | 7 | 179 | 42 | | 02 | 655 | 31 | 389 | 30 | |
| 3 | 8 | 208 | 40 | | 99599 | 684 | 28 | 418 | 26 | |
| | 9 | 237 | 38 | 976 | 96 | 713 | 24 | 447 | 22 | 51 |
| 10 | - 1 | 266 | | 09005 | 94 | 742 | 21 | 476 | 19 | |
| 1 | | 295 | 34 | | 91 | 771 | 18 | 504 | 15 | |
| 1 | _ | 324 | 31 | 063 | 88 | 800 | 15 | 533 | 11 | |
| 1 | - | 353 | 29 | 092 | 86 | \$29 | 12 | 562 | 08 | |
| 1 | | 382 | 27 | 121 | 83 | 858 | 09 | 591 | 04 | |
| 1 | | 411 | $\frac{25}{}$ | 150 | 80 | 887 | 06 | 620 | 00 | 15 |
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| | | | | 09179 | _ | | 99402 | | 99197 | |
| 17 | | 469 | 21 | 208 | 75 | | 99399 | | 93 | 43 |
| 118 | | 498 | 19 | 237 | 72 | 973 | 96 | 706 | 89 | 42 |
| 19 | | 527 | 1.6 | 266 | 70 | 11002 | 93 | 735 | 86 | 4 1 |
| 20 | - 7 | 556 | 14 | 295 | 67 | 031 | 90 | 764 | 82 | 40 |
| 2 | | 585 | 12 | 324 | 64 | 060 | 86 | | 78 | 39 |
| 22 | | 614 | 10 | 353 | 62 | 089 | 83 | 822 | 75 | 38 |
| 25 | Ł | 643 | 0.8 | 382 | 59 | 118 | 80 | 851 | 71 | |
| 24 | | 672 | 05 | 411 | 56 | 147 | 77 | 880 | 67 | |
| 25 | | 701 | 03 | 440 | . 53 | 176 | 74 | 908 | 63 | |
| 26 | | 730 | 01 | 469 | 5 1 | 205 | 70 | .937 | 60 | |
| 27 | | | 99599 | 498 | 48 | 234 | 67 | 966 | 56 | |
| 28 | | 788 | 96 | 527 | 45 | 263 | 64 | 995 | 52 | |
| 29 | | 81.7 | 94 | 556 | 42 | 291 | | 13024 | 48 | |
| 30 |)] | 846 | 92 | 585 | 40 | 320 | 57 | 053 | 44 | 30 |
| | 1 | NCS. | N.S. | NCS. | N.S. | NCS. | NS. | NCS. | N.S. | |
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| M | M N. S.N CS | | | NCS | | N. S. NCS | | | M |
| 31 | 07875 | | 09614 | | | | $\frac{\mathbf{N} \cdot \mathbf{S}}{\mathbf{S}}$ | NCS | |
| 32 | | | 642 | 99531 34 | 11349 378 | 99354 | | 99141 | 29 |
| 33 | | | 671 | 3 l | 407 | 51 47 | 110 | | 28 |
| 34 | 962 | 83 | 700 | 28 | | 44 | 139 | 33 | 27 |
| 35 | 991 | 80 | 729 | 26 | 465 | 41 | 168 | 29 | 26 |
| | 08020 | 78 | 758 | 23 | 494 | 37 | 197 | 25 | 25 |
| 37 | 049 | 76 | 787 | 20 | 523 | 34 | 226 254 | | 24 |
| 38 | 078 | 73 | 81 | 17 | 552 | 31 | 283 | 18 14 | 22 |
| 39 | . 107 | | 845 | - 14 | 580 | 27 | 312 | | 211 |
| 40 | 136 | 68 | 874 | 11 | 609 | 24 | 341 | 06 | 20 |
| 41 | 165 | 66 | 903 | 08 | 638 | 20 | 370 | | 10 |
| 42 | 194 | 64 | 932 | 06 | 667 | 17 | | 99098 | |
| 43 | 223 | 61 | 961 | 03 | 696 | 14 | | | 17 |
| 44 | 252 | 59 | 990 | 00 | 725 | 10 | | | 16 |
| 45 | 281 | 57 | 10019 | 99497 | 754 | 07 | 485 | 87 | 15 |
| 46 | 08310 | 99654 | 10048 | 99494 | 11783 | 99303 | | 99083 | |
| 47 | 339 | 52 | 077 | 91 | 812 | 00 | | | 13 |
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| 5 l | 455 | 42 | 192 | 79 | 927 | 86 | | | 1 4 |
| 52 | 484 | 39 | 221 | 76 | 956 | 83 | | 1 | 8 |
| 53 | | 37 | 250 | 73 | 985 | 79 | 716 | 1 | 1 1 |
| 54 | 542 | 35 | 279 | 70 | 12014 | 7 6 | 744 | . 51 | 6 |
| 55 | | 32 | | | 043 | 72 | | | 5 |
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| 57 | 629 | 27 | 366 | | 100 | 65 | 831 | 39 | 3 |
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| 0 | 13917 | 39027 | | 98769 | - | 98481 | | | |
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| 12 | 263 | 78 | 988 | 14 | 708 | 20 | | 98096 | |
| 13 | | | | 09 | 737 | 14 | | | 47 |
| 14 | | | | | | 09 | 481 | 84 | 46 |
| 15 | 349 | | | 00 | 794 | 04 | 509 | 7 9 | 45 |
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| 19 | 7 | 407 | 57 | 132 | 90 | 852 | 94 | 566 | 67 | 43 |
| 20 | 8 | 436 | | 2 | 86 | 880 | 89 | 595 | 61 | 42 |
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| - 1 | 29 | 443 | | 13025 | 271 | | | 149 | | |
| 3 | 30 | | 00996 | 051 | 259 | 620 | 493 | 175 | 701 | |
| - 1 | | | 90984 | | | | 89480 | 46201 | | |
| - 8 | 32 | 522 | | 10: | 233 | | 467 | 226 | | |
| - 3 | 33 | 549 | | 130 | 221 | 698 | | 2 52 | 661 | |
| - | 34 | 575 | 948 | 156 | 208 | | 441 | 278 | 647 | 26 |
| 1 | 35 | 602 | 936 | 182 | 196 | 750 | 428 | 304 | 634 | 25 |
| 1 | 36 | 628 | 924 | 209 | 183 | 776 | 415 | 330 | 620 | 24 |
| | 37 | 655 | 911 | 235 | 17 i | 802 | 402 | 355 | | |
| | 38 | 681 | 899 | 261 | 158 | 828 | 389 | 381 | 5 93 | |
| 1 | 39 | 707 | 887 | 287 | 146 | | 376 | | 580 | |
| į | 40 | 734 | 875 | 313 | 133 | | 363 | | | |
| | 4 l | 760 | | 340 | 120 | | 350 | 458 | 553 | |
| | 42 | 7 87 | | 366 | 108 | | | 484 | 539 536 | |
| | 43 | 813 | | 392 | 095 | | 324 311 | 5 10 5 36 | 526 512 | |
| | 44 | 840 | | 418 445 | 082 | 984 4501 (| 298 | 561 | 499 | |
| | 45 | 866 | | | | | | N. Col | | |
| | | | Nat. | N. Co Sine | | N. Co Sine. | Nat. Sinc. | | Sine. | TA |
| | M | oine. | Sine. | Sine | Office | Offic. | · JIIIC. | 51110. | 2110. | 161 |
| - | 1 | C . | _ | 6.4 | Deg. | 63 I |)e'cr | 62 I | eg. | • |
| ! | - | 05 | Deg. | | Deg. | 03 1 | Jog. | - J. J. | , S' | 30. |
| | | | 2 | 18 | | | | | | |
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| | 138 A TABLE OF NATURAL SINES. | | | | | | | | | |
|--------------------|-------------------------------|--------------|--------|-------|-------|----------|-------|---|-------|-----|
| 1 | NA | 24 I | Deg. | 25 I | eg. | 26 I | Deg. | 27 1 | | M |
| | M | N. S. | NCS. | N. S. | NCS. | N. S. | NCS. | N. S | NCS. | |
| | 46 | 41892 | 90802 | 43471 | 90057 | 45036 | 89285 | 46587 | 88485 | 14 |
| | 47 | 919 | 790 | | 045 | 063 | | | | 13 |
| | 48 | 945 | | | | | | | 458 | 12 |
| | 49 | 972 | | | | | | | 445 | 1 I |
| | 5 0 | | | | | | | | | 10 |
| | 5 l | 42024 | | | 89994 | | | | | 9 |
| | 52 | 05 l | 729 | | | | | | | 8 |
| 1 | 53 | 077 | 717 | 654 | - 12 | | | | | 7 |
| | 54 | 104 | | 680 | | | | | | |
| | 55 | 130 | | | | | | | | |
| | 56 | 156 | 680 | | | | | | 1 | , , |
| | 57 | | | | | | | | | |
| | 58 | 183 | | | | | | | 1 | _ |
| - | | 209 | | | 892 | 373 | | | | 1 1 |
| | 59 | , 235 | | | | <u> </u> | - | | | |
| | | | | NC3. | | NCS. | | | | M |
| | M | 65 l |)eg. | 64 |) g | 63 1 | Deg. | 62 | Deg. | |
| | = | 28 1 |) e.g. | 29 | Deg | 30] | Deg. | 31 | Deg. | , |
| | M' | | NES. | · | |) | NCS. | \overline{N} . \overline{S} | INCS | M |
| | | 1 | | | | 50000 | · | |] | 60 |
| | 0 | 46947 | | 506 | • | 7 | | | | 1 |
| 1 | 1 | 973 | | | | 2 | | | 1 | , |
| 1 | 2 | 999 | | | | | | | | |
| | 3 | 47024 050 | | | | _ | | | | |
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| | 5 | 076 | 213 | | | T | | | | i |
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| | ્ઠ | 153 | | 710 | 1 | A | | | , | |
| | 9 | 178 | | 735 | | 撰 | | | | |
| | 10 | 204 | | 761 | | 4 | 1 | | 1 | _ |
| | 11 | 229 | | 786 | | P | | | 1 | |
| | 12 | 001 | | 811 | | | | | 1 | |
| | 13 | 281 | 1 | | | 100 | | | 1 | _ |
| | 14 | 306 | 1 | | | | | | 4 | 1 |
| | 15 | 332 | 1 | | | F | | | | .[|
| | 16 | | | | | 50403 | | | | 12 |
| | 17 | 383 | | | | 2 | 1 | _ | į. | 5 |
| | 18 | 409 | | | | _ | 100 | | i i | |
| | 19 | 434 | | | 1.3 | 2 | | | i | 1 |
| | 20 | 460 | | | 3 | | | 52002 | 1 | 3 |
| | 21 | 486 | | 49014 | | | | | | |
| | 22 | 511 | 87993 | | | | | | | |
| | 23 | 537 | 1 | | | | | | | |
| | 24 | 562 | | | | | | | | |
| | 25 | 588 | | | | | | | | |
| | 26 | 614 | 1 | | 093 | | | | | |
| | 27 | 639 | | | | | | | | |
| | 28 | 665 | | · N | | | | | | |
| | 29 | 690 | | | | | | | | _ |
| 1 | 30 | 716 | | | | | 163 | | 264 | |
| 1 | / | \ | | NCS. | N. S. | NCS. | N. S. | NCS. | | |
| 1 | M | 61 1 | Deg. | 60 I | Deg. | 59 I | Deg. | 58 I | eg. | M |
| [14] 61 Deg 60 Deg | | | | | | | | THE RESERVE AND ADDRESS OF THE PARTY OF THE | | - |

| | 114 | 28 | Deg. | 29 | Deg. | 30 | Deg. | 31 | Deg. | |
|---|-----------|------------|-------------|-------|------------|--------------|-------|------------|----------------------|-----|
| | M | NS. | NCS. | N.S. | NCS. | N.S. | NCS. | N.S. | NCS. | M |
| 0 | 31 | 17741 | 87868 | 49268 | 87021 | 50779 | 86146 | 52275 | 85249 | 2.9 |
| 1 | 32 | 767 | | | | | | | 234 | 1 |
| | 33 | 1 | | | 86993 | 4 | | | 218 | |
| | 34 | 010 | | | | | | 349 | | |
| | 35 | 844 | | | | 879 | 089 | 374 | 188 | |
| | 36 | 869 | 798 | | | | | 399 | 173 | |
| | 37 | 895 | 784 | | 935 | 929 | 059 | 423 | 157 | |
| | 38 | 920 | 770 | 445 | 921 | 954 | 045 | 448 | 142 | 22 |
| | 39 | 946 | 756 | 470 | 906 | 979 | 030 | 473 | 127 | 21 |
| | 40 | 971 | 743 | 495 | 392 | 51004 | 015 | 498 | 112 | 20 |
| ۰ | 41 | 997 | 729 | 521 | 878 | | 000 | | 096 | 19 |
| | 42 | 48022 | 715 | 546 | 863 | 054 | 85985 | 547 | 081 | 18 |
| | 43 | 048 | 701 | 571 | 849 | 079 | 970 | 572 | 066 | 17 |
| | 44 | 073 | 687 | 596 | 834 | 104 | 956 | | 051 | 16 |
| | 4.5 | 099 | 673 | 622 | 820 | 129 | 941 | 621 | 035 | 15 |
| | | 48124 | 87659 | 49647 | 86805 | 51154 | 85926 | 52646 | 85020 | 14 |
| | 47 | 150 | 645 | 672 | 791 | 179 | | , | 005 | 13 |
| | 48 | 175 | 631 | 6.97 | 777 | | 2 | 696 | 84989 | |
| | 49 | 201 | 617 | 723 | 762 | | 2 | | | 1 |
| | 50 | 226 | 603 | 748 | 748 | 254 | 866 | 745 | 959 | 10 |
| | 51 | 252 | 5 89 | 773 | 733 | 279 | 851 | 770 | 943 | 9 |
| | 52 | 277 | 575 | 798 | 719 | | 836 | 794 | 928 | 8 |
| | 53 | 303 | 561 | 824 | 704 | 329 | 821 | 819 | 913 | 7 |
| | 54 | 328 | 546 | 849 | 690 | 354 | 806 | 844 | 897 | 6 |
| | 55 | 354 | 532 | 874 | 675 | 379 | 792 | 869 | 882 | 5 |
| | 56 | 379 | 518 | 899 | 661 | 404 | 777 | 893 | 866 | 4 |
| | 57 | 405 | 504 | 924 | 646 | 429 | 762 | 918 | 851 | 3 |
| - | 58 | 430 | 490 | 950 | 632 | 454 | 747 | 943 | 836 | 2 |
| | 59 | 456 | 476 | 975 | 617 | 479 | 732 | 967 | 820 | 1 |
| , | | NCS. | N.S. | NCS. | N.S. | NCS. | N.S. | VCS. | N.S | _ |
| | M | 61 | Jeg. | 60 | Deg. | 59 | Deg. | 58 | Deg. | M |
| | | | | | Deg. | | Deg. | ${35}$ | Deg. | = |
| | M' | | Deg. | N.S. | | 1 | NCS. | N.S. | NCS. | M |
| | , | N.5 | NCS. | | NCs. | | | | | |
| | l . | 52992 | 84505 | 5446- | | | 82904 | 57358 | 8 1915 899 | 60 |
| | 1 1 | 53017 | 789 | 488 | | | | 381 | 882 | 59 |
| | 2 | 041 | 774 | 513 | | | | 405 429 | | 58 |
| | 3 | 066 | 759 | 537 | 819 | 992 | | 453 | 848 | 57 |
| | 4 | 091 | 743 | | | 56016 040 | | 477 | 832 | 55 |
| | 5 | 115 | | | 788 772 | | | | 815 | |
| | 6 | 140 | | | 756 | | | | | 59 |
| | 7 | 164 189 | | 659 | 100 | | | | 782 | 52 |
| | 8 9 | | 1 | | | 1 | | | | |
| | 1 | 000 | | | 708 | | | | | |
| | 10 | 000 | | | 1 | 2 | | | 731 | 49 |
| | 11 | 000 | | 756 | - | | | | | 48 |
| | 12 | | | 781 | 660 | | | | | 47 |
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| | 13 | NCS. | | NCS. | N.S. | NCS. | N.S. | NCS | N.S. | - |
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| | ,vi | 57 | Deg. | 56 | Dec. | 55 | Deg. | 54. | Deg. | |
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| 140 | | | | | NATURAL SINES. 34 Deg. 35 Deg. | | | - | |
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| | 32 | Deg | 33 | Deg. | 34 | Deg. | 35. | Deg. | |
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| M | Nat. | N.Co | Nat. | N. Co | Nât. | N.Co | Nat. | N.Co | $ \mathbf{M} $ |
| | Sine | Sine | Sine | Sine | Sine | Sine | Sine | Sine | |
| | | 3 | | . 1 | 2 | | | | |
| 15 | 33886 | 84557 | 54854 | 83613 | 56305 | 82643 | 57738 | 81647 | 1 1 |
| 17 | 411 | 542 | | | | | | | i i |
| 18 | | 526 | | | | | | | 43 |
| 19 | | | 927 | | 353 | | t e | | |
| | | 511 | | | | 593 | 7 | | 41 |
| 30 | | 495 | | 549 | | 577 | 9 | | |
| 21 | 509 | 480 | | 533 | | 561 | ř | | |
| 22 | 534 | | | 517 | | 544 | 3 | 546 | |
| 23 | 558 | | 55024 | | 473 | 52 8 | 0 | | |
| 24 | 583 | 433 | | •485 | 497 | 511 | 928 | | |
| 25 | 607 | 417 | 072 | 469 | 521 | 495 | 952 | 496 | 35 |
| 26 | 632 | 402 | 097 | 453 | 545 | 478 | 976 | | 34 |
| 27 | 656 | 386 | 121 | 437 | | 462 | 999 | 462 | |
| 28 | 681 | 370 | | 421 | 593 | | 58023 | 445 | 32 |
| 29 | 705 | | | 405 | | 429 | | 428 | |
| 3. | 7:4 | 339 | | 389 | | 413 | | 412 | 30 |
| 3 | 375 | 343~4 | 55218 | 83373 | 56665 | 82396 | 58094 | 81395 | 29 |
| 3∡ | 779 | | 2 | | | 380 | 118 | 378 | 28 |
| 30 | 80 . | 292 | 266 | 340 | 713 | 363 | 141 | 361 | 27 |
| 34 | 82 | 277 | | 324 | | 347 | | 344 | 26 |
| 33 | 853 | 261 | | 308 | 760 | 330 | | 327 | 25 |
| 3. | 877 | 24: | 339 | 29. | 784 | 314 | 212 | 310 | 24 |
| 37 | | | | | 808 | 297 | | 293 | 22 |
| 38 | | | | 260 | 832 | 281 | 260 | 276 | |
| 39 | | 198 | | 244 | 856 | 264 | 283 | 259 | |
| 4(| ~ | | | | | | | | |
| 41 | 975 | | | 228 | 880 | 248 | | 242 | |
| | 54000 | | | 212 | | 231 | 330 | 225 | |
| 42 | V~ - | 151 | 484 | 195 | 928 | 214 | | 208 | |
| 45 | 1 | | | 179 | 9 | 198 | | | 17 |
| 44 | 0.0 | | | 163 | 976 | 181 | | 174 | 16 |
| 45 | 03. | | | | 57000 | 165 | | <u> </u> | 15 |
| 16 | 54122 | | | 83131 | 57024 | | | | 14 |
| 47 | 1.20 | 072 | | | THE STATE OF | 132 | | | 13 |
| 48 | | 057 | 630 | 098 | 071 | 115 | 496 | | 12 |
| 49 | 195 | 041 | 654 | 082 | 095 | 098 | 519 | 089 | 11 |
| 50 | | | | 066 | 119 | 082 | 543 | | 101 |
| 51 | | | | | _ | 065 | 567 | 055 | 9 |
| 52 | | 83994 | | | 100 | 048 | | | 8 |
| 53 | ~ 0.5 | | | | | 032 | | | 7 |
| 54 | , ,,, | | | | | 015 | | | 6 |
| 55 | | | | 82985 | | 81999 | S . | 80987 | |
| 56 | 0 1 ~ | | | | | | | | 5 |
| 57 | | 930 | | | | | | | 4 |
| 58 | 051 | | | | | | | | 3 |
| 59 | 110 | 899 | 871 | | | | | | 2 |
| 39 | 440 | 883 | 895 | 920 | 334 | 932 | 755 | 919 | 1 |
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| NA | N.Co | 74 | N.Co | | N.Co | | N.Co | 0: | |
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| | 57 | Deg. | 56 1 | Jeg. | 55 | Deg. | 54 | Deg. | |
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À TABLE OF NATURAL SINES. 141

| 1 | | 36 I | eg. | 37 I | eg. | 38 l | Deg. | |
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| - | \mathbf{M} | Nat. | N. Co | Nat. | N. Co | | | M |
| | .,, | Sine. | | | Sine. | | | |
| | <u>`</u> | 58779 | 80902 | 60182 | 79864 | 61566 | 78801 | 60 |
| 1 | 1 | 802 | | | 846 | | | 2 4 |
| ı | 2 | 826 | | 228 | 829 | 612 | | 5 |
| | 3 | 849 | | 251 | 811 | 635 | | 1 1 |
| | 4 | 873 | 833 | | 793 | 658 | 729 | 56 |
| | 5 | 896 | | 298 | 776 | 68 i | 711 | 55 |
| | 6 | 920 | 799 | 321 | 758 | 704 | 693 | 54 |
| | 7 | 943 | 782 | 344 | 741 | 726 | 676 | 53 |
| | 8 | 967 | 765 | 367 | 723 | 749 | 658 | 52 |
| | 9 | 990 | 748 | 390 | 706 | 772 | | |
| | 10 | 59014 | 730 | 414 | | | 1 | 50 |
| 1 | 11 | | 3 . | | | 818 | 1 | 1 1 |
| | 12 | 1 | 1 : | a contract of the contract of | | | 1 | 48 |
| | 13 | | | | | | 1 | 347 |
| | 14 | | | | | | | 46 |
| | 15 | 131 | 644 | 529 | 1 | | | 2 45 |
| | i 6 | à . | 80627 | | 1 | 6 | 78514 | |
| 3 | 17 | 178 | | K . | | | | 343 |
| | 18 | 201 | 593 | 5 99 | | | | 342 |
| | 19 | 1 | 4 | | | 62001 | 2 | |
| | 20 | | à | | | | | 240 |
| | 21 | , | 1 | <u> </u> | 100 | | • | 139 |
| | 22 | 4 | 1 | 23 | 1 | | · · | 38 |
| | 23 | | | | | - | | 37 |
| | 24 | 3 | | | 1 | | | 36 |
| | 25 | 3 | 1 | | | | | 35 |
| | 26 | 1 | | a | | | | 3'34 |
| | 27 | | 1 | | 1 | 4 | | 7 32 |
| | 28 | 1 | 1 | | | | | 931 |
| | 29 | ŕ | | 853 | | | | 130 |
| | 30 | | | Ħ | | | | 4 |
| | 1 | | 80368 | | | 6227 | 4 7 8 2 4 | 5 28 |
| | 39 | | | 922 | ž. | 12 | | 627 |
| | 3: | | | 94 <i>5</i> 968 | | 3 | | 826 |
| | 3. | , | 1 | | | 9 | | 025 |
| | i i | 5 599 6 629 | | 61015 | | 100 | | 224 |
| | 3 | | 1 | E . | 1 | | 1 | 425 |
| | 3 | | | | | | | 622 |
| | 3 | | | 2 | 1 | | 4 | 821 |
| | - E | 710 | 1 | 107 | | | | 920 |
| | 4 | | | | | | | 119 |
| | į | 2 76 | | | 122 | | | 3 18 |
| | - 1 | 3 78 | 1 | | | 7 | (| 5 17 |
| | - 1 | 4 809 | | 4 | | 57 | 0 00 | |
| | | 5 83 | | | 069 | 59 | 27798 | 8 15 |
| | - | N.C | o Nat. | N.C | Nat. | IN. C | o Nat | |
| | 1 | A Sine | . Sine | . Sine | . Sine | Sine | Sine | . M |
| | 1 | 1 | | 1 | | 1000 | | |
| | 1 | 1 | | 1 | 1. | | | _ |
| | | 53 | Deg. | 52 | Deg. | 51 | Deg. | |
| | 1 2 | | - | the same of the same of | THE PERSON NAMED IN COLUMN 2 I | | | |

142 A TABLE OF NATURAL SINES.

| 142 | | ADEL | | NATU | KAL | 21115 | |
|-----|-------|-------------|-------------|-------|-------|-------|------|
| 3/1 | | Jeg. | | Deg. | | Deg. | MI |
| M | N S. | NCS | N. S. | NCS | N. S. | NCS. | IVI |
| 40 | 59856 | 80108 | 61245 | 79051 | | | 144 |
| 47 | 1 | | 268 | | | | -,2 |
| 4.8 | | 9 | | | | | 12 |
| 49 | | | | 78998 | | | 7 1 |
| 1 | | | 100 | | | | _ 9 |
| 50 | | | 1 M LANKE | | | | 1 4 |
| 51 | 972 | | 360 | | | | 9 |
| 52 | 9 | | | | | 861 | 8 |
| | | 79986 | | | 40.00 | 843 | 7 |
| 54 | 1 | | | | | 824 | 6 |
| 55 | 1 1 | | | | | 806 | 5 |
| 56 | 1 | | | | | 788 | 4 |
| 57 | 112 | | 7.0 | | | 769 | 3 |
| 58 | 135 | 899 | 520 | 837 | 887 | 751 | 2 |
| 59 | 158 | 881 | 543 | 819 | 909 | 733 | 1 |
| 7 | NCS. | N. S. | NCS | N. 5 | NCS. | N. S. | |
| M | | Deg. | | | | | M |
| | | | | Deg. | 511 | | |
| M | 39 1 | Deg. | 40 l | Deg. | 411 | Jeg. | |
| | | NUS. | | NCS. | | NCS. | M |
| 0 | | | | 76604 | | | 60 |
| 1 | 955 | 696 | | | | | |
| 2 | 977 | 678 | | 9 | | | |
| 3 | 63000 | | | 9 | | _ | |
| 1 1 | | - | | | | | |
| 4 | | | | | | | |
| 5 | 045 | 623 | | 2 | | 375 | |
| 6 | 068 | 605 | 412 | 492 | | 356 | |
| 7 | 090 | 586 | 435 | | | 337 | - 5- |
| 8 | 113 | 5 68 | | 455 | | 318 | |
| 9 | 135 | 550 | | 1 | | 299 | |
| 10 | 158 | 531 | | 417 | | 280 | |
| 11 | 180 | 513 | | 398 | | 261 | |
| 12 | 203 | 494 | 546 | | | 241 | 3 |
| 13 | 225 | 476 | 568 | 361 | 891 | 222 | 47 |
| 14 | 248 | 458 | 590 | 342 | 913 | 203 | 46 |
| 15 | 271 | | 4 | 323 | | 184 | |
| | | | | 76304 | | | |
| 17 | 316 | | | | | 146 | |
| 18 | | 3 | | 3 | 66000 | 126 | |
| 19 | | 7 | | | | 120 | |
| į. | | | | | | | |
| 20 | | | 4 | | 1 | 088 | |
| 21 | 406 | 1 | - | | | 069 | 1 |
| 22 | | | | | | 050 | |
| 23 | | | | | | 030 | |
| 24 | 473 | | 812 | | | 011 | |
| 25 | | | | | | 74992 | |
| 26 | | | | | | 973 | 1 (|
| 27 | 540 | | 878 | 097 | 197 | 953 | 33 |
| 28 | 563 | 199 | 901 | 078 | 218 | 934 | 32 |
| 29 | | | 923 | 059 | 240 | 915 | 31 |
| 30 | | | | | 262 | | |
| - | NCS. | | NCS. | | NCS. | | |
| M | | | | - 1 | | | M |
| | 50 1 | Deg | 49 | Deg. | 48 | Deg. | 1 |

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| | A | TABI | LE OF | NAT | 'URA | LSIN | ES. I | 43 | |
|---|-----|--------------|-------|--|-------|-------|-------|-----|----|
| - | 171 | 39] | Deg. | 40] | Deg. | 41 1 | Deg. | 1 | |
| | M | N.S. | NCS. | N. S. | NCS. | N. S. | - | M | |
| | 31 | | | | | 66284 | | 00 | |
| | 32 | 63630 | | 989 | 003 | | | | |
| | 33 | 653 | | | 75984 | | 838 | 3 | |
| | 34 | 675 | | • | | | | | |
| | 35 | 698 | | 033 | | | 818 | | |
| | 36 | | | | - | | 799 | | |
| | 1 | 1.2~ | | 077 | 100 | | | | |
| | 37 | . 00 | | | , | | | | |
| | 38 | | | | 1 | | | _ | |
| | 39 | | 76996 | | 1 | | 722 | _ | |
| | 40 | | | | | | | | |
| | 41 | 854 | | 188 | | | 683 | | |
| | 42 | | | 210 | | | | | |
| | 43 | 899 | | 232 | | | | | |
| - | 44 | | | | | 4 | | | |
| | 45 | 944 | 884 | 276 | 756 | 588 | 606 | 15 | |
| | 46 | 63966 | 76866 | 65298 | | 66610 | 74586 | 14 | |
| | 47 | 989 | 847 | 320 | 719 | 632 | .567 | 13 | |
| | 48 | 64011 | 828 | 342 | 699 | 653 | 548 | 12 | |
| | 49 | | | 364 | | 675 | 528 | 11 | |
| 1 | 50 | | | 386 | | 697 | 509 | 10 | Ì |
| | 51 | 078 | | 408 | | 718 | 489 | 9 | |
| | 52 | | - 61 | 430 | 1 _ | 740 | 470 | 8 | |
| | 53 | | | | | | 451 | | |
| | 54 | | | 474 | | | | 6 | ı |
| | 55 | | - 11 | | | 3 | | | |
| | 56 | | | 4 | 1 | | | | ı |
| | 57 | | | | - 100 | | | _ | - |
| | 58 | | 3.7 | | 1 | | | | |
| | 59 | | | 10 | | | • | | ı |
| | | | | 16 | ; | E | | 1 1 | I |
| | M | NCS. | N. S. | | | NCS. | | M | ı |
| | 741 | 5 0] | Deg. | 49 | Deg. | 48 | Deg. | | l |
| | - | | Deg. | 43 | Deg | 44 | Deg. | = | l |
| | M | | | | | | | M | ۱ |
| | | | NCS. | | NCS. | 5 | NCS. | | |
| | 0 | | 74314 | | | | 71934 | 6(| 1 |
| | 1 | 935 | | | | 487 | 914 | 50 | - |
| | 2 | | | at the same of the | | | | 58 | |
| | 3 | 978 | | 264 | | | 873 | 57 | - |
| | 4 | 999 | | | | _ | | 56 | |
| | 5 | | | | | | | 54 | 1 |
| | 6 | 043 | | 327 | | | 813 | 54 | |
| | 7 | 064 | | 349 | 72996 | | 792 | 53 | - |
| | 8 | 086 | 159 | 370 | 976 | 633 | 772 | 52 | ŀ |
| | 9 | 107 | 139 | 391 | 957 | | 752 | 51 | - |
| | 10 | 129 | 120 | 412 | 937 | 675 | 732 | 50 | |
| | 11 | 151 | 100 | 435 | 917 | 696 | | 49 | 1 |
| | 12 | 172 | | 455 | 897 | 717 | 691 | 48 | |
| | 13 | 194 | | 471 | 877 | 737 | 671 | 47 | |
| | 14 | 215 | 041 | 497 | 857 | 758 | 650 | 46 | |
| | 15 | 237 | 022 | 518 | 837 | 779 | | 45 | |
| | | NCS. | N.S | NCS. | | NCS. | | | |
| | M | | - | | | | | M | |
| 1 | | 47 I | Deg. | 46 I | Deg. | 45 I | | | |
| | - | | | | | - | | | 41 |

| | 4.4 | AT | ABLE | | | JRAL SINE | | | 1 |
|---|------------|--------------|---|---|-------|------------|-------------|----|---------------|
| | 1 | [42] | Deg. | 43 | Deg | 44 | Deg | | - |
| | | | | | | (to 10 | | | i |
| | M | Nat. | | | N. Co | | N.Co | 2 | |
| | | Sine | Sine. | Sine. | Sine. | Sine. | S ne. | | Į |
| | | | | | 1 | | | / | |
| 1 | 16 | 67258 | 74002 | 68539 | 72817 | 69800 | 7:610 | 44 | - |
| | 17 | | 73983 | 4. 4 | 797 | | 5 90 | | ш |
| I | 18 | 301 | | | | 842 | 569 | , | - |
| | 19 | | - | | | 862 883 | 549 529 | | Į |
| 1 | 20 | 344 | 924 | | | 904 | 508 | | |
| ı | 21 | 366 | | | 697 | | 488 | | |
| Ì | 22 23 | 387 409 | 865 | 688 | | | 468 | | - |
| ì | 24 | 430 | | 400 | | 966 | 447 | | |
| Ì | 25 | | | W 70 C | | 987 | 427 | | |
| 1 | 26 | 473 | | | 617 | 70008 | 407 | 34 | |
| | 27 | | | 772 | | | 386 | | |
| | 28 | | | 793 | | | 366 | | - |
| į | 29 | 538 | 747 | | | | 345 | 31 | - |
| | 30 | | | | | 091 | 325 | | н |
| I | 31 | 67580 | 73708 | 68857 | 72517 | 70112 | 71305 | 29 | - |
| I | 32 | 602 | | 878 | 497 | 132 | 284 | | |
| 1 | 33 | 7 | * | 899 | | 158 | 264 | 27 | |
| Ì | 34 | | | 920 | | 174 | | 20 | |
| I | 35 | 666 | | | | 195 215 | 223 203 | 23 | - |
| - | 36 | - (| | | | 4.0 | | 23 | and and |
| Ì | 37 | | | $\begin{array}{c} 983 \\ 69004 \end{array}$ | | | | 22 | - |
| 1 | 38 | | | | | | 141 | 21 | To a grand |
| Ì | 39 40 | 752 773 | | | | 0.0 | 121 | 20 | - |
| 1 | 41 | 795 | 1 | | | | | 19 | National Park |
| Ì | 42 | 816 | | | 297 | 339 | | | |
| 1 | 43 | 837 | | | 277 | 360 | | | |
| ı | 44 | 8 5 9 | | | 257 | | | 3 | и |
| Į | 45 | 880 | 432 | 151 | 236 | 401 | 019 | - | l |
| | 46 | 67901 | 73412 | 69172 | 72216 | 70422 | | | |
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| | 48 | | 373 | | | | | | |
| | 4 9 | 965 | | | 1 | | | | |
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| | _ | 68008 | | | | 525 | | | - |
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| | 53 | | | 4 | 4 | 587 | 834 | | |
| | 54 55 | | | | | 608 | | | |
| | 56 | | $\begin{array}{c} 234 \\ 215 \end{array}$ | | | 628 | | | |
| | 57 | 0 | 3 | | 71995 | 649 | 772 | | |
| | 58 | | | | | 670 | 752 | | |
| | 59 | | | | | 690 | 731 |] | |
| | 60 | 200 | | | | 711 | 711 | O | - |
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| | | N.Co | Nat. | N.Co | Nat. | N.Co | | | |
| | M | Sine. | Sine. | Sine. | Sine. | Sine. | Sine | M | |
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| | | 47 I | 47 Deg. 46 Deg. | | | 45 1 | Deg. | | |

111. A TABLE of LOCARITHMS for NUMBEBS; and

IV. A TABLE of LOGARITHMIC OF ARTIFICIAL SINES, TAN-

Explanation of the Table of Logarithms for Numbers.

LOGARITHMS are Numbers in Arithmetical Progression, corresponding to other Numbers in Geometrical Proportion. As,

0. 1. 2. 3. 4. Logarithms. 1. 10. 100. 1000. Numbers.

The Logarithm for any Number less than 10 is a certain number of Decimals; for any number between 10 and 100 it is 1 with Decimals; for any Number between 100 and 1000 it is 2 with Decimals, &c. The whole Number in Logarithms, or the Number which stands at the Left hand of the Decimal Point is called the Index; and is always a Unit less than the places of figures in the whole Number for which it is the Logarithm: Thus,

The Log. of 6543 - is - 3.81578 654.3 - - 2.81578 65.43 - - 1.81578 6.543 - - 0.81578

The Log. of a Decimal Fraction is the same as that of an Integer, only the Index is negative; and is distinguished from an absolute one by placing a Point or a negative Sign before it: Thus,

The Log. of 0.6543 - is - .9.81578 or — 1.81578 0.06543 - - .8.81578 or — 2.81578

By the following Table the Log. of any number, containing three places of figures, whether whole numbers, mixed Num-

bers or Decimals, may be found true at once.

Look for the two first figures in the Left or Right hand Column, marked No. and for the third figure on the Top of the Page; against the two first figures and under the third will be the Logarithm.

EXAMPLES.

Required the Logarithm for 346.

Look for 34 in the Column marked No. and for 6 on the Top of the Page, under which and against 34 you find 53908 to which prefix 2 for the Index, because the Number consists of three places of figures.

In the same way the Log. for 28.3 will be found to be 1.45179

And the Log. for 3.23 to be 0.50920

To find the Number corresponding to any Logarithm.

Look in the Table till you find the given Log. without regarding the Index; the Number standing against it in the Column marked No. together with the figure on the Top, from the corresponding Number; whether whole, mixed or Decimals, will be determined by the Index. If you cannot find the exact Log. take the nearest to it.

If the Log. of any Number between 10 and 100, with two places of Decimals, be required, take the nearest number of tenths, which will be sufficiently exact for common practice. But, if great accuracy be desired, work by Natural Sines, in the manner pointed out in Trigonometry, and in the Introduction to

the Table of Natural Sines. Or,

The Log. of any Number containing more than three places of figures, may be found by the Table in this Book, as follows:

Find the Log. of the three first figures as before taught, sub-

19

tract that from the next greater Log. contained in the Table; multiply the difference by the remaining figure or figures in the given Number, and from the Product cut off as many figures from the Right hand as remain in the given Number; add the figure or figures, standing at the Left hand to the Log. of the three first figures, and the Sum will be the Log. required, to which prefix the proper Index.

I. Required the Logarithm of 7624 Log. of 763 - -

g. of 763 - - 188252 762 - - 188195

Difference - - 57 Remaining figure - 4

22.8

Log. of 762 - 88195 Required Log. 3.88217

Note. This is also the Log. of 762.4 or 76.24, &c. varying the Index according to the preceding directions.

2. Required the Logarithm of 541.25

Log. of 542 - - .73400 541 - - .73320

Difference - - 80

Remaining figures of the given Numb. 25

400 160

20.00 Log. of 541 - - .73320

Required Log. - 2.73340

To find the nearest Number corresponding to any Logarithm

for more than three places of figures.

Find the Log. next less than the given one, and take the difference between that and the given one; also take the difference between the next greater and the next less Log. than the given one; divide the former difference by the latter, according to the Rule in Division of Decimals; add the Quotient to the number answering to the Log. next less than the given one, and you will have the required Number; whether a whole or a mixed Number will be determined by the Index.

EXAMPLES.

1. Required the Number to the Logarithm 3.88218
Given Log. - .88218 Next greater Log. -

Next less - .88195 Next less - - - .88195

Difference - 23 Difference - 57

57)23.0(4

The Number to the Log. next less than the given one is 7620 because the Index is 3; to this add 4 and it makes 7624 the required Number.

2. Required the Number to the Logarithm 2.73340

| Given Log. Next less | 73340 73320 | Next greater Next less | Log | .734 | |
|-------------------------|----------------|---------------------------|-----|------|----|
| Difference | - 20 | Differen | ce | - | 80 |
| | 80) |)20.00 (25 160 | i | | |
| | | | | | |

400 400

The Number to the Log. next less than the given one is 541. to this add the figures in the preceding Quotient, which are known to be Decimals from the Index of the given Log. and the required Number will be 541,25

The addition and subtraction of Logarithms answers the same purpose as the multiplication and division of their corresponding Numbers: That is, the Log. of any two Numbers being added, their Sum will be the Log. of the Product of those Numbers; and the Log. of one Number being subtracted from the Log. of another Number, the Remainder will be the Log. of the Quotient of one of those Numbers divided by the other. Again, the Log. of any Number being doubled will produce the Log. of the Square of that Number; and one half the Log. of any Number is the Log. of the Square Root of that Number.

To perform Addition or Subtraction by Logarithms. The following Theorems for adding and subtracting by Logarithms were invented by Mr. EBENEZER R. WHITE of DANBURY, and by him communicated to the Compiler. Thoughtin common cases, they may not be particularly useful, yet in the solution of many Mathematical Questions they will greatly abridge the numerical operation. They are therefore here inserted.

Let a = greater greater b = lesser number to be added or subtracted.

Then $\frac{a}{b} + 1 \times b = a + b$

 $\operatorname{And} \frac{a}{b} - 1 \times b = a - b$

These Theorems may be expressed in words as follows: From the Log. of the greater number subtract the Log. of the lesser, and find the number corresponding to the Remainder: Then, if the original numbers are to be added together, add 1 to the number last found; but if they are to be subtracted, subtract 1 from it; and the Log. of the number thus increased or diminished added to the Log. of the lesser original number, will give the Log. of the Sum or Difference required.

Of the Table of Logarithmic or Artificial Sines, Tan-GENTS and SECANTS.

To find the Logarithmic Sine, &c. for any number of Degrees

and Minutes, within the Compass of the Table.

If the Degrees be less than 45, look for them at the top of the Columns, and under Sine, Tangent or Secant, whichever is wanted, and for the Minutes at the left hand; but if more than 45, look for the Degrees at the Bottom over Sine, &c. and for the Minutes at the Right hand; under or over the Degrees and against the Minutes will be the required Log. Sine, &c.

To find the Degrees and Minutes corresponding to a given

Logarithmic Sine, &c.

Look in the proper Column for the nearest Log. to the given one; and the Degrees and Minutes standing over or under and against it, are those required.

Note. When the Log. Sine, &c. for more than 90° is required, subtract the given number of Degrees from 180° and

make use of the Remainder.

It will be observed that this Table is calculated only for every 5 Minutes. This was thought sufficient for Surveyors, as few Compasses will take a Course to greater exactness. however a Question is to be solved where greater accuracy is required, work by natural Sines. Or,

The Log. Sine, &c. for any Minute may be found as follows: Look in the Table for the Log. of the nearest number of Minutes greater than the given one, and from this subtract the next less Log. contained in the Table: Then say, As 5 Minutes, Is to this difference; So is the excess of the given Minutes above 5, 10, 15, 20, 25, &c; To a fourth number, which add to the Log. of the Minutes next less than the given number, and the sum will be the Log. required.

EXAMPLE.

| 73 | 17 T | C 2 40 001 | |
|------------|---|-------------------|---|
| Kequirea i | the Logarithmic Sine of Sine of 34° 25' 34 20 | 9.7522 9.7512 | |
| | | 1 | _ |
| | Difference | 9 | 3 |
| As | 5:93::3:56 Sine of 34° 20' - | - 9.75128 | |
| | Add Sine of 34° 23' - | - 56 - 9.75184 | - |

To find the nearest Minutes corresponding to a given Log-

arithmic Sine, &c.

Look in the Table, in the proper Column, for the Log. next less than the given one, and take the difference between that and the given one; also take the difference between the next greater and the next less Log, than the given one; Then say, As the latter difference; Is to 5 Minutes; So is the former difference; To the number of Minutes to be added to the Minutes of the Log. next less than the given one.

EXAMPLE.

Required the Degrees and Minutes corresponding to the Logarithmic Tangent 9.73597.

Given Log. - 9.73597 Next greater Log. - 9.73627 Next less - 9.73476 Next less - - - 9.73476

Difference 121 Difference 151

As 151:5::121:4

The Degrees and Minutes for the Log. next less than the given one are 28° 30' to which add 4' and it makes 28° 34'

Note. As after the most careful attention of the Printers, some figures in the Table may be wrong; and as some may be so blurred as to be illegible, let it be observed, that the Sines and Co-Secants, the Co-Sines and Secants, and the Tangents and Co-Tangents, standing against each other respectively, being added together, will amount to 20.00000, if the Tables are accurate. Thus against 28° 20' the Sine 9.67633 added to the Co-Secant 10.32367 their Sum is 20.00000; so also is the Sum of the Co-Sine 9.94458 and the Secant 10.05542, and likewise the sum of the Tangent 9.73175 and the Co-Tangent 10.26825. An error may consequently be easily detected, or any defaced figure be supplied.

To calculate the Northing or Southing, &c. for any Course and Distance by Logarithms.

This is done by the first Case of RIGHT ANGLED TRIGO-

NOMETRY, as follows:

Find the Log. Sine and Co-Sine of the Course; to each of these add the Log. of the Distance; subtract Radius or 10.00000 from their Sums, and the Remainders will be the Log. of the required Latitude and Departure.

Note. When the Angle is very small or very large, and the Distance short, the sum of the Log. Sine or Co-Sine and the Log. of the Distance may be less than 10.00000 or Radius, which cannot therefore be subtracted. In such cases look for the Log. without regard to the Index, and the corresponding Number will be a Decimal, the first Figure of which will be Tenths if the Index be 9, and Hundredths if the Index be 8.

| I | 1 0 |) 1 | 2 | 3 | 4 | |
|-----|---------|---------|---------|---------------|---------|-----|
| No | | | 4 | | | No |
| 1 | 0.00000 | 0.01139 | 0.0.918 | 0.11394 | 0.14613 | 1 |
| 2 | 30103 | 32222 | | 36173 | | 2 |
| 3 | 47712 | 49136 | 50515 | 51851 | | 3 |
| 4 | 60206 | 61278 | 62325 | 63347 | 64345 | 4 |
| 5 | 69897 | 70757 | 71600 | 72428 | 73239 | 5 |
| 6 | 77815 | 78533 | 79239 | 79934 | 80618 | 6 |
| 7 | 84510 | 85126 | 85733 | 86332 | 86923 | 7 |
| 8 | 90309 | 90849 | 91381 | 91908 | | 8 |
| 9 | 95424 | 95904, | 96379 | | 97313 | 9 |
| 10 | 1.00000 | 1.00432 | 1.00860 | 1.01284 | 1.01703 | 10 |
| 11 | 1.04139 | 1.04532 | 1.04922 | 1.05308 | 1.05690 | 11 |
| 12 | 07918 | 08279 | 08636 | 08991 | 09342 | 12 |
| 13 | 11394 | 11727 | 12057 | 12385 | 12710 | 13 |
| 14 | 14613 | 14922 | 15229 | 1 5534 | 15836 | 14 |
| 15 | 17609 | 17898 | 18184 | 18469 | 18752 | 15 |
| 16 | 20412 | 20683 | 20951 | 21219 | 21484 | 16 |
| 17 | 23045 | 23300 | 23553 | 23805 | 24055 | 17 |
| 18 | 25527 | 25768 | 26007 | 26245 | 26482 | 18 |
| 19 | 27875 | 28103 | 28330 | 28556 | 28780 | 19 |
| 20 | 30103 | 30320 | 30535 | 30750 | 30963 | 20 |
| 21 | 1.32222 | 1.32428 | 1.32634 | 1.32838 | 1.33041 | 21 |
| 22 | 34242 | 34439 | 34635 | 34830 | 35025 | 22 |
| 23 | 36173 | 36361 | 36549 | 36736 | 36922 | 23 |
| 24 | 38021 | 38202 | 38382 | 38561 | 38739 | 24 |
| 25 | 39794 | 39967 | 40140 | 40312 | 40483 | 25 |
| 26 | 41497 | 41664 | 41830 | 41996 | 42160 | |
| 27 | 43136 | 43297 | 43457 | 43616 | 43775 | 27 |
| 28 | 44716 | 44871 | 45025 | 45179 | 45332 | 28 |
| 29 | 46240 | 46389 | 46538 | 46687 | 46835 | 29 |
| 30 | 47712 | 47857 | 48001 | 48144 | 48287 | 30 |
| 31 | 1.49136 | 1.49276 | 1.49415 | 1.49554 | 1.49693 | 31 |
| 32 | 50515 | 50650 | 50786 | 50920 | 51054 | 32 |
| 33 | 51851 | 51983 | 52114 | 52244 | 52375 | 83 |
| 34 | 53148 | 53275 | 53403 | 53529 | 53656 | 34 |
| 35 | 54407 | 54531 | 54654 | 54777 | 54900 | 35 |
| 36 | 55630 | 55751 | 55871 | 55991 | | 36 |
| 37 | 56820 | 56937 | 57054 | 57171 | | 37 |
| 38 | 57978 | 58092 | 58206 | 58320 | | 38 |
| 39 | 59106 | 59218 | 59329 | 59439 | 59550 | 39 |
| 40 | 60206 | 60314 | 60423 | 60530 | 60638 | 40 |
| 41 | 1.61278 | 1.61384 | 1.61490 | 1.61595 | 1.61700 | 41 |
| 42 | 62325 | 62428 | 62531 | 62634 | 62737 | 1 |
| 43 | 63347 | 63448 | 63548 | 63649 | 63749 | |
| 44 | 64345 | 64444 | 64542 | 64640 | 64738 | - 1 |
| 45 | 65321 | 65418 | 65514 | 65610 | 65706 | |
| 46 | 66276 | 66370 | 66464 | 66558 | 66652 | - 1 |
| 47 | 67210 | 67302 | 67394 | 67486 | | 47 |
| 4.8 | 68124 | 68215 | 68305 | 68395 | 68484 | |
| 49 | 69020 | 69408 | 69197 | 69285 | 69373 | - } |
| 50 | 69897 | 69981 | 70970 | 70157 | 70242 | |
| 170 | 00001 | | | | | 1 |
| | | | | | | |

| 1 | 5 | 6 | 7 | 8 1 | 9 | 1 |
|----|----------------|--|---------|----------------|----------------|-----|
| No | | | | | | No |
| 1 | 0.17609 | 0.20412 | 0.23045 | 0.25527 | 0.27875 | 1 |
| 2 | 39794 | 44497 | 43136 | 44716 | 46240 | 2 |
| 3 | 54407 | 55630 | 56820 | 57978 | 59106 | 3 |
| 4 | 65321 | 66276 | 67210 | 68124 | 69020 | 4 |
| 5 | 74036 | 74819 | 75587 | 76343 | 77085 | 5 |
| 6 | 81291 | 81954 | 82607 | 83251 | 83885 | 6 |
| 7 | 87506 | 88081 | 88649 | 89209 | 89763 | 7 |
| 8 | 92942 | 93450 | 93952 | 94448 | 94939 | 8 |
| 9 | 97772 | 98227 | 98677 | 99123 | 99564 | 9 |
| 10 | 1.02119 | 1.02531 | 1.02938 | 1.03342 | 1.03743 | 10 |
| 11 | 1.08070 | 1.06446 | 1.03819 | 1.07188 | 1.07555 | 11 |
| 12 | | 10037 | 10380 | 10721 | 11059 | 12 |
| 13 | 13033 | 13354 | 13672 | 13988 | 14302 | 13 |
| 14 | | 16435 | 16732 | 17026 | 17319 | 14 |
| 15 | 19033 | 19312 | 19590 | 19866 | 20140 | 15 |
| 16 | 21748 | 22011 | 22272 | 22531 | 22789 | 16 |
| 17 | 24304 | 24551 | 24797 | 25042 | 25285 | 17 |
| 18 | 26717 | 26951 | 27184 | 27416 | 27646 | 18 |
| 19 | 29003 | 29226 | 29447 | 29667 | 29385 | 19 |
| 20 | 31175 | 31387 | 31597 | 31806 | 32015 | 20 |
| 21 | 1.33244 | 1.33445 | 1.33646 | 1.33846 | 1.34044 | 21 |
| 22 | 35218 | 35411 | 35603 | 35793 | 35984 | 22 |
| 23 | 37107 | 37291 | 37475 | 37658 | 37340 | 23 |
| 24 | 38917 | 39093 | 39270 | 39445 | 39620 | 24 |
| 25 | | | | 41162 | | |
| 26 | | 42488 | 42651 | 42813 | 42975 | 1 3 |
| 27 | | 44091 | 44248 | 44404 | | |
| 28 | | 45637 | 45788 | 45939 | 46090 | 28 |
| 29 | 46982 | 471.29 | 47276 | 47422 | | |
| 30 | 48480 | 48572 | 48714 | 48855 | 48996 | 30 |
| 31 | 1.49831 | 1.49969 | 1.50106 | 1.50243 | 1.50379 | 31 |
| 32 | 51188 | 51322 | 51455 | 51587 | 51720 | 32 |
| 33 | 52504 | 52634 | 52763 | 22892 | | 1 |
| 34 | 53782 | 53908 | 54033 | 54158 | | |
| 35 | 55023 | 55145 | 55267 | 55388 | | 35 |
| 36 | 56229 | 56348 | 56467 | 56585 | | 1 |
| 37 | 57403 | 57519 | 57634 | 57749 | 57864 | 1 3 |
| 38 | 58546 | 58659 | 58771 | 58883 | | |
| 39 | 59660 60746 | 59770 | 59879 | 59988 | | |
| 40 | - | 60853 | 60959 | 61066 | 61172 | |
| 41 | 1.61805 | 1.61909 | 1.62014 | 1.62118 | | 41 |
| 42 | 62839 | 62941 | 63043 | 63144 | 63246 | 1 1 |
| 43 | 63849 | 63949 | 64048 | 64147 | | |
| 44 | 64836 | 64933 | 65031 | 65128 | | 44 |
| 45 | 65801 | 65896 | 65992 | 66087 | 66181 | 45 |
| 46 | 66745 | 66839 | 66932 | 67025 | | 46 |
| 47 | 67669 | 67761 | 67852 | 67943 | 68034 | 1 1 |
| 48 | 68574 | 68664 | 68753 | 68842 | 68931 | 48 |
| 49 | 69461 70329 | 69548 | 69636 | 69723 70586 | 69810 70672 | |
| 50 | 10329 | 70415 | 70501 | 10380 | 10072 | 50 |
| | - | The state of the s | | | | - |

| No | | 104 | 11 1 | Apre | | ANILII | | |
|--|---------------|--|---------|--|---------|---------|---------|-----|
| 52 71600 71684 71767 71850 71933 52 53 72428 72509 72591 72673 72754 53 54 73239 73320 73400 73480 73560 54 55 74036 74115 74194 74273 74351 55 56 74819 74896 74974 75051 75128 56 57 75587 75664 75740 75815 75891 57 58 76343 76418 76492 76567 76641 58 59 77085 77159 77305 77379 59 60 77815 77887 77960 78032 78104 60 61 1.78533 1.78604 1.78675 1.78746 1.78817 61 62 79239 79309 79379 79449 79518 62 63 7934 80003 80072 80140 80209 | | No | 0 | 1 | 2 | 3 | • 4 | No |
| 52 71600 71684 71767 71850 71933 52 53 72428 72509 72591 72673 72754 53 54 73239 73320 73400 73480 73560 54 55 74036 74115 74194 74273 74351 55 56 74819 74896 74974 75051 75128 56 57 75587 75664 75740 75815 75891 57 58 76343 76418 76492 76567 76641 58 59 77085 77159 77305 77379 59 60 77815 77887 77960 78032 78104 60 61 1.78533 1.78604 1.78675 1.78746 1.78817 61 62 79239 79309 79379 79449 79518 62 63 7934 80003 80072 80140 80209 | į | 51 | 1.70757 | 1.70842 | 1.70927 | 1.71012 | 1.71096 | 51 |
| 54 .73239 73320 73400 73480 73560 54 55 74036 74115 74194 74273 74351 55 56 74819 74896 74974 75051 75128 56 57 75587 75664 75740 75815 75815 776641 58 59 77085 77159 77232 77305 77379 59 60 77815 77887 77960 78032 78104 60 61 1.78533 1.78604 1.78675 1.78746 1.78817 61 62 79239 79309 79379 79449 79518 62 63 79934 80003 80072 80140 80209 63 64 80618 80686 80754 80821 80889 64 65 81291 81358 81425 81491 81558 65 68 83251 83315 83378 <td></td> <td>52</td> <td>71600</td> <td></td> <td>71767</td> <td>71850</td> <td>71933</td> <td>52</td> | | 52 | 71600 | | 71767 | 71850 | 71933 | 52 |
| 55 74036 74115 74194 74273 74351 55 56 74819 74896 74974 75051 75128 56 57 75587 75664 75740 75815 75891 57 58 76343 76418 76492 76567 76641 58 59 77085 77159 77305 77379 59 60 77815 77887 77960 78032 78104 60 61 1.78533 1.78604 1.78675 1.78746 1.78817 61 62 79239 79309 79379 79449 79518 62 63 79934 80003 80072 80140 80209 63 64 80618 80686 80754 80821 80889 64 65 81291 81358 81425 81491 81558 65 66 81954 82020 82686 82151 82217 | | 53 | 72428 | 72509 | 72591 | 72673 | 72754 | 53 |
| 56 74819 74896 74974 75051 75128 56 57 75587 75664 75740 75815 75891 57 58 76343 76418 76492 76567 76641 58 59 77085 77159 77232 77305 77379 59 60 77815 77867 77960 78032 77305 77379 59 61 1.78533 1.78604 1.78675 1.78746 1.78817 61 62 79239 79309 79379 79449 79518 62 63 79934 80003 80072 80140 80209 63 64 80618 80686 80754 80821 80889 64 65 81291 81358 81425 81491 81558 82217 66 68 83251 83315 83378 83442 83506 68 69 83885 83948 | | 54 | .73239 | 73320 | 73400 | 73480 | 73560 | 54 |
| 57 75587 75664 75740 75815 75891 57 58 76343 76418 76492 76567 76641 58 59 77085 77159 77232 77305 77379 59 60 77815 77887 77960 78032 78104 60 61 1.78533 1.78604 1.78675 1.78746 1.78817 61 62 79239 79309 79379 79449 79518 62 63 79934 80003 80072 80140 80209 63 64 80618 80686 80754 80821 80889 64 65 81291 81358 81425 81491 81558 65 66 81954 82020 82086 82151 82217 66 67 82607 82672 82737 82802 82866 67 68 83251 83315 83378 83442 | | 55 | 74036 | 74115 | 74194 | 74273 | 74351 | 55 |
| 58 76343 76418 76492 76567 76641 58 59 77085 77159 77232 77305 77379 59 60 77815 77887 77960 78032 78104 60 61 1.78533 1.78604 1.78675 1.78746 1.78817 61 62 79239 79309 79379 79449 79518 62 63 79934 80003 80072 80140 80209 63 64 80618 80686 80754 80821 80889 64 65 81291 81358 81425 81491 81558 65 66 81954 82020 82086 82151 82217 66 68 83251 83315 83378 83442 83506 68 69 83885 83948 84011 84073 84136 69 71 1.85162 1.85187 1 35248 1.85 | İ | 56 | 74819 | 74896 | 74974 | 75051 | 75128 | 56 |
| 58 76343 76418 76492 76567 76641 58 59 77085 77159 77232 77305 77379 59 60 77815 77887 77960 78032 78104 60 61 1.78533 1.78604 1.78675 1.78746 1.78817 61 62 79239 79309 79379 79449 79518 62 63 79934 80003 80072 80140 80209 63 64 80618 80686 80754 80821 80889 64 65 81291 81358 81425 81491 81558 65 66 81954 82020 82086 82151 82217 66 68 83251 83315 83378 83442 83506 68 69 83885 83948 84011 84073 84136 69 71 1.85162 1.85187 1 35248 1.85 | l | 57 | 75587 | 75664 | 75740 | 75815 | 75891 | 57 |
| 60 77815 77887 77960 78032 78104 60 61 1.78533 1.78604 1.78675 1.78746 1.78817 61 62 79239 79309 79379 79449 79518 62 63 79934 80003 80072 80140 80209 63 64 80618 80686 80754 80821 80889 64 65 81291 81358 81425 81491 81558 65 66 81954 82020 82086 82151 82217 66 67 82607 82672 82737 82802 82866 67 68 83251 83315 83378 83442 83506 68 69 83885 83948 84011 84073 84136 69 70 84510 84572 84634 84696 84757 70 71 1.85162 1.85187 185248 1.853 | - | | 76343 | 76418 | 76492 | 76567 | 76641 | 58 |
| 61 1.78533 1.78604 1.78675 1.78746 1.76817 61 62 79239 79309 79379 79449 79518 62 63 79934 80003 80072 80140 80209 63 64 80618 80686 80754 80821 80889 64 65 81291 81358 81425 81491 81558 65 66 81954 82020 82086 82151 82217 66 67 82607 82672 82737 82802 82866 67 68 83251 83315 83378 83442 83506 68 69 83885 83948 84011 84073 84136 69 70 84510 84572 84634 84696 84757 70 71 1.85162 1.85187 1 85248 1.85309 1.85370 71 72 85733 85794 85854 | į | 59 | 77085 | 77159 | 77232 | 77305 | 77379 | 59 |
| 62 79239 79309 79379 79449 79518 62 63 79934 80003 80072 80140 80209 63 64 80618 80686 80754 80821 80889 64 65 81291 81358 81425 81491 81558 65 66 81954 82020 82086 82151 82217 66 67 82607 82672 82737 82802 82866 68 68 83251 83315 83378 83442 83506 68 69 83885 83948 84011 84073 84136 69 70 84510 84572 84634 84696 84757 70 71 1.85162 1.85187 1 85248 1.85309 1.85370 71 72 85733 85794 85854 85914 85974 72 73 86322 86492 87040 87099 | | 60 | 77815 | 77887 | 77960 | 78032 | 78104 | 60 |
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| 66 81954 82020 82086 82151 82217 66 67 82607 82672 82737 82802 82866 67 68 83251 83315 83378 83442 83506 68 69 83885 83948 84011 84073 84136 69 70 84510 84572 84634 84696 84757 70 71 1.85162 1.85187 1 85248 1.85309 1.85370 71 72 85733 85794 85854 85914 85974 72 73 86332 86392 86451 86510 86570 73 74 86923 86982 87040 87099 87157 74 75 87506 87564 87622 88618 8874 77 76 88081 88138 88195 83252 83309 76 77 864949 8275 89321 89576 | 1 | 64 | 80618 | 80686 | 80754 | 80821 | 80889 | 64 |
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| 74 86923 86982 87040 87099 87157 74 75 87506 87564 87622 87679 87737 75 76 88081 88138 88195 88252 88309 76 77 88649 88705 88762 88818 88874 77 78 89269 89265 89321 89376 89432 78 79 89763 89818 89873 89927 89982 79 80 90309 90363 90417 90472 90526 80 81 1.90849 1.90902 1.90956 1.91009 1.91062 81 82 91381 91434 91487 91540 91593 82 83 91908 91960 92012 92065 92117 83 84 92428 92480 92531 92583 92634 84 85 92942 92993 93044 93095 | - | | | | | 86510 | | |
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| 79 89763 89818 89873 89927 89982 79 80 90309 90363 90417 90472 90526 80 81 1.90849 1.90902 1.90956 1.91009 1.91062 81 82 91381 91434 91487 91540 91593 82 83 91908 91960 92012 92065 92117 83 84 92428 92480 92531 92583 92634 84 85 92942 92993 93044 93095 93146 85 86 93450 93500 93551 93601 93651 86 87 93952 94002 94052 94101 94151 87 88 9448 94547 94596 94645 88 89 94939 94988 95036 95085 95134 89 90 95424 95472 95521 95569 96517 | - | 78 | 89209 | | | 89376 | | |
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| 83 91908 91960 92012 92065 92117 83 84 92428 92480 92531 92583 92634 84 85 92942 92993 93044 93095 93146 85 86 93450 93500 93551 93601 93651 36 87 93952 94002 94052 94101 94151 87 88 94448 94498 94547 94596 94645 88 89 94939 94988 95036 95085 95134 89 90 95424 95472 95521 95569 95617 90 91 1.95904 1.95952 1.95999 1.96047 1.96095 91 92 96379 96426 96473 96520 96567 92 93 96848 96895 96942 96988 97035 93 94 97313 97359 97405 97451 97497 94 95 97772 97818 97864 9790 | - | 81 | 1.90849 | 1.90902 | 1.90956 | 1.91009 | 1.91062 | 81 |
| 83 91908 91960 92012 92065 92117 83 84 92428 92480 92531 92583 92634 84 85 92942 92993 93044 93095 93146 85 86 93450 93500 93551 93601 93651 36 87 93952 94002 94052 94101 94151 87 88 94448 94498 94547 94596 94645 88 89 94939 94988 95036 95085 95134 89 90 95424 95472 95521 95569 95617 90 91 1.95904 1.95952 1.95999 1.96047 1.96095 91 92 96379 96426 96473 96520 96567 92 93 96848 96895 96942 96988 97035 93 94 97313 97359 97405 97451 97497 94 95 97772 97818 97864 9790 | | 82 | 91381 | 91434 | 91487 | 91540 | | |
| 84 92428 92480 92531 92583 92634 84 85 92942 92993 93044 93095 93146 85 86 93450 93500 93551 93601 93651 86 87 93952 94002 94052 94101 94151 87 88 94448 94498 94547 94596 94645 88 89 94939 94988 95036 95085 95134 89 90 95424 95472 95521 95569 95617 90 91 1.95904 1.95952 1.95999 1.96047 1.96095 91 92 96379 96426 96473 96520 96567 92 93 96848 96895 96942 96988 97035 93 94 97313 97359 97405 97451 97497 94 95 97772 97818 97864 97909 | | | 91908 | 91960 | 92012 | 92065 | | |
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| No. C. Sine C. Tang. C. C. C. C. C. C. C. | } | 517 | rificial | | | nd Secant | 8. 1 | 59 (| | | |
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| No. C. Sine Tang. C. Tang. Tang. C. Tang | | | | | | | | | | | |
| No. | - | C. Sille | OHIC (| | | C. Secamp | Becant | 1141 | | | |
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| 1 (4 1) EP (CCS. | - | | , | | Degrees. | | | .) | | | |

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| | 35 40 | 1 | | 52870 | | | 4 | |
| | 45 | 50710 | 97632 | 53078 | | | | |
| | 4 5 | | 97610 | | | | | |
| | 55 | 51080 | 97589 | 53492 | 46508 | | | |
| 1 | 60 | | | 53697 | 46303 | | | |
| 1 | | Co-Sine | | C. Tang | | C Secant | | |
| | VIII | Co-Sine | Sine) | | egrees. | o Secant | Secant. | TAT |
| | _ | | | | | | | = |
| | | | | | egrees. | | | |
| | M | Sine | Co.Sine | Tang. | C. Tang. | Secant. | C.Secant | M |
| | 0 | 9.51264 | 9.97567 | 9.53697 | 10.46303 | 10.02433 | 10.48736 | 60 |
| | 5 | 51447 | 97545 | 53902 | 46098 | 02455 | 48553 | 55 |
| | 10 | 51629 | 97523 | 54106 | 45894 | | | 2 |
| | 15 | 51811 | 97501 | 54309 | | | | 1 |
| | 20 | 51991 | 97479 | 54512 | | | | |
| | 25 | 52171 | 97457 | 54714 | 45286 | 02543 | 47829 | 35 |
| 1 | 30 | 52350 | 97435 | 54915 | 45085 | 02565 | 47650 | 30 |
| | 35 | 9.52527 | 9.97412 | 9.55115 | 10.44885 | 10.02588 | 10.47473 | 25 |
| | 40 | 52705 | 07390 | 5531 5 | | | | 20 |
| | 45 | 52881 | 97367 | 55514 | | | | |
| | 50 | 53056 | | 55712 | | | | |
| - 1 | 5 5 | 53231 | 97322 | 55910 | | | | • |
| 1 | 60' | 53405 | 1 | 56107 | | | 100 | 0 |
| * | M | Co-Sine | Sine | C.Tang | | C.Secant | Secant . | M |
| | M | | | 70 L | egrees | | | |
| 1 | = | | | 20 1 | egrees. | | | =. |
| | $\overline{\mathbf{M}}$ | Sine | Co-Sine | | C. Targ | Secant. | C.Secant | M |
| | | | | | | | 10.46395 | |
| | 5 | 53578 | 97275 | 56303 | | | | |
| 1 | 10 | 53751 | 97252 | 56498 | | | | |
| | 15 | 53922 | 97229 | 56693 | | | | |
| | 20 | 1 | 97206 | 56887 | | | | |
| | 25 | 54263 | 97182 | 57081 | | | | _ |
| | 30 | | 97159 | 57274 | 42726 | | 45567 | |
| | | | | 9.57466 | 10.42534 | 10.02865 | 10.45399 | $\frac{1}{25}$ |
| | 40 | | | 57658 | | | 45231 | _ |
| | 45 | | | 57849 | | 02913 | 45064 | |
| | 50 | | 1 | 58039 | 41961 | 02937 | 44898 | - 1 |
| | 55 | | | 58229 | 41771 | 02961 | 44732 | 5 |
| * | 60 | | 1 . | 58418 | 41582 | 02985 | 44567 | 0 |
| - | | C.Sine. | | C.Tang | Tang. | C.Secant | Secant | $\overline{\mathbf{M}}$ |
| 1 | - | , 0.0 | | | egrees. | | | - [|

| 1 - | | | | Degrees. | d Secants. | 16 | |
|---------------|--|---------|---------|----------|--|------------|----|
| M | Sine | C. Sine | | | | C.Secanty | 1 |
| - | | | | | | 10.44567 6 | |
| 5 | 55597 | 96991 | 5860 6 | | 03009 | | |
| 110 | | 96966 | 58794 | 41206 | 03009 | | |
| 15 | 55923 | 96942 | 58981 | 41019 | 03058 | | |
| 20 | 56085 | 96917 | 59168 | 40832 | 03083 | | |
| 25 | 56247 | 96893 | 59354 | 40646 | 03107 | 437533 | _ |
| 30 | 56408 | 96868 | 59540 | 40460 | 031 32 | 435923 | |
| 35 | | 9.96843 | 9.59725 | 10.40275 | 10.03157 | _ | 25 |
| 40 | | 96818 | 59909 | 40091 | 03182 | 43273 2 | |
| 45 | 56836 | 96793 | 60093 | 39907 | 03207 | | 5 |
| 50 | | 96767 | 60276 | 39724 | | 100 | 0 |
| 55 | 57201 | 96742 | 60459 | 39541 | | | 5 |
| 160 | | 96717 | 60641 | 39359 | | 42642 | 0 |
| $\frac{1}{M}$ | C. Sine | Sine. | C·Tang: | Tang. | C.Secant | Secant. | M |
| 1- | , | | | egrees. | | | |
| 1- | | | | egrees. | | | - |
| 1 | Qin o | C Sino | | | Socont | C.Secant/ | М |
| M | | C.Sine | Tang. | C. Tang | - | | |
| | 1 | 9.96717 | | | 10.03283 | 1 | |
| 5 | | 1 | 60823 | | | | |
| 10 | 1 | | | | 1 | | |
| 15 | | | | | ì | | |
| 20 | • | | | | | 1 | |
| 25 | 1 | | | | | | |
| 30 | | | | | - | | - |
| - 1 | 1 | | | 10.38099 | | 10.41564 | |
| 40 | | | | | | | |
| 45 | 1 | | | | | 1 | 1 |
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| NI - | C.Sine | Sine | | | C.Secan. | Secant. | - |
| ١. | | | 67 L | egrees. | The second secon | | _ |
| | Branchik all Wijersele Albertanssteine – ter | - | | egrees. | | | |
| M | Sine | C.Sine | Tang. | C. Tang | Secant | C.Secant | M |
| 1 | 9.59188 | | | | | 10.40812 | |
| 5 | 1 | | | | | | |
| 10 | | | 63135 | 36865 | 03651 | 40516 | 50 |
| 12.5 | | | 63310 | | | | 3 |
| 20 | 59778 | 96294 | 63484 | 36516 | 03706 | | |
| 25 | 59924 | 96267 | 1 | | | | |
| 30 | 60070 | 96240 | 63830 | 36170 | 03760 | 39930 | 30 |
| 3 | 9.60215 | 9.96212 | 9.64003 | 10.35997 | 10.03788 | 10.39785 | 25 |
| 4(| | | | | | 39641 | 20 |
| 4. | 60503 | 96157 | 64346 | | | | |
| 5(| 60646 | 96129 | 64517 | | | | _ |
| 5 | 60789 | 1 | 1 | | 1 | | 5 |
| 60 | 60931 | 96073 | 64858 | | | 1 | 0 |
| IV | I C.Sine | Sine | C.Tang. | l Tang. | C.Secano | Secant | M |
| 1 | | | | Degrees. | | | |

| re |) <u>ど</u> | Artifici | | , , , | ts and Se | cants. | | | | |
|--------|-------------|------------------|----------|-------------------------|-----------|-----------|------------------------------------|--|--|--|
| 1_ | 24 Degrees. | | | | | | | | | |
| M | Sine | CoSine | Tang. | C. Tang. | Secant | C.Secant | M | | | |
| C | 9.60931 | 9.96073 | 9.64858 | 10.3514^{2} | 10.03927 | 10.39069 | 60 | | | |
| 5 | 6107.3 | 96045 | 65028 | 34972 | 03955 | 38927 | 55 | | | |
| 10 | 61214 | 96017 | 65197 | 34803 | 03983 | 38786 | 50 | | | |
| 15 | 61354 | 95988 | 65366 | 34634 | 04012 | | 1 | | | |
| 20 | 61494 | 95960 | 65535 | 34465 | 04040 | | _ | | | |
| 25 | 61634 | 95931 | 65703 | 34297 | 04069 | | | | | |
| 30 | 61773 | 95902 | 65870 | 34130 | 04098 | | | | | |
| 35 | 9.61911 | 9.95873 | 9,66038 | 10.33962 | 10,04127 | 10.38089 | 2.5 | | | |
| 40 | | 95844 | | | | 1-0.000 | 1 | | | |
| 45 | | 95815 | | | | | | | | |
| 50 | 1 | | - | | | 0.0.1 | | | | |
| 55 | | 95757 | 66702 | | | | 5 | | | |
| 60 | | 95728 | | | | | | | | |
| M | | | | | C.Secant | | $\overline{\overline{\mathbf{M}}}$ | | | |
| - | 00 011,0 | | | Degrees | | . Sccanc | | | | |
| - | | | | | | | | | | |
| 1_ | | | | Degrees | | | | | | |
| M | Sine | Co-sine | Tang. | C. Tang. | Secant | C.Secant | M | | | |
| 0 | | 9.95728 | 9.66867 | 10.33133 | 10.04272 | 10.37405 | 60 | | | |
| 5 | 72730 | 95698 | 67032 | 32968 | 04302 | 37270 | 55 | | | |
| 10 | 62865 | 95668 | 67196 | 32804 | 04332 | 37135 | 50 | | | |
| 15 | 62999 | 95639 | 67360 | 32640 | 04361 | 37001 | 45 | | | |
| 20 | | 95609 | 67524 | 32476 | 04391 | 36867 | 40 | | | |
| 25 | | 95579 | 67687 | 32313 | 04421 | 36734 | 35 | | | |
| 30 | 63398 | 95549 | 67850 | 32150 | 04451 | 36602 | 30 | | | |
| 35 | 9.63551 | 9.95519 | 9.68012 | 10.31988 | 10.04481 | 10.36469 | 25 | | | |
| 40 | | | 63174 | 34826 | | 36338 | - 1 | | | |
| 45 | 63794 | 95458 | 68336 | 31664 | 04542 | 36206 | 15 | | | |
| 50 | 63924 | 95427 | 68497 | 31503 | 04573 | 36076 | 10 | | | |
| 55 | 64054 | 95397 | 68658 | 31342 | -04603 | 35946 | 5 | | | |
| 60 | 64184 | 95366 | 68818 | 31,182 | 04634 | 35816 | 0 | | | |
| M | Co-Sine | Sine | C.Tang. | Tang. | C.Secant | Secant | $\overline{\mathbf{M}}$ | | | |
| | | | | Degrees. | ′ | | _ | | | |
| | | | 26 | Degrees. | | | - | | | |
| M | Sine | Co-Sine | | C. Tang. | Secont | C.Secant | NA | | | |
| 1 | | | | | | | | | | |
| 0 5 | 64313 | 9.95366 95335 | | 31022 | | 10.35816 | - 1 | | | |
| 10 | | 95304 | 69138 | 30862 | | 35687 | - 1 | | | |
| 15 | 64571 | 95273 | 69298 | 30702 | | 35558 | - 1 | | | |
| 20 | | | 69298 | 30702 | 04727 | 35429 | - 1 | | | |
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| 104 | 164 Artificial Sines, Tangents and Secants. | | | | | | | | | |
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| \ | 30 Degrees. | | | | | | | | | |
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| | Co diffic | , conse | The second secon | egrees. | io secant | Secant. IM | | | | | | |
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| Dita | 0: | C - Ci | | Degrees. | | | | | | | | |
| M | | Co.Sine | 1 | C. Tang. | | C.Secant M | | | | | | |
| | 9.80807 | 9.88425 | 9.92381 | 10.07619 | | 10.19193 60 | | | | | | |
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| 1 | | | | | | $\frac{10.18672}{10.18672}$ 25 | | | | | | |
| 40 | 81402 | 87996 | 93406 | | | | | | | | | |
| 45 | 81475 | | | | | | | | | | | |
| 50 | 81549 | 87887 | | | | | | | | | | |
| 55 | | | 93789 | 06211 | | | | | | | | |
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| M | Co-Sine | Sine. | C.Tang | Tang. | C.Secant | Secant M | | | | | | |
| _ | | The Control of the Co | 49 I | egrees. | * | | | | | | | |
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| 1 | C.Sine. | - | | | C.Secant | | | | | | | |
| - | · C.OHC. | Jille. | THE PERSON NAMED IN COLUMN 1997 | The second secon | O.Becant | - Decant IVI | | | | | | |
| 1 | | | 48 Degrees. | | | | | | | | | |

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|------------|-----------------|----------|---------|---------|--|----------|----------|----------------|
| 1 | M | Sinc | C. Sine | Tang. | C. Tang. | Secant | C.Secant | M |
| | 0 | 9.82551 | 9.87107 | 9.95444 | 10.04556 | 10.12893 | 10.17449 | 60 |
| | 5 | 82621 | 87050 | 95571 | 04429 | 12950 | 17379 | 55 |
| 1 | 0 | 82691 | 86993 | 95698 | 04302 | 13007 | 17309 | 50 |
| 1 | . 5 | 82761 | 86936 | 95825 | 04175 | 13064 | 17239 | 45 |
| 2 | 20 | 82830 | 86879 | 95952 | 04048 | 13121 | 17170 | 40 |
| 2 | 25 | 82899 | 86821 | 96078 | 03922 | 13179 | 17101 | 35 |
| 3 | 30 | 82968 | 86763 | 96205 | 03795 | 13237 | 17032 | 30 |
| 3 | 35 | 9.83037 | 2.86705 | 9.96332 | 10.03668 | 10.13295 | 10.16963 | $\frac{}{25}$ |
| - 1 | ŀO. | 83106 | 86647 | 96459 | 03541 | 13353 | 16894 | |
| | 5 | 83174 | 86589 | 96586 | | | 16826 | |
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| - [| 55 | 83310 | 86472 | 96839 | | | 16690 | |
| | 50 | 83378 | 86413 | 96966 | | | 16622 | |
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| 1 | VII | C. Sine | Sine | | | C.Secant | Secant | M |
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